## Part IA Paper 1: Mechanical Engineering

## THERMOFLUID MECHANICS

## Examples Paper 5

(Starter questions are marked "s", Elementary ones $\dagger$, and Tripos standard *)
sQ1 A refrigerator extracts heat at a rate of 800 W from a cold space while rejecting heat to the atmosphere at a rate of 1.2 kW . Calculate the power input and the COP?
sQ2 Calculate the efficiency of a reversible heat engine operating between temperature limits of 1000 K and 300 K .
sQ3 Give two examples of (a) irreversible processes, and (b) reversible processes. What defines a reversible process?
sQ4 A quantity of Argon gas $(\gamma=1.67)$, initially at 1 bar and 300 K , is compressed adiabatically and reversibly (and hence isentropically) to half its initial volume. Calculate the final pressure and temperature.

## The Second Law and Entropy

Q5 Fill in the blanks as appropriate for the following systems (a-f), all of which are undergoing cyclic processes and exchanging heat with two reservoirs. Identify each of the possible devices as an engine, refrigerator, heat pump or other device.

| System: | a | b | c | $\mathbf{d}$ | e | $\mathbf{f}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Source temperature, ${ }^{\circ} \mathrm{C}$ | 327 |  | 300 | 60 | 327 | 140 |
| Sink temperature, ${ }^{\circ} \mathrm{C}$ | 27 | 70 | 100 | 60 | 827 |  |
| Heat from source, $\mathrm{kJ} / \mathrm{h}$ | 10000 | 7000 |  |  | 6000 | 6000 |
| Heat to sink, $\mathrm{kJ} / \mathrm{h}$ | 5500 |  |  | 1440 |  | 5000 |
| Power output, kW |  |  | 29.3 | -0.4 |  | 0.3 |
| Thermal efficiency, $\%$ |  |  | 40 |  |  |  |
| $\mathrm{COP}_{\mathrm{R}}$ |  | 3.5 |  |  |  |  |
| $\mathrm{COP}_{\mathrm{F}}$ |  |  |  |  | 2.2 |  |
| Rev., irrev., impossible |  | rev |  |  |  |  |

A gas-powered refrigerator works by taking in heat from a heat exchanger at $500^{\circ} \mathrm{C}$ and from a cold space at $-10^{\circ} \mathrm{C}$, while rejecting heat to the environment at $35^{\circ} \mathrm{C}$. The refrigerator is a cyclic device, and there is no work input or output. Use the Clausius inequality to find the minimum rate at which heat must be supplied by the heat exchanger in order to extract heat at a rate of 1 kW from the cold space.
*Q7 A cyclic heat pump takes 600 MJ (mega joules) of heat at $27^{\circ} \mathrm{C}$ while rejecting heat to a system whose temperature rises $1^{\circ} \mathrm{C}$ for each MJ of energy supplied to it. Initially this system is also at $27^{\circ} \mathrm{C}$.
(a) Explain why there is a limit on the final temperature of the system. State whether it is an upper or lower limit, and under what circumstances it would be reached.
(b) Calculate the limit on the final temperature of the system. What is the work input to the heat pump when this limit is achieved?

Q8 (a) A mass, $m$, of iron is heated reversibly from temperature $T_{1}$ to $T_{2}$. During this process it may be assumed that the change in volume is negligible. Show that the change in entropy is given by:

$$
\Delta S=m c_{\mathrm{v}} \ln \left(\frac{T_{2}}{T_{1}}\right)
$$

where $c_{v}$ is assumed constant.
(b)* A system comprises two blocks of iron, one of mass 1 kg and initially at $20^{\circ} \mathrm{C}$, the other of mass 2 kg and initially at $400^{\circ} \mathrm{C}$. The blocks are brought into thermal contact so that there is heat transfer between them, but there is no heat exchange with the surroundings.
(i) Use the First Law to determine the final temperature of the system.
(ii) Calculate the increase in entropy of the 1 kg block.
(iii) Calculate the decrease in entropy of the 2 kg block.
(iv) Show that the process is irreversible.
(v) Explain why the result derived in part (a) for a reversible process is still valid for this irreversible process.
Take $c_{\mathrm{v}}=450 \mathrm{~J} / \mathrm{kgK}$ for iron.
(c)* Describe how the system described in part (b) can be returned to its initial state by means of a reversible heat pump. What other process is also required? Explain why the original process in (b) must have been irreversible, even though the initial state can be restored.
*Q9 With reference to sketches of suitable cyclic devices, show that violation of the Clausius statement of the Second Law implies violation of the Kelvin-Planck statement and vice versa and hence that the two statements are equivalent. (Hint: you may wish to review example 5.2 in the notes first.)

Q10 Starting from the appropriate "Tds" equation, show that lines of constant specific volume on a T-s diagram for a perfect gas have gradients that are proportional to the absolute temperature. Sketch carefully two such lines, distinguishing between high and low specific volume.

Q11 A certain gas has a specific heat capacity at constant volume given by $c_{v}=(\alpha+\beta T)$ where $\alpha=200 \mathrm{~J} \mathrm{~K}^{-1} \mathrm{~kg}^{-1}, \beta=0.1 \mathrm{~J} \mathrm{~K}^{-2} \mathrm{~kg}^{-1}$ and $T$ is the temperature in Kelvin. When it is expanded reversibly and adiabatically from a temperature of 1000 K to a larger volume, its temperature falls to 700 K . When it is expanded adiabatically from the same initial state into an evacuated space such that the final volume is the same, its temperature falls instead to 950 K .
(a) Sketch the two processes on a T-S diagram.
(b) Explain why the gas cannot be an ideal gas.
(c) Calculate for each process the entropy change per unit mass of gas.

Q12 (a) Calculate the work done and change in entropy when 0.1 kg of helium, confined in a cylinder by a piston, expands adiabatically from a volume of $0.1 \mathrm{~m}^{3}$ and a pressure of 8 bar to a volume of $0.8 \mathrm{~m}^{3}$ and a pressure of 0.4 bar.
(b) Sketch the process on a T-S diagram and include the lines of constant volume that pass through the initial and final states.
(c) By reference to the sketch, determine which type of process will give the maximum work output for any adiabatic expansion from the same initial conditions to the same final volume. Calculate this maximum work output.

## Reciprocating Internal Combustion Engines

Q13 The air-standard Otto cycle provides an approximate model for spark ignition engines. The following data apply to the gas engines that you have tested in the laboratory, when operating at 250 rpm .

|  | National | Hornsby-S. |
| :--- | :---: | :---: |
| Cylinder diameter | 0.178 m | 0.184 m |
| Piston stroke (distance between TDC and BDC) | 0.381 m | 0.381 m |
| Compression ratio $\left(\mathrm{V}_{\max } / \mathrm{V}_{\min }\right)$ | 4.5 | 4.5 |
| Firing strokes per minute | 107 | 107 |
| Atmospheric pressure | 101325 Pa | 101325 Pa |
| Atmospheric temperature | 293 K | 293 K |
| Indicator calibration | $54 \mathrm{kPa} / \mathrm{mm}$ | $54 \mathrm{kPa} / \mathrm{mm}$ |

In the following calculations, assume that the airffuel mixture and the products of combustion all have the same properties as air, and that the combustion process is equivalent to a heat input of $1460 \mathrm{~kJ} / \mathrm{kg}$.
(a) For the engine that you tested calculate:
(i) The maximum and minimum volumes during the cycle.
(ii) The mass of air in the cylinder, assuming that conditions at the start of the compression process are the same as those of the atmosphere.
(iii) The pressure and temperature at the end of the compression process, assuming this to be isentropic. Calculate also the compression work.
(iv) The pressure and temperature at the end of the combustion process, assuming this to occur at constant volume.
(v) The pressure and temperature at the end of the power stroke, assuming this to be isentropic. Calculate also the work done during this expansion process.
(vi) The work done per cycle, the thermal efficiency and the power output. Confirm that the value of efficiency agrees with that given by the expression for $\eta_{\text {oto }}$ derived in lectures.
(b) Compare the values of pressure calculated above with those you have measured in the laboratory experiment on the indicator diagram. Compare also the measured power output and efficiency based on the work determined from the indicator diagram (i.e. the indicated efficiency) with that calculated above.

Q14 The figure below shows the p-V diagram for an air-standard Diesel cycle.

(a) For this cycle, find expressions for:
(i) The temperature at the end of the compression, $T_{\mathrm{B}}$, in terms of $T_{\mathrm{A}}$ and $r_{\mathrm{v}}$.
(ii) The temperature after "combustion", $T_{\mathrm{C}}$, in terms of $T_{\mathrm{A}}, r_{\mathrm{v}}$, and $\alpha$.
(iii) The temperature after the expansion, $T_{\mathrm{D}}$, in terms of $T_{\mathrm{A}}, r_{\mathrm{v}}$, and $\alpha$.
(b) Using your answers to (a), find expressions for the heat input, $Q_{1}$, and heat rejected, $Q_{2}$, per unit mass of air. Hence show that the cycle efficiency is given by:

$$
\eta_{\text {diesel }}=1-\frac{1}{r_{v}^{\gamma-1}}\left(\frac{\alpha^{\gamma}-1}{\gamma(\alpha-1)}\right)
$$

(c) Noting that the term in brackets is always greater than unity, show that the Diesel cycle is always less efficient than an Otto cycle with the same compression ratio.
(d) Why do "diesel" engine cars usually have a better fuel economy than similar petrol engine cars?

## ANSWERS:


Q14
(a) (i) $T_{\mathrm{B}}=T_{\mathrm{A}} r_{\mathrm{v}}^{\gamma-1}$
(ii) $T_{\mathrm{C}}=T_{\mathrm{A}} \alpha_{v}^{\gamma-1}$
(iii) $T_{\mathrm{D}}=T_{\mathrm{A}} \mathrm{\alpha}^{\gamma}$

## SUGGESTED TRIPOS QUESTIONS:

| Part IB Paper 4: | 2007 Q1 $^{*}$ | 2006 Q2 | 2005 Q2 (a) \& (b) | 2003 Q3 |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Part 1A Paper 1: | 2012 Q4, Q5 | 2010 Q3 | 2008 Q6 | 2007 Q6 $^{2}$ | 2004 Q3 |

* NOTE: Replace "PER" with "COP" in this question

