# Structures Data Book 

## 2018 Edition



## Cambridge University Engineering Department

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## 1. Physical properties of structural materials

Representative values to be used in calculations (further details in Materials Data Book and Section 10)

|  |  | Steel | Aluminium <br> Alloy | Concrete $^{*}$ | Softwood* <br> along <br> grain | Water | units |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Young's modulus | $E$ | 210 | 70 | 30 | 9 | - | GPa |
| Shear modulus | $G$ | 81 | 26 | 13 | - | - | GPa |
| Bulk modulus | $K$ | 175 | 69 | 14 | - | 2.2 | GPa |
| Poisson's ratio | $v$ | 0.30 | 0.33 | 0.15 | - | - |  |
| Thermal expansion | $\alpha$ | 11 | 23 | 12 | - | 60 | $\times 10^{-6} \mathrm{~K}^{-1}$ |
| Density | $\rho$ | 7840 | 2700 | 2400 | - | 1000 | $\mathrm{~kg} \mathrm{~m}^{-3}$ |

* Typical values

For isotropic solids,

$$
G=\frac{E}{2(1+v)} ; \quad K=\frac{E}{3(1-2 v)}
$$

## 2. Stress and strain

### 2.1. Notation for stress

$\sigma_{x x}$ is the normal stress on the $x$ face acting in the $x$ direction.
$\tau_{x y}$ is the shear stress on the $x$ face acting in the $y$ direction.
In this data book, with the exception of Section 9, tensile stresses are defined as positive.

### 2.2. Strain definition

$\varepsilon_{x x}$ is the normal strain in the $x$ direction.
$\gamma_{x y}$ is the shear strain between the $x$ and $y$ faces.

$$
\varepsilon_{x x}=\frac{\partial u}{\partial x} ; \quad \gamma_{x y}=\frac{\partial u}{\partial y}+\frac{\partial v}{\partial x} \quad \text { etc. }
$$

where: $u, v$ are the small displacement components with respect to rectangular co-ordinates $x, y$.

### 2.3. Stress-strain relations for isotropic elastic solids

$$
\begin{gathered}
\varepsilon_{x x}=\frac{1}{E}\left(\sigma_{x x}-v \sigma_{y y}-v \sigma_{z z}\right)+\alpha \Delta T \quad \text { etc. } \\
\gamma_{x y}=\frac{1}{G} \tau_{x y} \quad \text { etc. }
\end{gathered}
$$

where: $\Delta T$ is the temperature change.
For plane stress with the $z$ face unstressed and $\Delta T=0$, the inverse relationship is

$$
\sigma_{x x}=\frac{E}{\left(1-v^{2}\right)}\left(\varepsilon_{x x}+v \varepsilon_{y y}\right) \quad \text { etc. }
$$

### 2.4. Complementary shear

From equilibrium of a small element,

$$
\tau_{x y}=\tau_{y x} \quad \text { etc. }
$$

From its definition,

$$
\gamma_{x y}=\gamma_{y x} \quad \text { etc. }
$$

### 2.5. Planar transformation equations for stress



From equilibrium of an elementary triangle,

$$
\begin{aligned}
& \sigma_{a a}=\sigma_{x x} \cos ^{2} \theta+\sigma_{y y} \sin ^{2} \theta+2 \tau_{x y} \sin \theta \cos \theta \\
& \tau_{a b}=-\sigma_{x x} \sin \theta \cos \theta+\sigma_{y y} \sin \theta \cos \theta+\tau_{x y}\left(\cos ^{2} \theta-\sin ^{2} \theta\right)
\end{aligned}
$$

### 2.6. Mohr's circle of stress

A plot of normal stress against shear stress on a face for varying $\theta$ gives a circle, provided a special sign convention is used:

For Mohr's circle, shear stress is plotted positive when it is clockwise


The stresses on perpendicular faces, $\left(\sigma_{x x},-\tau_{x y}\right)$ and $\left(\sigma_{y y}, \tau_{y x}\right)$, plot at the opposite ends of a diameter. If new faces are considered at angle $\theta$ (see Section 2.5), the stresses on the new faces can be obtained by rotating the diameter of Mohr's circle by $2 \theta$ in the same direction.

### 2.7. Planar transformation equations for strain



By geometry,

$$
\begin{aligned}
\varepsilon_{a a} & =\varepsilon_{x x} \cos ^{2} \theta+\varepsilon_{y y} \sin ^{2} \theta+\gamma_{x y} \sin \theta \cos \theta \\
\gamma_{a b} & =-2 \varepsilon_{x x} \sin \theta \cos \theta+2 \varepsilon_{y y} \sin \theta \cos \theta+\gamma_{x y}\left(\cos ^{2} \theta-\sin ^{2} \theta\right)
\end{aligned}
$$

### 2.8. Mohr's circle of strain

A plot of normal strain against half shear strain for varying $\theta$ gives a circle, if the sign convention for shear strains is the same as for corresponding shear stresses:


The strains in perpendicular directions, $\left(\varepsilon_{x x},-\gamma_{x y} / 2\right)$ and $\left(\varepsilon_{y y}, \gamma_{y x} / 2\right)$, plot at the opposite ends of a diameter. If new faces are considered at angle $\theta$ (see Section 2.7), the strains in the new directions can be obtained by rotating the diameter of Mohr's circle by $2 \theta$ in the same direction.

### 2.9. Principal stresses in $\mathbf{3}$ dimensions

The principal stresses can be calculated as the eigenvalues of the stress matrix $\underline{\sigma}$, and the principal directions are the corresponding eigenvectors.

$$
\underline{\boldsymbol{\sigma}}=\left[\begin{array}{ccc}
\sigma_{x x} & \tau_{x y} & \tau_{x z} \\
\tau_{y x} & \sigma_{y y} & \tau_{y z} \\
\tau_{z x} & \tau_{z y} & \sigma_{z z}
\end{array}\right]
$$

### 2.10. Yield criteria for isotropic solids

Tresca's hypothesis:

$$
\max \left[\left|\sigma_{1}-\sigma_{2}\right|,\left|\sigma_{2}-\sigma_{3}\right|,\left|\sigma_{3}-\sigma_{1}\right|\right]=Y
$$

Von Mises' hypothesis:

$$
\left(\sigma_{1}-\sigma_{2}\right)^{2}+\left(\sigma_{2}-\sigma_{3}\right)^{2}+\left(\sigma_{3}-\sigma_{1}\right)^{2}=2 Y^{2}
$$

where: $\quad Y$ is the current yield stress in simple tension $\sigma_{1}, \sigma_{2}, \sigma_{3}$ are the principal stresses.

## 3. Stresses in thin-walled circular pressure vessels with closed ends

$$
\sigma_{h}=\frac{p r}{t} ; \quad \sigma_{l}=\frac{p r}{2 t}
$$

where: $p$ is the internal gauge pressure
$r$ is the radius of the vessel
$t$ is the wall thickness
$\sigma_{h} \quad$ is the hoop stress
$\sigma_{l}$ is the longitudinal stress.

## 4. Beam behaviour

### 4.1. Databook sign convention



### 4.2. Compatibility

$$
\kappa=\frac{d \psi}{d s}=\frac{1}{R}
$$

where: $\kappa$ is the curvature
$R \quad$ is the local radius of curvature
$s$ is a distance along a beam
$\psi \quad$ is the angle turned by tangent to the curve.
For plane sections remaining plane

$$
\varepsilon=\kappa y
$$

where: $\varepsilon$ is the strain due to the curvature
$y$ is the distance from the centroidal axis.
For a beam that has small transverse deflections $v(x)$ from the $x$-axis

$$
\psi \approx-\frac{d v}{d x} ; \quad \kappa \approx-\frac{d^{2} v}{d x^{2}}
$$

### 4.3. Equilibrium


where: $M$ is the bending moment
$S$ is the transverse shear force
$w$ is the transverse external load per unit length of beam.

### 4.4. Elastic bending formulae

### 4.4.1. Longitudinal stresses

$$
\begin{gathered}
\frac{\sigma}{y}=\frac{M}{I}=E \Delta \kappa ; \quad I=\int y^{2} d A \\
M=Z_{e} \sigma_{\max }
\end{gathered}
$$

For an initially straight beam:

$$
M=E I\left(-\frac{d^{2} v}{d x^{2}}\right)
$$

where: $y \quad$ is the distance from the centroidal axis
$\Delta \kappa \quad$ is change of curvature from an initially unstressed configuration
$Z_{e} \quad$ is the elastic section modulus
$\sigma_{\max }$ is the stress at the outermost fibre
$I \quad$ is the second moment of area about a principal axis through the centroid (see also Mechanics Data Book).

## Values of I for simple shapes

Solid circular section

$I_{x x}=\frac{\pi r_{o}^{4}}{4}$

Thin-walled circular section

$I_{x x} \approx \pi r^{3} t$

Solid rectangle


$$
I_{x x}=\frac{b h^{3}}{12}
$$

### 4.4.2. Transverse shear

If a free body is formed by cutting out part of the cross-section of a beam,

$$
q=\frac{S}{I} \int_{A_{c}} y d A=\frac{S A_{c} \bar{y}}{I}
$$

where: is the total longitudinal shear force per unit longitudinal length of the beam (shear flow)
$A_{c} \quad$ is the area of the cut off portion of the cross-section
$A_{c} \bar{y}$ is the first moment of area of the cut off portion about the centroidal axis.
At the cut, the shear stress is, on average:

$$
\tau=\frac{q}{a}
$$

where: $a$ is the length of the cut in the plane of the cross-section.

### 4.5. Formulae for elastic analysis

4.5.1. Deflections for statically determinate structures


$$
\frac{W l^{2}}{24 E I}=\frac{w l^{3}}{24 E I}
$$

$$
\theta=\frac{M l}{3 E I}
$$

4.5.2. Clamping moments for statically indeterminate structures


| $\boldsymbol{M}_{A}$ | $\boldsymbol{M}_{B}$ |
| :--- | :--- |
| $\frac{W l}{8}$ | $\frac{W l}{8}$ |


$\frac{W b^{2} a}{l^{2}}$
$\frac{W a^{2} b}{l^{2}}$

$\frac{W l}{12}=\frac{w l^{2}}{12}$
$\frac{W l}{12}=\frac{w l^{2}}{12}$

$\frac{6 E I \delta}{l^{2}} \quad \frac{6 E I \delta}{l^{2}}$

$\frac{2 E I \theta}{l}$
$\frac{4 E I \theta}{l}$
4.5.3. Bending moment values for selected statically indeterminate cases
$\boldsymbol{M}_{\boldsymbol{A}}$


$$
\frac{W l}{8}=\frac{w l^{2}}{8}
$$



$$
M_{B}
$$

$$
\frac{W l}{16}=\frac{w l^{2}}{16}
$$

4.5.4. Bending moments at mid-span for simply supported beams


### 4.6. Plastic bending

For an initially unstressed beam, first yield in bending

$$
M_{y}=Z_{e} \sigma_{y}
$$

where: $M_{y}$ is the moment at first yield
$Z_{e}$ is the elastic section modulus.

For a beam fully yielded in bending, carrying no axial load, the neutral axis is at the equal-area axis, and

$$
M_{p}=Z_{p} \sigma_{y} ; \quad Z_{p}=\int|y| d A
$$

where: $M_{p}$ is the plastic moment
$Z_{p}$ is the plastic section modulus.
For cross-sections that can be easily split into regions that are fully yielded in either tension or compression,

$$
Z_{p}=\sum A_{i}\left|y_{i}\right|
$$

where: $A_{i}$ is the area of a region
$y_{i}$ is the distance from the beam's equal-area axis to the centroid of the region.
Values of $Z_{e}$ and $Z_{p}$ for simple shapes

Solid circular section

$Z_{e}=\frac{\pi r_{o}^{3}}{4}$
$Z_{e} \approx \pi r^{2} t$
$Z_{p} \approx 4 r^{2} t$
$Z_{p}=\frac{4 r_{o}{ }^{3}}{3}$


Solid rectangle


$$
Z_{e}=\frac{b h^{2}}{6}
$$

$$
Z_{p}=\frac{b h^{2}}{4}
$$

### 4.7. Torsion formulae

### 4.7.1. Circular shafts

For an elastic shaft,

$$
\begin{gathered}
\frac{\tau}{r}=\frac{T}{J} ; \quad J=\int r^{2} d A \\
T=G J \phi
\end{gathered}
$$

where: $T$ is the applied torque
$\phi \quad$ is the angle of twist per unit length
$r$ is the radius
$J$ is the polar second moment of area.

## Values of J for simple circular shapes

Solid circular section Thick-walled circular section Thin-walled circular section


$$
J=\frac{\pi r_{o}{ }^{4}}{2}
$$



$$
J=\frac{\pi\left(r_{o}^{4}-r_{i}^{4}\right)}{2}
$$



$$
J \approx 2 \pi r^{3} t
$$

4.7.2. Thin walled tubes (i.e. closed sections) of arbitrary cross-section By equilibrium,

$$
q=\frac{T}{2 A_{e}}
$$

By kinematics,

$$
\phi=\frac{\oint \gamma d s}{2 A_{e}}
$$

For an elastic tube,

$$
T=G \frac{4 A_{e}^{2}}{\oint \frac{d s}{t}} \phi
$$

where: $q$ is the shear flow $=\tau t$
$A_{e}$ is the area enclosed by the cross-section.

### 4.7.3. Thin-walled open sections

$$
T=G \sum \frac{1}{3} b t^{3} \phi
$$

where: $b$ is the length, and
$t$ is the thickness of a region of the cross-section; $t \ll b$.

## 5. Euler buckling

For a perfect elastic pin-ended compression member (strut),

$$
P_{E}=\frac{\pi^{2} E I}{L^{2}}
$$

where: $P_{E}$ is the Euler buckling load
$E I$ is the bending stiffness of the strut about the appropriate axis
$L \quad$ is the length of the strut

$$
\sigma_{E}=\frac{P_{E}}{A}=\frac{\pi^{2} E}{(L / k)^{2}}
$$

where: $\sigma_{E}$ is the Euler buckling stress
$A$ is the cross-sectional area of the strut
$k \quad$ is the radius of gyration $=\sqrt{I / A}$.

## 6. Pin-jointed trusses - statical determinacy

For a pin-jointed assembly (Maxwell's rule, modified):

$$
s-m=b+r-D j
$$

where: the pin jointed assembly is in $D$ dimensions ( 2 or 3 ) with $b$ bars and $j$ joints
$r$ is the number of restraints on joint displacement
$s \quad$ is the number of redundancies (states of self-stress)
$m$ is the number of independent mechanisms (degrees of freedom).

## 7. Equation of virtual work

For a pin-jointed framework, for any system of external forces $W$ at the joints in equilibrium with bar tensions $P$, and any system of joint displacements $\delta$ compatible with member extensions $e$,

equilibrium set
compatible set
For other kinds of structure the equation is similar: external virtual work equals internal virtual work, provided that all the relevant contributing terms are included.

On L.H.S.: force•displacement, and/or couple•rotation, or pressure•swept volume, etc.
On R.H.S.: tension extension, and/or bending moment curvature $\delta s$, and/or $\sigma \cdot \varepsilon \delta V$, or $\tau \cdot \gamma \delta V$, etc.

## 8. Cables

### 8.1. Flexible cable in frictional contact with a curved surface

$$
T_{2}=T_{1} e^{\mu \theta}
$$

where: $\quad T_{1}$ and $T_{2}$ are the cable tensions on either side of the contact
$\mu$ is the coefficient of friction between the surface and the cable
$\theta$ is the angle subtended by the contact.

### 8.2. Flexible cable between supports subjected to a uniformly distributed

 load$T=w \sqrt{\left(\frac{L^{2}}{2 d}\right)^{2}+x^{2}} ; \quad s=\int \sqrt{1+\left(\frac{d y}{d x}\right)^{2}} d x \approx 2 L+\frac{4}{3} \frac{d^{2}}{L}$ for small $d / L$
where: $T$ is the tension in the cable
$w$ is the load per unit horizontal length
$2 L$ is the length between supports
$d$ is the sag at midspan
$x$ is the horizontal distance from the centre
$s \quad$ is the cable length.

## 9. Soil mechanics

### 9.1. Definitions



Specific Gravity of soil solids
Voids ratio:

Water content:

Degree of saturation:

Bulk unit weight of soil:

Dry unit weight of soil:

Unit weight of dry soil:

Buoyant unit weight of soil

Relative density
$G_{s}$
$e=\frac{V_{v}}{V_{s}} \quad$ Unit weight of water $\gamma_{w}=9.81 \mathrm{kN} \mathrm{m}^{-3}$ $w=\frac{W_{w}}{W_{s}}$ $S_{r}=\frac{V_{w}}{V_{v}}=w \frac{G_{S}}{e}$
$\gamma=\frac{W_{t}}{V_{t}}=\frac{\gamma_{w}\left(G_{s}+S_{r} e\right)}{(1+e)}$
$\gamma=\frac{W_{s}}{V_{t}}=\frac{\gamma_{w} G_{S}}{(1+e)}$
$\gamma=\frac{s}{V_{t}}=\frac{\gamma_{w}\left(G_{S}\right)}{(1+e)}$
$\gamma^{\prime}=\gamma-\gamma_{w}=\frac{\gamma_{w}\left(G_{S}-1\right)}{(1+e)}$
$I_{D}=\frac{\left(e_{\max }-e\right)}{\left(e_{\max }-e_{\min }\right)}$
where: $e_{\max }$ is the maximum voids ratio achievable in a quick tilt test, and
$e_{\min }$ is the minimum voids ratio achievable by vibratory compaction.

### 9.2. Classification of particle sizes

Clay smaller than 0.002 mm (two microns)
Silt between 0.002 and 0.06 mm
Sand between 0.06 and 2 mm

Gravel between 2 and 60 mm
Cobbles between 60 and 200 mm
Boulders larger than 200 mm
$D \quad$ equivalent diameter of soil particle
$D_{10}, D_{60} \quad$ particle size such that $10 \%$ (or $60 \%$ ) by weight of a soil sample is composed of finer grains.

### 9.3. Groundwater seepage

porewater pressure $u$

$h=u / \gamma_{w}$
Potential
$\bar{h}=h+y$
Hydraulic gradient $\quad i=-\nabla \bar{h}$

Darcy's law for laminar flow:

$$
v=k i
$$

where: $v$ is superficial seepage velocity
$k$ is coefficient of permeability.
Typical values:
clays $\quad: k$ between $10^{-11}$ and $10^{-9} \mathrm{~m} \mathrm{~s}^{-1}$
1 micron $<D_{10}<10 \mathrm{~mm}: k$ approximately $0.01\left(D_{10} \text { in } \mathrm{mm}\right)^{2} \mathrm{~m} \mathrm{~s}^{-1}$
$D_{10}>10 \mathrm{~mm}:$ non-laminar flow.

### 9.4. Stresses in soils

### 9.4.1. Sign convention

The normal sign convention for soil mechanics is to denote compressive stresses as positive. Hence in Section 9.4 only, compressive stresses are positive quantities.

### 9.4.2. Principle of effective stress (saturated soil)

Total stress Effective stress Pore water components components pressure
$\sigma \quad=\quad \sigma^{\prime} \quad+$
u
$\tau \quad=$
$\tau^{\prime}$
$+$
0
(The dash on the effective shear stress components is normally omitted).

### 9.4.3. Plane strain stresses in soil: Definitions

Mohr's circle of stress:
mobilised angle of shearing $\phi^{\prime}$
mean effective stress
mobilised shear strength

$$
\begin{aligned}
& s^{\prime}=\left(\sigma_{1}^{\prime}+\sigma_{3}^{\prime}\right) / 2 \\
& t=\left(\sigma_{1}^{\prime}-\sigma_{3}^{\prime}\right) / 2=\left(\sigma_{1}-\sigma_{3}\right) / 2 \\
& \sin \phi^{\prime}=\frac{\mathrm{t}}{s^{\prime}}=\frac{\sigma_{1}-\sigma_{3}}{\sigma_{1}+\sigma_{3}}
\end{aligned}
$$

### 9.5. Undrained strength of soil: Cohesion hypothesis (Tresca)

Undrained behaviour is exhibited by clays in the short term.
In constant-volume tests on clay, failure occurs when $t$ reaches $t_{\text {max }}=c_{u}$
where: $c_{u}$ is the undrained shear strength, which depends primarily on the voids ratio $e$.
The active and passive total horizontal stresses ( $\sigma_{a}$ and $\sigma_{p}$ ) are related to the vertical total stress $\sigma_{v}$ by

$$
\begin{aligned}
& \sigma_{a}=\sigma_{v}-2 c_{u} \\
& \sigma_{p}=\sigma_{v}+2 c_{u}
\end{aligned}
$$

### 9.6. Drained strength of soil: Friction hypothesis (Coulomb)

Drained behaviour is exhibited by sands in the short term and all soils in the longterm.

Earth pressure coefficient

$$
\begin{gathered}
K \\
\sigma_{h}^{\prime}=K \sigma_{v}^{\prime}
\end{gathered}
$$

Active pressure $\left(\sigma_{v}^{\prime}>\sigma_{h}^{\prime}\right)$

$$
K_{a}=\frac{1-\sin \phi^{\prime}}{1+\sin \phi^{\prime}}
$$

Passive pressure $\left(\sigma_{v}^{\prime}<\sigma_{h}^{\prime}\right)$
[Assuming principal stresses are vertical and horizontal]
Angle of shearing resistance:
At peak strength $\quad \phi^{\prime}{ }_{\text {max }}$
At large strain $\quad \phi^{\prime}$ crit $\quad$ (at critical state)
In any shear test on soil, failure occurs when $\phi^{\prime}$ reaches $\phi^{\prime}{ }_{\max }$, and

$$
\phi_{\max }^{\prime}=\phi_{\text {crit }}^{\prime}+\phi_{\text {dilatang }}^{\prime}
$$

where: $\phi^{\prime}$ crit is the ultimate angle of shearing resistance of a random aggregate deforming at constant volume, and $\phi^{\prime}$ dilatancy $\rightarrow 0$ as $I_{D} \rightarrow 0$, or $s^{\prime}$ becomes large.

Typical properties for a quartz sand;

$$
\phi_{c r i t}^{\prime}=33^{\circ} \quad, \quad \phi_{\max }^{\prime}=53^{\circ} \quad\left(I_{D}=1, s^{\prime}<150 \mathrm{kN} \mathrm{~m}^{-2}\right) .
$$

## 10. Design of reinforced concrete



Design compressive strength of concrete is based on the characteristic cylinder strength $f_{c k}$ :

$$
f_{c d}=\alpha_{c c} \frac{f_{c k}}{1.5}
$$

$\alpha_{c c}=0.85$ for compression in flexure and axial loading and $\alpha_{c c}=1.0$ for other phenomena
Design tensile strength of steel is based on the characteristic tensile yield stress of steel $f_{y k}$ :

$$
f_{y d}=\frac{f_{y k}}{1.15}
$$

### 10.1. Design Equations

At failure in bending, the stress in the concrete $=0.6 f_{c d}$ over the whole area of concrete in compression and the stress in the steel $=f_{y d}$.

Moment capacity of singly reinforced beam

$$
\begin{aligned}
& M=f_{y d} A_{s}\left(d-\frac{x}{2}\right) \\
& x=1.67 \frac{f_{y d}}{f_{c d}}\left(\frac{A_{s}}{b}\right) \quad(\leq 0.5 d \text { to avoid over reinforcement })
\end{aligned}
$$

Moment capacity of double reinforced beam (if compression reinforcement is yielding)

$$
M=0.6 f_{c d} b x\left(d-\frac{x}{2}\right)+A_{s}^{\prime} f_{y d}\left(d-d^{\prime}\right)
$$

## Shear capacity of beams

Shear capacity of unreinforced webs:

Where:

$$
\begin{aligned}
V_{R d, c}= & \frac{0.18}{\gamma_{c}}\left(k\left(100 \rho_{l} f_{c k}\right)^{\frac{1}{3}}\right) b_{w} d \\
& \geq 0.035 k^{3 / 2} f_{c k}^{1 / 2} b_{w} d
\end{aligned}
$$

$$
k=1+\sqrt{200 / d} \leq 2.0 \quad[d \mathrm{in} \mathrm{~mm}]
$$

$b_{w}$ is the width of the web and $\rho_{l}$ is the reinforcement ratio of the anchored steel:

$$
\rho_{l}=A_{s} /\left(b_{w} d\right) \leq 0.02
$$

If this resistance is insufficient to carry the applied load, internal stirrups are required, designed (assuming a 45 degrees truss angle) according to:

$$
\left.\begin{array}{ll}
V_{s}=\frac{A_{s w} f_{y d}(0.9 d)}{1.15 s} & \text { where } A_{s w} \text { is the area of the stirrup legs } \\
\text { and } s \text { is the stirrup spacing }
\end{array}\right] \begin{array}{ll} 
\\
V_{\max }=\frac{f_{c, \max }}{2}(0.9 b d) & \text { where } f_{c, \max }=0.4 f_{c k}\left(1-f_{c k} / 250\right)
\end{array}
$$

The shear resistance is controlled by the smaller of $V_{s}$ or $V_{\max }$.

### 10.2. Available steel types

| Deformed high yield steel | $f_{y k}=500 \mathrm{~N} \mathrm{~mm}^{-2}$ |
| :--- | :--- |
| Plain mild steel | $f_{y k}=250 \mathrm{~N} \mathrm{~mm}^{-2}$ |

### 10.3. Standard bar sizes and reinforcement areas per metre width

| Diameter (mm) | 6 | 8 | 10 | 12 | 16 | 20 | 25 | 32 | 40 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area ( $\mathbf{m m}^{\mathbf{2}}$ ) | 28 | 50 | 78 | 113 | 201 | 314 | 491 | 804 | 1256 |


|  | Spacing of bars (mm) |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ | $\mathbf{2 7 5}$ | $\mathbf{3 0 0}$ |
| Bar Dia. <br> (mm) |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6}$ | 377 | 283 | 226 | 189 | 162 | 142 | 126 | 113 | 103 | 94.3 |
| $\mathbf{8}$ | 671 | 503 | 402 | 335 | 287 | 252 | 224 | 201 | 183 | 168 |
| $\mathbf{1 0}$ | 1050 | 785 | 628 | 523 | 449 | 393 | 349 | 314 | 285 | 262 |
| $\mathbf{1 2}$ | 1510 | 1130 | 905 | 754 | 646 | 566 | 503 | 452 | 411 | 377 |
| $\mathbf{1 6}$ | 2680 | 2010 | 1610 | 1340 | 1150 | 1010 | 894 | 804 | 731 | 670 |
| $\mathbf{2 0}$ | 4190 | 3140 | 2510 | 2090 | 1800 | 1570 | 1400 | 1260 | 1140 | 1050 |
| $\mathbf{2 5}$ | 6550 | 4910 | 3930 | 3270 | 2810 | 2450 | 2180 | 1960 | 1790 | 1640 |
| $\mathbf{3 2}$ | 10700 | 8040 | 6430 | 5360 | 4600 | 4020 | 3570 | 3220 | 2920 | 2680 |
| $\mathbf{4 0}$ | 16800 | 12600 | 10100 | 8380 | 7180 | 6280 | 5580 | 5030 | 4570 | 4190 |

[^0]
## 11. Typical properties and forms of structural materials

The following selection of mechanical properties and sections is for teaching purposes only. When designing any structure, reference should be made to the relevant British or European Standard.

### 11.1. Mechanical properties of steel and aluminium

|  | Structural Steel |  | Aluminium |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Grade 43 <br> $($ BS EN - S275) | Grade 50 <br> (BS EN - S355) | Alloy <br> $6082-\mathrm{T} 6$ | Alloy <br> $5251-\mathrm{H} 24$ |
| Yield stress $\sigma_{y}$ <br> (MPa) | $275^{*}$ | $355^{*}$ | $255^{*}$ | $185^{*}$ |
| Typical form | Hot-rolled sections and plate | Extruded <br> sections, plate | Plate, sheet |  |

* Typical values


### 11.2. Mechanical properties of glass fibre reinforced plastic (GFRP)

Properties of GFRP can vary widely. One particular example is as follows:

| Glass fibre in Polyester Matrix |  |  |  |
| :---: | :---: | :---: | :---: |
| Fibreforce Composites Ltd - Force 800-Mat/roving |  |  |  |$|$| Longitudinal Tensile <br> Properties |  | In-plane <br> Shear <br> Modulus |
| :---: | :---: | :---: |
| Modulus | Breaking <br> Stress <br> SPa $)$ | Density <br> $\sigma_{t}(\mathrm{MPa})$ |
| 17.2 | 207 | 2.9 |

### 11.3. Structural steel sections (hot-rolled)

Pages 14-21 are reproduced and adapted from Steelwork Design Guide to BS5950: Part 1: 1990 - Volume 1, Section Properties and Member Capacities (5th Edition), by kind permission of the Director, The Steel Construction Institute, Ascot, Berkshire.


| Section Designation | $\begin{aligned} & \text { Mass } \\ & \text { Per } \\ & \text { Metre } \end{aligned}$ | Depth <br> Section | Width Of Section | Thickness |  | Second Moment Of Area |  | Radius Of Gyration |  | Elastic Modulus |  | Plastic Modulus |  | Torsional Constant | Area Of Section |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Web | Flange | $\begin{gathered} \text { Axis } \\ x-x \end{gathered}$ | $\begin{aligned} & \text { Axis } \\ & y-y \end{aligned}$ | $\underset{x-x}{\text { Axis }}$ | $\begin{aligned} & \text { Axis } \\ & y-y \end{aligned}$ | $\begin{gathered} \text { Axis } \\ x-x \end{gathered}$ | Axis y-y | $\begin{gathered} \text { Axis } \\ x-x \end{gathered}$ | Axis $y-y$ |  |  |
|  |  | $\underset{\mathrm{mm}}{\mathrm{D}}$ | $\begin{gathered} B \\ \mathrm{~mm} \end{gathered}$ | $\stackrel{t}{\mathbf{m m}}$ | $\begin{gathered} T \\ \mathrm{~mm} \end{gathered}$ |  |  | cm | cm | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\underset{\mathrm{cm}^{4}}{\mathrm{~J}}$ | $\underset{\mathrm{cm}^{2}}{\mathrm{~A}}$ |
| 914×419×388 | 388.0 | 921.0 | 420.5 | 21.4 | 36.6 | 719600 | 45440 | 38.2 | 9.59 | 15630 | 2161 | 17670 | 3341 | 1734 | $494$ |
| $914 \times 419 \times 388$ $914 \times 419 \times 343$ | 343.3 | 911.8 | 418.5 | 19.4 | 32.0 | 625800 | 39160 | 37.8 | 9.46 | 13730 | 1871 | 15480 | 2890 | 1193 | $437$ |
| 914×305×289 | 289.1 | 926.6 | 307.7 | 19.5 | 32.0 | 504200 | 15600 | 37.0 | 6.51 | 10880 | 1014 | 12570 | 1601 | 926 | 368 |
| $914 \times 305 \times 253$ | 253.4 | 918.4 | 305.5 | 17.3 | 27.9 | 436300 | 13300 | 36.8 | 6.42 | 9501 | 871 | 10940 | 1371 | 626 | 323 |
| $914 \times 305 \times 224$ | 224.2 | 910.4 | 304.1 | 15.9 | 23.9 | 376400 | 11240 | 36.3 | 6.27 | 8269 | 739 | 9535 | 1163 | 422 | 286 |
| 914x $305 \times 201$ | 200.9 | 903.0 | 303.3 | 15.1 | 20.2 | 325300 | 9423 | 35.7 | 6.07 | 7204 | 621 | 8351 | 98 | 29 | 256 |
| $838 \times 292 \times 226$ | 226.5 | 850.9 | 293.8 | 16.1 | 26.8 | 339700 | 11360 | 34.3 | 6.27 | 7985 | 773 | 9155 | 1212 | 514 | 289 |
| $838 \times 292 \times 194$ | 193.8 | 840.7 | 292.4 | 14.7 | 21.7 | 279200 | 9066 | 33.6 | 6.06 | 6641 | 620 | 7640 | 974 | 306 | 247 |
| $838 \times 292 \times 176$ | 175.9 | 834.9 | 291.7 | 14.0 | 18.8 | 246000 | 7799 | 33.1 | 5.90 | 5893 | 535 | 6808 | 842 | 1 | 4 |
| 762x267×197 | 196.8 | 769.8 | 268.0 | 15.6 | 25.4 | 240000 | 8175 | 30.9 | 5.71 | 6234 | 610 | 7167 | 959 | 404 | 251 |
| $762 \times 267 \times 173$ | 173.0 | 762.2 | 266.7 | 14.3 | 21.6 | 205300 | 6850 | 30.5 | 5.58 | 5387 | 514 | 6198 | 807 | 267 | 220 |
| $762 \times 267 \times 147$ | 146.9 | 754.0 | 265.2 | 12.8 | 17.5 | 168500 | 5455 | 30.0 | 5.40 | 4470 | 411 | 5156 | 647 | 159 | 7 |
| $762 \times 267 \times 134$ | 133.9 | 750.0 | 264.4 | 12.0 | 15.5 | 150700 | 4788 | 29.7 | 5.30 | 4018 | 36 | 46 | 570 | 9 | 171 |
| $686 \times 254 \times 170$ | 170.2 | 692.9 | 255.8 | 14.5 | 23.7 | 170300 | 6630 | 28.0 | 5.53 | 4916 | 518 | 5631 | 811 | 308 | 217 |
| $686 \times 254 \times 152$ | 152.4 | 687.5 | 254.5 | 13.2 | 21.0 | 150400 | 5784 | 27.8 | 5.46 | 4374 | 455 | 5000 | 710 | 220 | 194 |
| $686 \times 254 \times 140$ | 140.1 | 683.5 | 253.7 | 12.4 | 19.0 | 136300 | 5183 | 27.6 | 5.39 | 3987 | 409 | 4558 | 38 | 9 | 78 |
| $686 \times 254 \times 125$ | 125.2 | 677.9 | 253.0 | 11.7 | 16.2 | 118000 | 4383 | 27.2 | 5.24 | 3481 | 34 | 3994 | 54 | 116 | 159 |
| $610 \times 305 \times 238$ | 238.1 | 635.8 | 311.4 | 18.4 | 31.4 | 209500 | 15840 | 26.3 | 7.23 | 6589 | 1017 | 7486 | 1574 | 785 | 303 |
| $610 \times 305 \times 179$ | 179.0 | 620.2 | 307.1 | 14.1 | 23.6 | 153000 | 11410 | 25.9 | 7.07 | 4935 | 743 | 5547 | 1144 | 340 | 228 |
| $610 \times 305 \times 149$ | 149.2 | 612.4 | 304.8 | 11.8 | 19.7 | 125900 | 9308 | 25.7 | 7.00 | 4111 | 611 | 4594 | 93 | 200 | 190 |
| $610 \times 229 \times 140$ | 139.9 | 617.2 | 230.2 | 13.1 | 22.1 | 111800 | 4505 | 25.0 | 5.03 | 3622 | 391 | 4142 | 611 | 216 | 178 |
| $610 \times 229 \times 125$ | 125.1 | 612.2 | 229.0 | 11.9 | 19.6 | 98610 | 3932 | 24.9 | 4.97 | 3221 | 343 | 3676 | 469 | 111 | 159 |
| $610 \times 229 \times 113$ | 113.0 | 607.6 | 228.2 | 11.1 | 17.3 | 87320 75780 | 3434 2915 | 24.6 24.2 | 4.88 | 2874 2515 | 256 | 2881 | 400 | 77.0 | 129 |
| $610 \times 229 \times 101$ | 101.2 | 602.6 | 227.6 | 10.5 | 14.8 | 75780 | 2915 | 24.2 | 4.75 | 2515 | 256 | 2881 |  |  |  |
| $533 \times 210 \times 122$ | 122.0 | 544.5 | 211.9 | 12.7 | 21.3 | 76040 | 3388 | 22.1 | 4.67 | 2793 | 320 | 3196 | 500 | 178 | 155 139 |
| $533 \times 210 \times 109$ | 109.0 | 539.5 | 210.8 | 11.6 | 18.8 | 66820 | 2943 | 21.9 | 4.60 | 2477 | 279 | 2828 | 436 399 | 126 | 139 |
| $533 \times 210 \times 101$ | 101.0 | 536.7 | 210.0 | 10.8 | 17.4 | 61520 | 2692 | 21.9 | 4.57 | 2292 | 25 | 2360 | 35 | 75.7 | 129 |
| $533 \times 210 \times 92$ | 92.1 | 533.1 | 209.3 | 10.1 | 15.6 | 55230 47540 | 2389 2007 | 21.7 21.3 | 4.51 | 1800 | 192 | 2059 | 300 | 51.5 | 105 |
| $533 \times 210 \times 82$ | 82.2 | 528.3 | 208.8 | 9.6 | 13.2 | 47540 | 2007 | 21.3 | 4.38 | 1800 | 192 | 2059 | 300 | 51.5 | 105 |
| $457 \times 191 \times 98$ | 98.3 | 467.2 | 192.8 | 11.4 | 19.6 | 45730 | 2347 | 19.1 | 4.33 | 1957 | 243 | 2232 | 379 338 | 121 | 125 |
| $457 \times 191 \times 89$ | 89.3 | 463.4 | 191.9 | 10.5 | 17.7 | 41020 | 2089 | 19.0 | 4.29 | 1770 | 218 | 2014 | 338 | 90.7 | 114 |
| $457 \times 191 \times 82$ | 82.0 | 460.0 | 191.3 | 9.9 | 16.0 | 37050 | 1871 | 18.8 | 4.23 | 1611 | 19 | 16 | 272 | 51.8 | 104 94.6 |
| $457 \times 191 \times 74$ | 74.3 | 457.0 | 190.4 | 9.0 | 14.5 | 33320 29380 | 1671 1452 | 18.8 | 4.20 | 1296 | 153 | 1471 | 237 | 37.1 | 85.5 |
| $457 \times 191 \times 67$ | 67.1 | 453.4 | 189.9 | 8.5 | 12.7 | 29380 | 1452 | 18.5 | 4.12 | 1296 | 153 | 1471 | 237 | 37.1 | 85.5 |
| $457 \times 152 \times 82$ | 82.1 | 465.8 | 155.3 | 10.5 | 18.9 | 36590 | 1185 | 18.7 | 3.37 | 1571 | 153 | 1811 | 240 | 89.2 | $105$ |
| $457 \times 152 \times 74$ | 74.2 | 462.0 | 154.4 | 9.6 | 17.0 | 32670 | 1047 | 18.6 | 3.33 | 1414 | 136 | 1627 | 213 | 65.9 | 94.5 |
| $457 \times 152 \times 67$ | 67.2 | 458.0 | 153.8 | 9.0 | 15.0 | 28930 | 913 | 18.4 | 3.27 3.23 | 1263 | 119 | 1287 | 163 | 33.8 | 85.6 |
| $457 \times 152 \times 60$ | 59.8 | 454.6 | 152.9 | 8.1 | 13.3 | 25500 21370 | 795 645 | 18.3 17.9 | 3.23 3.11 | 1122 950 | 84.6 | 1096 | 133 | 21.4 | 66.6 |
| 457×152×52 | 52.3 | 449.8 | 152.4 | 7.6 | 10.9 | 21370 | 645 | 17.9 |  |  |  |  |  |  |  |

Note: In the Section Tables in 10.3 and 10.4, the torsional constant $J$ is defined by the equation $J=T /(G \phi)$ and will not be the polar second moment of area (unless the cross-section is circular).


UNIVERSAL BEAMS


| Section Designation | Mass <br> Per Metre <br> kg/m | Depth Of Section <br> D mm | Width Of Section <br> B mm | Thickness |  | Second Moment Of Area |  | Radius Of Gyration |  | Elastic Modulus |  | Plastic Modulus |  | Torsional Constant$\underset{\mathrm{cm}^{4}}{\mathrm{~J}}$ | Area Of Section$\underset{\mathrm{cm}^{2}}{\mathrm{~A}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Web | Flange | $\underset{x-x}{\text { Axis }}$ | $\begin{gathered} \text { Axis } \\ y-y \end{gathered}$ | Axis $x-x$ | Axis $y-y$ | Axis $x-x$ | Axis $y-y$ | Axis $x-x$ | $\begin{gathered} \text { Axis } \\ y-y \end{gathered}$ |  |  |
|  |  |  |  | $\begin{gathered} \mathbf{t} \\ \mathbf{m m} \end{gathered}$ | $\begin{gathered} T \\ \mathrm{~mm} \end{gathered}$ | cm ${ }^{4}$ | $\mathrm{cm}^{4}$ | cm | cm | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ |  |  |
| $406 \times 178 \times 74$ | 74.2 | 412.8 | 179.5 | 9.5 | 16.0 | 27310 | 1545 | 17.0 | 4.04 | 1323 | 172 | 1501 | 267 | 62.8 | 94.5 |
| $406 \times 178 \times 67$ | 67.1 | 409.4 | 178.8 | 8.8 | 14.3 | 24330 | 1365 | 16.9 | 3.99 | 1189 | 153 | 1346 | 237 | 46.1 | 85.5 |
| $406 \times 178 \times 60$ | 60.1 | 406.4 | 177.9 | 7.9 | 12.8 | 21600 | 1203 | 16.8 | 3.97 | 1063 | 135 | 1199 | 209 | 33.3 | 76.5 |
| $406 \times 178 \times 54$ | 54.1 | 402.6 | 177.7 | 7.7 | 10.9 | 18720 | 1021 | 16.5 | 3.85 | 930 | 115 | 1055 | 178 | 23.1 | 69.0 |
| $406 \times 140 \times 46$ | 46.0 | 403.2 | 142.2 | 6.8 | 11.2 | 15690 | 538 | 16.4 | 3.03 | 778 | 75.7 | 888 | 118 | 19.0 | 58.6 |
| $406 \times 140 \times 39$ | 39.0 | 398.0 | 141.8 | 6.4 | 8.6 | 12510 | 410 | 15.9 | 2.87 | 629 | 57.8 | 724 | 90.8 | 10.7 | 49.7 |
| $356 \times 171 \times 67$ | 67.1 | 363.4 | 173.2 | 9.1 | 15.7 | 19460 | 1362 | 15.1 | 3.99 | 1071 | 157 | 1211 | 243 | 55.7 | 85.5 |
| $356 \times 171 \times 57$ | 57.0 | 358.0 | 172.2 | 8.1 | 13.0 | 16040 | 1108 | 14.9 | 3.91 | 896 | 129 | 1010 | 199 | 33.4 | 72.6 |
| $356 \times 171 \times 51$ | 51.0 | 355.0 | 171.5 | 7.4 | 11.5 | 14140 | 968 | 14.8 | 3.86 | 796 | 113 | 896 | 174 | 23.8 | 64.9 |
| $356 \times 171 \times 45$ | 45.0 | 351.4 | 171.1 | 7.0 | 9.7 | 12070 | 811 | 14.5 | 3.76 | 687 | 94.8 | 775 | 147 | 15.8 | 57.3 |
| 356x127x39 | 39.1 | 353.4 | 126.0 | 6.6 | 10.7 | 10170 | 358 | 14.3 | 2.68 | 576 | 56.8 | 659 | 89.1 | 15.1 | 49.8 |
| $356 \times 127 \times 33$ | 33.1 | 349.0 | 125.4 | 6.0 | 8.5 | 8249 | 280 | 14.0 | 2.58 | 473 | 44.7 | 543 | 70.3 | 8.79 | 42.1 |
| $305 \times 165 \times 54$ | 54.0 | 310.4 | 166.9 | 7.9 | 13.7 | 11700 | 1063 | 13.0 | 3.93 | 754 | 127 | 846 | 196 | 34.8 | 68.8 |
| $305 \times 165 \times 46$ | 46.1 | 306.6 | 165.7 | 6.7 | 11.8 | 9899 | 896 | 13.0 | 3.90 | 646 | 108 | 720 | 166 | 22.2 | 58.7 |
| $305 \times 165 \times 40$ | 40.3 | 303.4 | 165.0 | 6.0 | 10.2 | 8503 | 764 | 12.9 | 3.86 | 560 | 92.6 | 623 | 142 | 14.7 | 51.3 |
| 305×127×48 | 48.1 | 311.0 | 125.3 | 9.0 | 14.0 | 9575 | 461 | 12.5 | 2.74 | 616 | 73.6 | 711 | 116 | 31.8 | 61.2 |
| $305 \times 127 \times 42$ | 41.9 | 307.2 | 124.3 | 8.0 | 12.1 | 8196 | 389 | 12.4 | 2.70 | 534 | 62.6 | 614 | 98.4 | 21.1 | 53.4 |
| $305 \times 127 \times 37$ | 37.0 | 304.4 | 123.4 | 7.1 | 10.7 | 7171 | 336 | 12.3 | 2.67 | 471 | 54.5 | 539 | 85.4 | 14.8 | 47.2 |
| 305x102x33 | 32.8 | 312.7 | 102.4 | 6.6 | 10.8 | 6501 | 194 | 12.5 | 2.15 | 416 | 37.9 | 481 | 60.0 | 12.2 | 41.8 |
| $305 \times 102 \times 28$ | 28.2 | 308.7 | 101.8 | 6.0 | 8.8 | 5366 | 155 | 12.2 | 2.08 | 348 | 30.5 | 403 | 48.5 | 7.40 4.77 | 31.8 31.6 |
| $305 \times 102 \times 25$ | 24.8 | 305.1 | 101.6 | 5.8 | 7.0 | 4455 | 123 | 11.9 | 1.97 | 292 | 24.2 | 342 | 38.8 | 4.77 | 31.6 |
| $254 \times 146 \times 43$ | 43.0 | 259.6 | 147.3 | 7.2 | 12.7 | 6544 | 677 | 10.9 | 3.52 | 504 | 92.0 | 566 | 141 | 23.9 | 54.8 |
| $254 \times 146 \times 37$ | 37.0 | 256.0 | 146.4 | 6.3 | 10.9 | 5537 | 571 | 10.8 | 3.48 | 433 | 78.0 | 483 | 119 | 15.3 | 47.2 |
| 254×146x31 | 31.1 | 251.4 | 146.1 | 6.0 | 8.6 | 4413 | 448 | 10.5 | 3.36 | 351 | 61.3 | 393 | 94.1 | 8.55 | 39.7 |
| 254×102×28 | 28.3 | 260.4 | 102.2 | 6.3 | 10.0 | 4005 | 179 | 10.5 | 2.22 | 308 | 34.9 | 353 | 54.8 | 9.57 | 36.1 |
| $254 \times 102 \times 25$ | 25.2 | 257.2 | 101.9 | 6.0 | 8.4 | 3415 | 149 | 10.3 | 2.15 | 266 | 29.2 | 306 | 46.0 | 6.42 | 32.0 |
| 254×102×22 | 22.0 | 254.0 | 101.6 | 5.7 | 6.8 | 2841 | 119 | 10.1 | 2.06 | 224 | 23.5 | 259 | 37.3 | 4.15 | 28.0 |
| $203 \times 133 \times 30$ | 30.0 | 206.8 | 133.9 | 6.4 | 9.6 | 2896 | 385 | 8.71 | 3.17 | 280 | 57.5 | 314 | 88.2 | 10.3 | 38.2 |
| $203 \times 133 \times 25$ | 25.1 | 203.2 | 133.2 | 5.7 | 7.8 | 2340 | 308 | 8.56 | 3.10 | 230 | 46.2 | 258 | 70.9 | 5.96 | 32.0 |
| $203 \times 102 \times 23$ | 23.1 | 203.2 | 101.8 | 5.4 | 9.3 | 2105 | 164 | 8.46 | 2.36 | 207 | 32.2 | 234 | 49.8 | 7.02 | 29.4 |
| $178 \times 102 \times 19$ | 19.0 | 177.8 | 101.2 | 4.8 | 7.9 | 1356 | 137 | 7.48 | 2.37 | 153 | 27.0 | 171 | 41.6 | 4.41 | 24.3 |
| 152x89x16 | 16.0 | 152.4 | 88.7 | 4.5 | 7.7 | 834 | 89.8 | 6.41 | 2.10 | 109 | 20.2 | 123 | 31.2 | 3.56 | 20.3 |
| 127×76x13 | 13.0 | 127.0 | 76.0 | 4.0 | 7.6 | 473 | 55.7 | 5.35 | 1.84 | 74.6 | 14.7 | 84.2 | 22.6 | 2.85 | 16.5 |



| Section Designation | Mass Per Metre | Depth Of <br> Section | Width Of Section | Thickness |  | Second Moment Of Area |  | Radius Of Gyration |  | Elastic <br> Modulus |  | Plastic Modulus |  | Torsional Constant | Area Of Section |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Web | Flange | $\underset{x-x}{\text { Axis }}$ | $\begin{aligned} & \text { Axis } \\ & y-y \end{aligned}$ | $\underset{x-x}{\text { Axis }}$ | $\begin{aligned} & \text { Axis } \\ & y-y \end{aligned}$ | $\begin{aligned} & \text { Axis } \\ & x-x \end{aligned}$ | $\begin{gathered} \text { Axis } \\ y-y \end{gathered}$ | Axis $x-x$ | Axis $y-y$ |  |  |
|  |  | $\underset{\mathrm{mm}}{\mathrm{D}}$ | $\underset{\mathrm{mm}}{\mathbf{B}}$ | $\begin{gathered} \mathbf{t} \\ \mathrm{mm} \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \mathrm{~mm} \end{gathered}$ | $\mathrm{cm}^{4}$ |  |  |  | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\mathrm{cm}^{3}$ | $\underset{\mathrm{cm}^{4}}{\mathrm{~J}}$ | $\underset{\mathrm{cm}^{2}}{\mathrm{~A}}$ |
|  | 633.9 | 474.6 | 424.0 | 47.6 | 77.0 | 274800 | 98130 | 18.4 | 11.0 | 11580 | 4629 | 14240 | 7108 | 13720 | 808 |
| $356 \times 406 \times 634$ $356 \times 406 \times 551$ | 633.9 551.0 | 474.6 455.6 | 424.0 418.5 | 47.6 | 67.5 | 226900 | 82670 | 18.0 | 10.9 | 9962 | 3951 | 12080 | 6058 | 9240 | 702 |
| $356 \times 406 \times 551$ $356 \times 406 \times 467$ | 467.0 | 436.6 | 418.5 412.2 | 42.1 35.8 | 58.0 | 183000 | 67830 | 17.5 | 10.7 | 8383 | 3291 | 10000 | 5034 | 5809 | 595 |
| $356 \times 406 \times 467$ $356 \times 406 \times 393$ | 393.0 | 419.0 | 407.0 | 30.6 | 49.2 | 146600 | 55370 | 17.1 | 10.5 | 6998 | 2721 | 8222 | 4154 | 3545 | 501 |
| $356 \times 406 \times 340$ | 339.9 | 406.4 | 403.0 | 26.6 | 42.9 | 122500 | 46850 | 16.8 | 10.4 | 6031 | 2325 | 6999 | 4 | 234 | 3 |
| $356 \times 406 \times 287$ | 287.1 | 393.6 | 399.0 | 22.6 | 36.5 | 99880 | 38680 | 16.5 | 10.3 | 5075 | 1939 | 12 | 949 | 144 | 6 |
| $356 \times 406 \times 235$ | 235.1 | 381.0 | 394.8 | 18.4 | 30.2 | 79080 | 30990 | 16.3 | 10.2 | 4151 | 70 | 4687 | 3 | 812 | 299 |
| $356 \times 368 \times 202$ | 201.9 | 374.6 | 374.7 | 16.5 | 27.0 | 66260 | 23690 | 16.1 | 9.60 | 3538 | 1264 | 3972 | 1920 | 558 | 257 |
| $356 \times 368 \times 177$ | 177.0 | 374.6 368.2 | 372.6 | 14.4 | 23.8 | 57120 | 20530 | 15.9 | 9.54 | 3103 | 1102 | 3455 | 1671 | 381 | 226 |
| $356 \times 368 \times 153$ | 152.9 | 362.0 | 370.5 | 12.3 | 20.7 | 48590 | 17550 | 15.8 | 9.49 | 2684 | 948 | 2965 | 1435 | 251 | 5 |
| $356 \times 368 \times 129$ | 129.0 | 355.6 | 368.6 | 10.4 | 17.5 | 40250 | 14610 | 15.6 | 9.43 | 2264 | 793 | 2479 | 9 | 153 | 4 |
| $305 \times 305 \times 283$ | 282.9 | 365.3 | 322.2 | 26.8 | 44.1 | 78870 | 24630 | 14.8 | 8.27 | 4318 | 1529 | 5105 | 2342 | 2034 | 360 |
| $305 \times 305 \times 240$ | 240.0 | 352.5 | 318.4 | 23.0 | 37.7 | 64200 | 20310 | 14.5 | 8.15 | 3643 | 1276 | 4247 | 1951 | 1271 | 306 |
| $305 \times 305 \times 198$ | 198.1 | 339.9 | 314.5 | 19.1 | 31.4 | 50900 | 16300 | 14.2 | 8.04 | 2995 | 1037 | 3440 | 1581 | 734 | 252 |
| $305 \times 305 \times 158$ | 158.1 | 327.1 | 311.2 | 15.8 | 25.0 | 38750 | 12570 | 13.9 | 7.90 | 2369 | 808 | 268 | 1053 | 49 | 174 |
| $305 \times 305 \times 137$ | 136.9 | 320.5 | 309.2 | 13.8 | 21.7 | 32810 | 10700 | 13.7 | 7.83 | 2048 | 692 | 2 |  | 16 | 150 |
| $305 \times 305 \times 118$ | 117.9 | 314.5 | 307.4 | 12.0 | 18.7 | 27670 | 9059 | 13.6 | 7.77 7.69 | 1760 | 479 | 1592 | 726 | 91.2 | 123 |
| $305 \times 305 \times 97$ | 96.9 | 307.9 | 305.3 | 9.9 | 15.4 | 22250 | 7308 | 13.4 | 7.69 | 1445 | 479 | 1592 | 726 | 91.2 |  |
| 254×254x167 | 167.1 | 289.1 | 265.2 | 19.2 | 31.7 | 30000 | 9870 | 11.9 | 6.81 | 2075 | 744 | 2424 | 1137 878 | 626 | 213 |
| 254×254×132 | 132.0 | 276.3 | 261.3 | 15.3 | 25.3 | 22530 | 7531 | 11.6 | 6.69 | 1631 | 576 | 1869 | 878 | 319 | 168 |
| $254 \times 254 \times 107$ | 107.1 | 266.7 | 258.8 | 12.8 | 20.5 | 17510 | 5928 | 11.3 | 6.59 | 1313 | 458 | 1484 | 697 | 172 | 136 |
| 254×254×89 | 88.9 | 260.3 | 256.3 | 10.3 | 17.3 | 14270 | 4857 | 11.2 | 6.55 | 1096 | 379 | 1224 | 575 | 102 | 113 93.1 |
| 254×254×73 | 73.1 | 254.1 | 254.6 | 8.6 | 14.2 | 11410 | 3908 | 11.1 | 6.48 | 898 | 307 | 992 | 465 | 57.6 | 93.1 |
| $203 \times 203 \times 86$ | 86.1 | 222.2 | 209.1 | 12.7 | 20.5 | 9449 | 3127 | 9.28 | 5.34 | 850 | 299 | 977 | 456 | 137 | 110 |
| $203 \times 203 \times 71$ | 71.0 | 215.8 | 206.4 | 10.0 | 17.3 | 7618 | 2537 | 9.18 | 5.30 | 706 | 246 | 799 | 374 | 80.2 | 90.4 |
| $203 \times 203 \times 60$ | 60.0 | 209.6 | 205.8 | 9.4 | 14.2 | 6125 | 2065 | 8.96 | 5.20 | 584 | 201 | 656 | 305 | 47.2 31.8 | 66.4 |
| $203 \times 203 \times 52$ | 52.0 | 206.2 | 204.3 | 7.9 | 12.5 | 5259 | 1778 | 8.91 | 5.18 5.13 | 510 450 | 174 152 | 567 497 | 264 | 31.8 22.2 | 58.7 |
| $203 \times 203 \times 46$ | 46.1 | 203.2 | 203.6 | 7.2 | 11.0 | 4568 | 1548 | 8.82 | 5.13 | 450 | 152 | 497 | 231 |  |  |
| 152×152×37 | 37.0 | 161.8 | 154.4 | 8.0 | 11.5 | 2210 | 706 | 6.85 | 3.87 | 273 | 91.5 | 309 | 140 | 19.2 | 47.1 |
| $152 \times 152 \times 30$ | 30.0 | 157.6 | 152.9 | 6.5 | 9.4 | 1748 | 560 | 6.76 | 3.83 | 222 | 73.3 | 248 | 112 | 10.5 | 38.3 29.2 |
| $152 \times 152 \times 23$ | 23.0 | 152.4 | 152.2 | 5.8 | 6.8 | 1250 | 400 | 6.54 | 3.70 | 164 | 52.6 | 182 | 80.2 | 4.63 | 29.2 |



| Designation |  | Depth Of Section D mm | Width Of Section B mm | Thickness |  | Second Moment Of Area |  | Radius Of Gyration |  | Elastic <br> Modulus |  | Plastic <br> Modulus |  | Torsional Constant$\underset{\mathrm{cm}}{ }{ }^{\mathrm{J}}$ | Area of Section$\underset{\mathrm{cm}^{2}}{\mathrm{~A}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal | Mass |  |  | Web$\begin{gathered} \mathrm{t} \\ \mathrm{~mm} \end{gathered}$ | Flange <br> T mm |  |  |  |  |  |  |  |  |
| Size <br> mm | Per <br> Metre kg |  |  |  |  | $\begin{gathered} \hline \text { Axis } \\ \mathrm{x}-\mathrm{x} \\ \mathrm{~cm}^{4} \\ \hline \end{gathered}$ | Axis $y-y$ $\mathrm{cm}^{4}$ |  |  | Axis x-x cm | $\begin{aligned} & \text { Axis } \\ & y-y \\ & c m \end{aligned}$ | $\begin{gathered} \text { Axis } \\ x-x \\ \mathrm{~cm}^{3} \end{gathered}$ | $\begin{aligned} & \text { Axis } \\ & y-y \\ & \mathrm{~cm}^{3} \end{aligned}$ |  |  | $\begin{aligned} & \text { Axis } \\ & x-x \\ & \mathrm{~cm}^{3} \end{aligned}$ | Axis $y-y_{3}$ $\mathrm{cm}^{3}$ |
| $432 \times 102$ | 65.54 | 431.8 | 101.6 | 12.2 | 16.8 | 21370 | 627 | 16.0 | 2.74 | 990 | 79.9 | 1205 | 153 | 61.5 | 83.4 |
| 381x102 | 55.10 | 381.0 | 101.6 | 10.4 | 16.3 | 14870 | 579 | 14.6 | 2.87 | 781 | 75.7 | 931 | 144 | 46.4 | 70.1 |
| $305 \times 102$ | 46.18 | 304.8 | 101.6 | 10.2 | 14.8 | 8208 | 499 | 11.8 | 2.91 | 539 | 66.5 | 638 | 128 | 35.9 | 58.9 |
| 305x89 | 41.69 | 304.8 | 88.9 | 10.2 | 13.7 | 7078 | 326 | 11.5 | 2.47 | 464 | 48.6 | 559 | 92.9 | 28.1 | 53.3 |
| 254x89 | 35.74 | 254.0 | 88.9 | 9.1 | 13.6 | 4445 | 302 | 9.89 | 2.58 | 350 | 46.7 | 414 | 89.6 | 23.2 | 45.4 |
| 254x76 | 28.29 | 254.0 | 76.2 | 8.1 | 10.9 | 3355 | 162 | 9.67 | 2.12 | 264 | 28.1 | 316 | 53.9 | 12.3 | 35.9 |
| 229x89 | 32.76 | 228.6 | 88.9 | 8.6 | 13.3 | 3383 | 285 | 9.01 | 2.61 | 296 | 44.8 | 348 | 86.3 | 20.6 | 41.6 |
| 229x76 | 26.06 | 228.6 | 76.2 | 7.6 | 11.2 | 2615 | 159 | 8.87 | 2.19 | 229 | 28.3 | 271 | 54.5 | 11.6 | 33.2 |
| 203x89 | 29.78 | 203.2 | 88.9 | 8.1 | 12.9 | 2492 | 265 | 8.11 | 2.64 | 245 | 42.4 | 287 | 81.7 | 18.1 | 37.9 |
| 203x76 | 23.82 | 203.2 | 76.2 | 7.1 | 11.2 | 1955 | 152 | 8.02 | 2.24 | 192 | 27.7 | 226 | 53.5 | 10.6 | 30.4 |
| 178x89 | 26.81 | 177.8 | 88.9 | 7.6 | 12.3 | 1753 | 241 | 7.17 | 2.66 | 197 | 39.3 | 230 | 75.4 | 15.3 | 34.1 |
| 178x76 | 20.84 | 177.8 | 76.2 | 6.6 | 10.3 | 1338 | 134 | 7.10 | 2.25 | 151 | 24.8 | 176 | 48.1 | 8.26 | 26.6 |
| 152x89 | 23.84 | 152.4 | 88.9 | 7.1 | 11.6 | 1168 | 216 | 6.20 | 2.66 | 153 | 35.8 | 178 | 68.3 | 12.7 | 30.4 |
| 152x76 | 17.88 | 152.4 | 76.2 | 6.4 | 9.0 | 852 | 114 | 6.11 | 2.23 | 112 | 21.0 | 130 | 41.2 | 6.05 | 22.8 |
| 127x64 | 14.90 | 127.0 | 63.5 | 6.4 | 9.2 | 482 | 67.2 | 5.04 | 1.88 | 76.0 | 15.2 | 89.4 | 29.3 | 5.00 | 19.0 |
| $102 \times 51$ | 10.42 | 101.6 | 50.8 | 6.1 | 7.6 | 207 | 29.0 | 3.95 | 1.48 | 40.8 | 8.14 | 48.7 | 15.7 | 2.58 | 13.3 |
| 76x38 | 6.70 | 76.2 | 38.1 | 5.1 | 6.8 | 74.3 | 10.7 | 2.95 | 1.12 | 19.5 | 4.09 | 23.5 | 7.78 | 1.26 | 8.56 |



EQUAL ANGLES

DIMENSIONS AND PROPERTIES


| Designation |  | Mass Per Metre kg | Radius |  | Area Of Section $\mathrm{cm}^{2}$ | Distance Of Centre Of Gravity cx and cy cm | Second Moment Of Area |  |  | Radius Of Gyration |  |  | Elastic <br> Modulus <br> Axis <br> $x-x, y-y$ <br> $\mathrm{cm}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size <br> A A mm | Thickness <br> t mm |  | $\begin{gathered} \text { Root } \\ \mathrm{r} 1 \\ \mathrm{~mm} \end{gathered}$ | Toe <br> r 2 mm |  |  | $\begin{gathered} \text { Axis } \\ x-x, y-y \\ \mathrm{~cm}^{4} \end{gathered}$ | $\begin{aligned} & \text { Axis } \\ & \mathrm{u}-\mathrm{u} \\ & \mathrm{~cm}^{4} \end{aligned}$ | Axis v-v $\mathrm{cm}^{4}$ | $\begin{aligned} & \text { Axis } \\ & x-x, y-y \\ & \mathrm{~cm} \end{aligned}$ | Axis u-u cm | Axis $\mathrm{v}-\mathrm{v}$ cm |  |
| $250 \times 250$ | 35 | 128 | 20.0 | 4.8 | 164 | 7.51 | 9305 | 14720 | 3886 | 7.54 | 9.49 | 4.88 | 532 |
|  | 32 | 118 | 20.0 | 4.8 | 151 | 7.40 | 8650 | 13710 | 3592 | 7.58 | 9.54 | 4.89 | 491 |
|  | 28 | 104 | 20.0 | 4.8 | 133 | 7.25 | 7741 | 12290 | 3194 | 7.63 | 9.61 | 4.90 | 436 |
|  | 25 | 93.6 | 20.0 | 4.8 | 120 | 7.14 | 7030 | 11170 | 2890 | 7.67 | 9.67 | 4.92 | 394 |
| $200 \times 200$ | 24 | 71.1 | 18.0 | 4.8 | 90.8 | 5.85 | 3356 | 5322 | 1391 | 6.08 | 7.65 | 3.91 | 237 |
|  | 20 | 59.9 | 18.0 | 4.8 | 76.6 | 5.70 | 2877 | 4569 | 1185 | 6.13 | 7.72 | 3.93 | 201 |
|  | 18 | 54.2 | 18.0 | 4.8 | 69.4 | 5.62 | 2627 | 4174 | 1080 | 6.15 | 7.76 | 3.95 | 183 |
|  | 16 | 48.5 | 18.0 | 4.8 | 62.0 | 5.54 | 2369 | 3765 | 973 | 6.18 | 7.79 | 3.96 | 164 |
| 150x150 | 18 | 40.1 | 16.0 | 4.8 | 51.2 | 4.38 | 1060 | 1680 | 440 | 4.55 | 5.73 | 2.93 | 99.8 |
|  | 15 | 33.8 | 16.0 | 4.8 | 43.2 | 4.26 | 909 | 1442 | 375 | 4.59 | 5.78 | 2.95 | 84.6 |
|  | 12 | 27.3 | 16.0 | 4.8 | 35.0 | 4.14 | 748 | 1187 | 308 | 4.62 | 5.82 | 2.97 | 68.9 |
|  | 10 | 23.0 | 16.0 | 4.8 | 29.5 | 4.06 | 635 | 1008 | 262 | 4.64 | 5.85 | 2.99 | 58.0 |
| 120x120 | 15 | 26.6 | 13.0 | 4.8 | 34.0 | 3.52 | 448 | 710 | 186 | 3.63 | 4.57 | 2.34 | 52.8 |
|  | 12 | 21.6 | 13.0 | 4.8 | 27.6 | 3.41 | 371 | 589 | 153 | 3.66 | 4.62 | 2.35 | 43.1 |
|  | 10 | 18.2 | 13.0 | 4.8 | 23.3 | 3.32 | 316 | 502 | 130 | 3.69 | 4.65 | 2.37 | 36.4 |
|  | 8 | 14.7 | 13.0 | 4.8 | 18.8 | 3.24 | 259 | 411 | 107 | 3.71 | 4.67 | 2.38 | 29.5 |
| $100 \times 100$ | 15 | 21.9 | 12.0 | 4.8 | 28.0 | 3.02 | 250 | 395 | 105 | 2.99 | 3.76 | 1.94 | 35.8 |
|  | 12 | 17.8 | 12.0 | 4.8 | 22.8 | 2.91 | 208 | 330 | 86.5 | 3.02 | 3.81 | 1.95 | 29.4 |
|  | 10+ | 15.0 | 12.0 | 4.8 | 19.2 | 2.83 | 178 | 283 | 73.7 | 3.05 | 3.84 | 1.96 | 24.8 |
|  | 8 | 12.2 | 12.0 | 4.8 | 15.6 | 2.75 | 146 | 232 | 60.5 | 3.07 | 3.86 | 1.97 | 20.2 |
| $90 \times 90$ | 12 | 15.9 | 11.0 | 4.8 | 20.3 | 2.66 | 149 | 235 | 62.0 | 2.70 | 3.40 | 1.75 | 23.5 |
|  | 10 | 13.4 | 11.0 | 4.8 | 17.2 | 2.58 | 128 | 202 | 52.9 | 2.73 | 3.43 | 1.76 | 19.9 |
|  | 8 | 10.9 | 11.0 | 4.8 | 13.9 | 2.50 | 105 | 167 | 43.4 | 2.75 | 3.46 | 1.77 | 16.2 |
|  | 7 | 9.61 | 11.0 | 4.8 | 12.3 | 2.46 | 93.2 | 148 | 38.6 | 2.76 | 3.47 | 1.77 | 14.3 |
|  | 6 | 8.30 | 11.0 | 4.8 | 10.6 | 2.41 | 81.0 | 128 | 33.6 | 2.76 | 3.48 | 1.78 | 12.3 |
| 80x80 | 10 | 11.9 | 10.0 | 4.8 | 15.1 | 2.34 | 87.6 | 139 | 36.4 | 2.41 | 3.03 | 1.55 | 15.5 |
|  | 8 | 9.63 | 10.0 | 4.8 | 12.3 | 2.26 | 72.4 | 115 | 29.9 | 2.43 | 3.06 | 1.56 | 12.6 |
|  | 6 | 7.34 | 10.0 | 4.8 | 9.36 | 2.17 | 56.0 | 88.7 | 23.2 | 2.45 | 3.08 | 1.57 | 9.60 |
| 70x70 | 10 | 10.3 | 9.0 | 2.4 | 13.1 | 2.10 | 58.0 | 91.6 | 24.4 | 2.10 | 2.64 | 1.36 | 11.8 |
|  | 8 | 8.36 | 9.0 | 2.4 | 10.7 | 2.02 | 48.3 | 76.5 | 20.1 | 2.12 | 2.67 | 1.37 | 9.70 |
|  | 6 | 6.38 | 9.0 | 2.4 | 8.19 | 1.94 | 37.7 | 59.8 | 15.6 | 2.15 | 2.70 | 1.38 | 7.45 |
| 60x60 | 10 | 8.69 | 8.0 | 2.4 | 11.1 | 1.85 | 35.3 | 55.6 | 15.0 | 1.78 | 2.24 | 1.16 | 8.51 |
|  | 8 | 7.09 | 8.0 | 2.4 | 9.07 | 1.78 | 29.6 | 46.7 | 12.4 | 1.80 | 2.27 | 1.17 | 7.00 |
|  | 6 | 5.42 | 8.0 | 2.4 | 6.95 | 1.70 | 23.2 | 36.8 | 9.64 | 1.83 | 2.30 | 1.18 | 5.39 |
|  | 5 | 4.57 | 8.0 | 2.4 | 5.86 | 1.65 | 19.8 | 31.4 | 8.23 | 1.84 | 2.31 | 1.18 | 4.56 |
| 50x50 | 8 | 5.82 | 7.0 | 2.4 | 7.44 | 1.53 | 16.5 | 25.9 | 6.96 | 1.49 | 1.87 | 0.968 | 4.74 |
|  | 6 | 4.47 | 7.0 | 2.4 | 5.72 | 1.45 | 13.0 | 20.6 | 5.43 | 1.51 | 1.90 | 0.974 | 3.67 |
|  | 5 | 3.77 | 7.0 | 2.4 | 4.83 | 1.41 | 11.1 | 17.7 | 4.63 | 1.52 | 1.91 | 0.979 | 3.11 |
|  | 4 | 3.06 | 7.0 | 2.4 | 3.92 | 1.37 | 9.16 | 14.5 | 3.82 | 1.53 | 1.92 | 0.987 | 2.52 |
|  | 3 | 2.33 | 7.0 | 2.4 | 2.99 | 1.32 | 7.06 | 11.1 | 2.97 | 1.54 | 1.93 | 0.996 | 1.92 |
| $45 \times 45$ | 6 | 4.00 | 7.0 | 2.4 | 5.12 | 1.33 | 9.30 | 14.7 | 3.90 | 1.35 | 1.69 | 0.872 | 2.93 |
|  | 5 | 3.38 | 7.0 | 2.4 | 4.33 | 1.29 | 7.99 | 12.6 | 3.33 | 1.36 | 1.71 | 0.877 | 2.49 |
|  | 4 | 2.74 | 7.0 | 2.4 | 3.52 | 1.24 | 6.58 | 10.4 | 2.75 | 1.37 | 1.72 | 0.883 | 2.02 |
|  | 3 | 2.09 | 7.0 | 2.4 | 2.69 | 1.20 | 5.08 | 8.03 | 2.14 | 1.37 | 1.73 | 0.892 | 1.54 |
| $40 \times 40$ | 6 | 3.52 | 6.0 | 2.4 | 4.49 | 1.20 | 6.37 | 10.1 | 2.68 | 1.19 | 1.50 | 0.773 | 2.28 |
|  | 5 | 2.97 | 6.0 | 2.4 | 3.80 | 1.17 | 5.48 | 8.68 | 2.29 | 1.20 | 1.51 | 0.776 | 1.93 |
|  | 4 | 2.42 | 6.0 | 2.4 | 3.09 | 1.12 | 4.53 | 7.18 | 1.89 | 1.21 | 1.52 | 0.781 | 1.58 |
|  | 3 | 1.84 | 6.0 | 2.4 | 2.36 | 1.08 | 3.51 | 5.55 | 1.47 | 1.22 | 1.53 | 0.788 | 1.20 |
| 30x30 | 5 | 2.18 | 5.0 | 2.4 | 2.78 | 0.919 | 2.17 | 3.42 | 0.919 | 0.883 | 1.11 | 0.575 | 1.04 |
|  | 4 | 1.78 | 5.0 | 2.4 | 2.27 | 0.879 | 1.81 | 2.86 | 0.756 | 0.893 | 1.12 | 0.577 | 0.852 |
|  | 3 | 1.36 | 5.0 | 2.4 | 1.74 | 0.836 | 1.41 | 2.23 | 0.588 | 0.900 | 1.13 | 0.581 | 0.652 |
| $25 \times 25$ | 5 | 1.77 | 3.5 | 2.4 | 2.25 | 0.796 | 1.19 | 1.87 | 0.515 | 0.728 | 0.912 | 0.478 | 0.701 |
|  | 4 | 1.45 | 3.5 | 2.4 | 1.84 | 0.758 | 1.00 | 1.58 | 0.421 | 0.737 | 0.926 | 0.478 | 0.574 |
|  | 3 | 1.11 | 3.5 | 2.4 | 1.41 | 0.718 | 0.784 | 1.24 | 0.325 | 0.745 | 0.939 | 0.480 | 0:440 |


y

DIMENSIONS AND PROPERTIES

| Designation |  | Mass <br> per <br> Metre <br> kg | Area of Section A $\mathrm{cm}^{2}$ | Ratio <br> for <br> Local <br> Buckling <br> $D / t$ | Second Moment <br> of Area <br> 1 <br> $\mathrm{~cm}^{4}$ | Radius <br> of Gyration <br> r <br> cm | Elastic Modulus$\underset{\mathrm{cm}^{3}}{\mathrm{Z}}$ | Plastic Modulus$\begin{gathered} \mathrm{S} \\ \mathrm{~cm}^{3} \end{gathered}$ | Torsional Constants |  | Surface <br> Area <br> per <br> Metre <br> $\mathrm{m}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Outside | Thickness |  |  |  |  |  |  |  |  |  |  |
| D $\mathrm{mm}$ | $\begin{gathered} \mathrm{t} \\ \mathrm{~mm} \end{gathered}$ |  |  |  |  |  |  |  | $\begin{gathered} \mathrm{J} \\ \mathrm{~cm} \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ \mathrm{~cm}^{3} \end{gathered}$ |  |
| 21.3 | $3.2 \Delta$ | 1.43 | 1.82 | 6.66 | 0.768 | 0.650 | 0.722 | 1.06 | 1.54 | 1.44 | 0.0669 |
| 26.9 | $3.2 \Delta$ | 1.87 | 2.38 | 8.41 | 1.70 | 0.846 | 1.27 | 1.81 | 3.41 | 2.53 | 0.0845 |
| 33.7 | $\begin{aligned} & 2.6 \Delta \\ & 3.2 \Delta \\ & 4.0 \Delta \end{aligned}$ | $\begin{aligned} & 1.99 \\ & 2.41 \\ & 2.93 \end{aligned}$ | $\begin{aligned} & 2.54 \\ & 3.07 \\ & 3.73 \end{aligned}$ | $\begin{aligned} & 13.0 \\ & 10.5 \\ & 8.43 \end{aligned}$ | $\begin{aligned} & 3.09 \\ & 3.60 \\ & 4.19 \end{aligned}$ | $\begin{aligned} & 1.10 \\ & 1.08 \\ & 1.06 \end{aligned}$ | $\begin{aligned} & 1.84 \\ & 2.14 \\ & 2.49 \end{aligned}$ | $\begin{aligned} & 2.52 \\ & 2.99 \\ & 3.55 \end{aligned}$ | $\begin{aligned} & 6.19 \\ & 7.21 \\ & 8.38 \end{aligned}$ | $\begin{aligned} & 3.67 \\ & 4.28 \\ & 4.97 \end{aligned}$ | $\begin{aligned} & 0.106 \\ & 0.106 \\ & 0.106 \end{aligned}$ |
| 42.4 | $\begin{aligned} & 2.6 \Delta \\ & 3.2 \Delta \\ & 4.0 \Delta \end{aligned}$ | $\begin{aligned} & 2.55 \\ & 3.09 \\ & 3.79 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.94 \\ & 4.83 \end{aligned}$ | $\begin{aligned} & 16.3 \\ & 13.3 \\ & 10.6 \end{aligned}$ | $\begin{aligned} & 6.46 \\ & 7.62 \\ & 8.99 \end{aligned}$ | $\begin{aligned} & 1.41 \\ & 1.39 \\ & 1.36 \end{aligned}$ | $\begin{aligned} & 3.05 \\ & 3.59 \\ & 4.24 \end{aligned}$ | $\begin{aligned} & 4.12 \\ & 4.93 \\ & 5.92 \end{aligned}$ | $\begin{aligned} & 12.9 \\ & 15.2 \\ & 18.0 \end{aligned}$ | $\begin{aligned} & 6.10 \\ & 7.19 \\ & 8.48 \end{aligned}$ | $\begin{aligned} & 0.133 \\ & 0.133 \\ & 0.133 \end{aligned}$ |
| 48.3 | $\begin{aligned} & 3.2 \\ & 4.0 \\ & 5.0 \end{aligned}$ | $\begin{aligned} & 3.56 \\ & 4.37 \\ & 5.34 \end{aligned}$ | $\begin{aligned} & 4.53 \\ & 5.57 \\ & 6.80 \end{aligned}$ | $\begin{aligned} & 15.1 \\ & 12.1 \\ & 9.66 \end{aligned}$ | $\begin{aligned} & 11.6 \\ & 13.8 \\ & 16.2 \end{aligned}$ | $\begin{aligned} & 1.60 \\ & 1.57 \\ & 1.54 \end{aligned}$ | $\begin{aligned} & 4.80 \\ & 5.70 \\ & 6.69 \end{aligned}$ | $\begin{aligned} & 6.52 \\ & 7.87 \\ & 9.42 \end{aligned}$ | $\begin{aligned} & 23.2 \\ & 27.5 \\ & 32.3 \end{aligned}$ | $\begin{aligned} & 9.59 \\ & 11.4 \\ & 13.4 \end{aligned}$ | $\begin{aligned} & 0.152 \\ & 0.152 \\ & 0.152 \end{aligned}$ |
| 60.3 | $\begin{aligned} & \hline 3.2 \\ & 4.0 \\ & 5.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.51 \\ & 5.55 \\ & 6.82 \end{aligned}$ | $\begin{aligned} & 5.74 \\ & 7.07 \\ & 8.69 \end{aligned}$ | $\begin{aligned} & 18.8 \\ & 15.1 \\ & 12.1 \end{aligned}$ | $\begin{aligned} & 23.5 \\ & 28.2 \\ & 33.5 \end{aligned}$ | $\begin{aligned} & 2.02 \\ & 2.00 \\ & 1.96 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 7.78 \\ & 9.34 \\ & 11.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10.4 \\ & 12.7 \\ & 15.3 \end{aligned}$ | $\begin{aligned} & 46.9 \\ & 56.3 \\ & 67.0 \end{aligned}$ | $\begin{aligned} & 15.6 \\ & 18.7 \\ & 22.2 \end{aligned}$ | $\begin{aligned} & 0.189 \\ & 0.189 \\ & 0.189 \\ & \hline \end{aligned}$ |
| 76.1 | $\begin{aligned} & 3.2 \\ & 4.0 \\ & 5.0 \end{aligned}$ | $\begin{aligned} & 5.75 \\ & 7.11 \\ & 8.77 \end{aligned}$ | $\begin{aligned} & 7.33 \\ & 9.06 \\ & 11.2 \end{aligned}$ | $\begin{aligned} & 23.8 \\ & 19.0 \\ & 15.2 \end{aligned}$ | $\begin{aligned} & 48.8 \\ & 59.1 \\ & 70.9 \end{aligned}$ | $\begin{aligned} & 2.58 \\ & 2.55 \\ & 2.52 \end{aligned}$ | $\begin{aligned} & 12.8 \\ & 15.5 \\ & 18.6 \end{aligned}$ | $\begin{aligned} & 17.0 \\ & 20.8 \\ & 25.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 97.6 \\ & 118 \\ & 142 \\ & \hline \end{aligned}$ | $\begin{aligned} & 25.6 \\ & 31.0 \\ & 37.3 \end{aligned}$ | $\begin{aligned} & 0.239 \\ & 0.239 \\ & 0.239 \end{aligned}$ |
| , 88.9 | $\begin{aligned} & 3.2 \\ & 4.0 \\ & 5.0 \end{aligned}$ | $\begin{aligned} & 6.76 \\ & 8.38 \\ & 10.3 \end{aligned}$ | $\begin{aligned} & 8.62 \\ & 10.7 \\ & 13.2 \end{aligned}$ | $\begin{aligned} & 27.8 \\ & 22.2 \\ & 17.8 \end{aligned}$ | $\begin{gathered} 79.2 \\ 96.3 \\ 116 \end{gathered}$ | $\begin{aligned} & 3.03 \\ & 3.00 \\ & 2.97 \\ & \hline \end{aligned}$ | $\begin{aligned} & 17.8 \\ & 21.7 \\ & 26.2 \end{aligned}$ | $\begin{aligned} & 23.5 \\ & 28.9 \\ & 35.2 \end{aligned}$ | $\begin{aligned} & 158 \\ & 193 \\ & 233 \\ & \hline \end{aligned}$ | $\begin{aligned} & 35.6 \\ & 43.3 \\ & 52.4 \end{aligned}$ | $\begin{aligned} & 0.279 \\ & 0.279 \\ & 0.279 \end{aligned}$ |
| 114.3 | $\begin{aligned} & 3.6 \\ & 5.0 \\ & 6.3 \end{aligned}$ | $\begin{aligned} & 9.83 \\ & 13.5 \\ & 16.8 \end{aligned}$ | $\begin{aligned} & 12.5 \\ & 17.2 \\ & 21.4 \end{aligned}$ | $\begin{aligned} & \hline 31.8 \\ & 22.9 \\ & 18.1 \end{aligned}$ | $\begin{aligned} & 192 \\ & 257 \\ & 313 \end{aligned}$ | $\begin{aligned} & 3.92 \\ & 3.87 \\ & 3.82 \end{aligned}$ | $\begin{aligned} & 33.6 \\ & 45.0 \\ & 54.7 \end{aligned}$ | $\begin{aligned} & 44.1 \\ & 59.8 \\ & 73.6 \end{aligned}$ | $\begin{aligned} & 384 \\ & 514 \\ & 625 \end{aligned}$ | $\begin{gathered} 67.2 \\ 89.9 \\ 109 \end{gathered}$ | $\begin{aligned} & 0.359 \\ & 0.359 \\ & 0.359 \end{aligned}$ |
| 139.7 | $\begin{gathered} 5.0 \\ 6.3 \\ 8.0 \\ 10.0 \\ \hline \end{gathered}$ | $\begin{aligned} & 16.6 \\ & 20.7 \\ & 26.0 \\ & 32.0 \end{aligned}$ | $\begin{aligned} & 21.2 \\ & 26.4 \\ & 33.1 \\ & 40.7 \end{aligned}$ | $\begin{aligned} & 27.9 \\ & 22.2 \\ & 17.5 \\ & 14.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 481 \\ & 589 \\ & 720 \\ & 862 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4.77 \\ & 4.72 \\ & 4.66 \\ & 4.60 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 68.8 \\ & 84.3 \\ & 103 \\ & 123 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 90.8 \\ 112 \\ 139 \\ 169 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 961 \\ 1177 \\ 1441 \\ 1724 \\ \hline \end{gathered}$ | $\begin{aligned} & 138 \\ & 169 \\ & 206 \\ & 247 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.439 \\ & 0.439 \\ & 0.439 \\ & 0.439 \\ & \hline \end{aligned}$ |
| 168.3 | $\begin{gathered} 5.0 \\ 6.3 \\ 8.0 \\ 10.0 \\ 12.5 \end{gathered}$ | $\begin{aligned} & 20.1 \\ & 25.2 \\ & 31.6 \\ & 39.0 \\ & 48.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 25.7 \\ & 32.1 \\ & 40.3 \\ & 49.7 \\ & 61.2 \end{aligned}$ | $\begin{aligned} & \hline 33.7 \\ & 26.7 \\ & 21.0 \\ & 16.8 \\ & 13.5 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 856 \\ 1053 \\ 1297 \\ 1564 \\ 1868 \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 5.78 \\ & 5.73 \\ & 5.67 \\ & 5.61 \\ & 5.53 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 102 \\ & 125 \\ & 154 \\ & 186 \\ & 222 \end{aligned}$ | $\begin{aligned} & 133 \\ & 165 \\ & 206 \\ & 251 \\ & 304 \end{aligned}$ | $\begin{aligned} & 1712 \\ & 2107 \\ & 2595 \\ & 3128 \\ & 3737 \\ & \hline \end{aligned}$ | 203 250 308 372 444 | 0.439 0.529 0.529 0.529 0.529 |
| 193.7 | 5.0 6.3 8.0 10.0 12.5 16.0 | $\begin{aligned} & 23.3 \\ & 29.1 \\ & 36.6 \\ & 45.3 \\ & 55.9 \\ & 70.1 \end{aligned}$ | 29.6 37.1 46.7 57.7 71.2 89.3 | $\begin{aligned} & 38.7 \\ & 30.7 \\ & 24.2 \\ & 19.4 \\ & 15.5 \\ & 12.1 \end{aligned}$ | $\begin{aligned} & 1320 \\ & 1630 \\ & 2016 \\ & 2442 \\ & 2934 \\ & 3554 \end{aligned}$ | $\begin{aligned} & \hline 6.67 \\ & 6.63 \\ & 6.57 \\ & 6.50 \\ & 6.42 \\ & 6.31 \end{aligned}$ | $\begin{aligned} & 136 \\ & 168 \\ & 208 \\ & 252 \\ & 303 \\ & 367 \end{aligned}$ | $\begin{aligned} & 178 \\ & 221 \\ & 276 \\ & 338 \\ & 411 \\ & 507 \end{aligned}$ | $\begin{aligned} & 2640 \\ & 3260 \\ & 4031 \\ & 4883 \\ & 5869 \\ & 7109 \\ & \hline \end{aligned}$ | 273 337 416 504 606 734 | $\begin{aligned} & 0.609 \\ & 0.609 \\ & 0.609 \\ & 0.609 \\ & 0.609 \\ & 0.609 \end{aligned}$ |

## SQUARE HOLLOW SECTIONS



DIMENSIONS AND PROPERTIES
y

| Designation |  | Mass per Metre | Area <br> of <br> Section <br> $A$ <br> $\mathrm{~cm}^{2}$ | RatioforLocalBuckling$d / t^{(1)}$ | Second Moment of Area <br> 1 $\mathrm{cm}^{4}$ | Radius of Gyration$\begin{gathered} \mathrm{r} \\ \mathrm{~cm} \end{gathered}$ | Elastic Modulus$\begin{gathered} \mathrm{Z} \\ \mathrm{~cm}^{3} \\ \hline \end{gathered}$ | PlasticModulusS$\mathrm{cm}^{3}$ | Torsional Constants |  | Surface <br> Area <br> per <br> Metre <br> $\mathrm{m}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size | Thickness |  |  |  |  |  |  |  |  |  |  |
| $\begin{gathered} \text { D D } \\ \mathrm{mm} \end{gathered}$ | $\begin{gathered} \mathrm{t} \\ \mathrm{~mm} \end{gathered}$ |  |  |  |  |  |  |  | $\begin{gathered} \mathrm{J} \\ \mathrm{~cm}^{4} \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ \mathrm{~cm}^{3} \end{gathered}$ |  |
| $40 \times 40$ | 2.5 | 2.89 | 3.68 | 13.0 | 8.54 | 1.52 | 4.27 | 5.14 | 13.6 | 6.22 | 0.154 |
|  | 3.0 | 3.41 | 4.34 | 10.3 | 9.78 | 1.50 | 4.89 | 5.97 | 15.7 | 7.10 | 0.152 |
|  | 3.2 | 3.61 | 4.60 | 9.50 | 10.2 | 1.49 | 5.11 | 6.28 | 16.5 | 7.42 | 0.152 |
|  | 4.0 | 4.39 | 5.59 | 7.00 | 11.8 | 1.45 | 5.91 | 7.44 | 19.5 | 8.54 | 0.150 |
|  | 5.0 | 5.28 | 6.73 | 5.00 | 13.4 | 1.41 | 6.68 | 8.66 | 22.5 | 9.60 | 0.147 |
| 50x50 | 2.5 | 3.68 | 4.68 | 17.0 | 17.5 | 1.93 | 6.99 | 8.29 | 27.5 | 10.2 | 0.194 |
|  | 3.0 | 4.35 | 5.54 | 13.7 | 20.2 | 1.91 | 8.08 | 9.70 | 32.1 | 11.8 | 0.192 |
|  | 3.2 | 4.62 | 5.88 | 12.6 | 21.2 | 1.90 | 8.49 | 10.2 | 33.8 | 12.4 | 0.192 |
|  | 4.0 | 5.64 | 7.19 | 9.50 | 25.0 | 1.86 | 9.99 | 12.3 | 40.4 | 14.5 | 0.190 |
|  | 5.0 | 6.85 | 8.73 | 7.00 | 28.9 | 1.82 | 11.6 | 14.5 | 47.6 | 16.7 | 0.187 |
|  | 6.3 | 8.31 | 10.6 | 4.94 | 32.8 | 1.76 | 13.1 | 17.0 | 55.2 | 18.8 | 0.184 |
| $60 \times 60$ | 3.0 | 5.29 | 6.74 | 17.0 | 36.2 | 2.32 | 12.1 | 14.3 | 56.9 | 17.7 | 0.232 |
|  | 3.2 | 5.62 | 7.16 | 15.8 | 38.2 | 2.31 | 12.7 | 15.2 | 60.2 | 18.6 | 0.232 |
|  | 4.0 | 6.90 | 8.79 | 12.0 | 45.4 | 2.27 | 15.1 | 18.3 | 72.5 | 22.0 | 0.230 |
|  | 5.0 | 8.42 | 10.7 | 9.00 | 53.3 | 2.23 | 17.8 | 21.9 | 86.4 | 25.7 | 0.227 |
|  | 6.3 | 10.3 | 13.1 | 6.52 | 61.6 | 2.17 | 20.5 | 26.0 | 102 | 29.6 | 0.224 |
|  | 8.0 | 12.5 | 16.0 | 4.50 | 69.7 | 2.09 | 23.2 | 30.4 | 118 | 33.4 | 0.219 |
| $70 \times 70$ | 3.0 | 6.24 | 7.94 | 20.3 | 59.0 | 2.73 | 16.9 | 19.9 | 92.2 | 24.8 | 0.272 |
|  | 3.6 | 7.40 | 9.42 | 16.4 | 68.6 | 2.70 | 19.6 | 23.3 | 108 | 28.7 | 0.271 |
|  | 5.0 | 9.99 | 12.7 | 11.0 | 88.5 | 2.64 | 25.3 | 30.8 | 142 | 36.8 | 0.267 |
|  | 6.3 | 12.3 | 15.6 | 8.11 | 104 | 2.58 | 29.7 | 36.9 | 169 | 42.9 | 0.264 |
|  | 8.0 | 15.0 | 19.2 | 5.75 | 120 | 2.50 | 34.2 | 43.8 | 200 | 49.2 | 0.259 |
| $80 \times 80$ | 3.0 | 7.18 | 9.14 | 23.7 | 89.8 | 3.13 | 22.5 | 26.3 | 140 | 33.0 | 0.312 |
|  | 3.6 | 8.53 | 10.9 | 19.2 | 105 | 3.11 | 26.2 | 31.0 | 164 | 38.5 | 0.311 |
|  | 5.0 | 11.6 | 14.7 | 13.0 | 137 | 3.05 | 34.2 | 41.1 | 217 | 49.8 | 0.307 |
|  | 6.3 | 14.2 | 18.1 | 9.70 | 162 | 2.99 | 40.5 | 49.7 | 262 | 58.7 | 0.304 |
|  | 8.0 | 17.5 | 22.4 | 7.00 | 189 | 2.91 | 47.3 | 59.5 | 312 | 68.3 | 0.299 |
| $90 \times 90$ | 3.6 | 9.66 | 12.3 | 22.0 | 152 | 3.52 | 33.8 | 39.7 | 237 | 49.7 | 0.351 |
|  | 5.0 | 13.1 | 16.7 | 15.0 | 200 | 3.45 | 44.4 | 53.0 | 316 | 64.8 | 0.347 |
|  | 6.3 | 16.2 | 20.7 | 11.3 | 238 | $3.40$ | 53.0 | 64.3 | 382 | 77.0 | 0.344 |
|  | 8.0 | 20.1 | 25.6 | 8.25 | 281 | 3.32 | 62.6 | 77.6 | 459 | 90.5 | 0.339 |
| 100×100 | 4.0 | 11.9 | 15.2 | 22.0 | 232 | 3.91 | 46.4 | 54.4 | 361 | 68.2 | 0.390 |
|  | 5.0 | 14.7 | 18.7 | 17.0 | 279 | 3.86 | 55.9 | 66.4 | 439 | 81.8 | 0.387 |
|  | 6.3 | 18.2 | 23.2 | 12.9 | 336 | 3.80 | 67.1 | 80.9 | 534 | 97.8 | 0.384 |
|  | 8.0 | 22.6 | 28.8 | 9.50 | 400 | 3.73 | 79.9 | 98.2 | 646 | 116 | 0.379 |
|  | 10.0 | 27.4 | 34.9 | 7.00 | 462 | 3.64 | 92.4 | 116 | 761 | 133 | 0.374 |
| $120 \times 120$ | 4.0 | 14.4 | 18.4 | 27.0 | 410 | 4.72 | 68.4 | 79.7 | 635 | 101 | 0.470 |
|  | 5.0 | 17.8 | 22.7 | 21.0 | 498 | 4.68 | 83.0 | 97.6 | 777 | 122 | 0.467 |
|  | 6.3 | 22.2 | 28.2 | 16.0 | 603 | 4.62 | 100 | 120 | 950 | 147 | 0.464 |
|  | 8.0 | 27.6 | 35.2 | 12.0 | 726 | 4.55 | 121 | 146 | 1160 | 176 | 0.459 |
|  | 10.0 | 33.7 | 42.9 | 9.00 | 852 | 4.46 | 142 | 175 | 1382 | 206 | 0.454 |
|  | 12.5 | 40.9 | 52.1 | 6.60 | 982 | 4.34 | 164 | 207 | 1623 | 236 | 0.448 |



DIMENSIONS AND PROPERTIES
y

| Designation |  | Mass <br> per <br> Metre <br> kg | Area <br> of <br> Section <br> $A$ <br> $\mathrm{~cm}^{2}$ | Ratios for Local Buckling |  | Second Moment of Area |  | Radius of Gyration |  | Elastic Modulus |  | Plastic Modulus |  | Torsional Constants |  | Surface <br> Area <br> per <br> Metre <br> $\mathrm{m}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size | Th |  |  |  |  | Axis | Axis |  |  | Axis | Axis | Axis | Axis |  |  |  |
| $\begin{gathered} \text { D B } \\ \mathrm{mm} \end{gathered}$ | $\begin{gathered} \mathrm{t} \\ \mathrm{~mm} \end{gathered}$ |  |  | (1) <br> d/t | (1) <br> b/t | $\begin{array}{r} x-x \\ \mathrm{~cm}^{4} \\ \hline \end{array}$ | $\begin{gathered} y-y \\ c m^{4} \end{gathered}$ | $\begin{aligned} & x-x \\ & c m \end{aligned}$ | $\begin{aligned} & y-y \\ & \mathrm{~cm} \\ & \hline \end{aligned}$ | $\begin{array}{r} x-x \\ \mathrm{~cm}^{3} \\ \hline \end{array}$ | $\begin{gathered} y-y \\ \mathrm{~cm}^{3} \end{gathered}$ | $\begin{array}{r} x-x \\ \mathrm{~cm}^{3} \\ \hline \end{array}$ | $\begin{gathered} y-y \\ c^{3} \\ \hline \end{gathered}$ | $\underset{\mathrm{cm}}{ }{ }^{\mathrm{J}}$ | $\begin{gathered} \mathrm{C} \\ \mathrm{~cm}^{3} \end{gathered}$ |  |
| 50x30 | 2.5 | 2.89 | 3.68 | 17.0 | 9.00 | 11.8 | 5.22 | 1.79 | 1.19 | 4.73 | 3.48 | 5.92 | 4.11 | 11.7 | 5.73 | 0.154 |
|  | 3.0 | 3.41 | 4.34 | 13.7 | 7.00 | 13.6 | 5.94 | 1.77 | 1.17 | 5.43 | 3.96 | 6.88 | 4.76 | 13.5 | 6.51 | 0.152 |
|  | 3.2 | 3.61 | 4.60 | 12.6 | 6.38 | 14.2 | 6.20 | 1.76 | 1.16 | 5.68 | 4.13 | 7.25 | 5.00 | 14.2 | 6.80 | 0.152 |
|  | 4.0 | 4.39 | 5.59 | 9.50 | 4.50 | 16.5 | 7.08 | 1.72 | 1.13 | 6.60 | 4.72 | 8.59 | 5.88 | 16.6 | 7.77 | 0.150 |
|  | 5.0 | 5.28 | 6.73 | 7.00 | 3.00 | 18.7 | 7.89 | 1.67 | 1.08 | 7.49 | 5.26 | 10.0 | 6.80 | 19.0 | 8.67 | 0.147 |
| $60 \times 40$ | 2.5 | 3.68 | 4.68 | 21.0 | 13.0 | 22.8 | 12.1 | 2.21 | 1.60 | 7.61 | 6.03 | 9.32 | 7.02 | 25.1 | 9.73 | 0.194 |
|  | 3.0 | 4.35 | 5.54 | 17.0 | 10.3 | 26.5 | 13.9 | 2.18 | 1.58 | 8.82 | 6.95 | 10.9 | 8.19 | 29.2 | 11.2 | 0.192 |
|  | 3.2 | 4.62 | 5.88 | 15.8 | 9.50 | 27.8 | 14.6 | 2.18 | 1.57 | 9.27 | 7.29 | 11.5 | 8.64 | 30.8 | 11.7 | 0.192 |
|  | 4.0 | 5.64 | 7.19 | 12.0 | 7.00 | 32.8 | 17.0 | 2.14 | 1.54 | 10.9 | 8.52 | 13.8 | 10.3 | 36.7 | 13.7 | 0.190 |
|  | 5.0 | 6.85 | 8.73 | 9.00 | 5.00 | 38.1 | 19.5 | 2.09 | 1.50 | 12.7 | 9.77 | 16.4 | 12.2 | 43.0 | 15.7 | 0.187 |
|  | 6.3 | 8.31 | 10.6 | 6.52 | 3.35 | 43.4 | 21.9 | 2.02 | 1.44 | 14.5 | 11.0 | 19.2 | 14.2 | 49.5 | 17.6 | 0.184 |
| $80 \times 40$ | 3.0 | 5.29 | 6.74 | 23.7 | 10.3 | 54.2 | 18.0 | 2.84 | 1.63 | 13.6 | 9.00 | 17.1 | 10.4 | 43.8 | 15.3 | 0.232 |
|  | 3.2 | 5.62 | 7.16 | 22.0 | 9.50 | 57.2 | 18.9 | 2.83 | 1.63 | 14.3 | 9.46 | 18.0 | 11.0 | 46.2 | 16.1 | 0.232 |
|  | 4.0 | 6.90 | 8.79 | 17.0 | 7.00 | 68.2 | 22.2 | 2.79 | 1.59 | 17.1 | 11.1 | 21.8 | 13.2 | 55.2 | 18.9 | 0.230 |
|  | 5.0 | 8.42 | 10.7 | 13.0 | 5.00 | 80.3 | 25.7 | 2.74 | 1.55 | 20.1 | 12.9 | 26.1 | 15.7 | 65.1 | 21.9 | 0.227 |
|  | 6.3 | 10.3 | 13.1 | 9.70 | 3.35 | 93.3 | 29.2 | 2.67 | 1.49 | 23.3 | 14.6 | 31.1 | 18.4 | 75.6 | 24.8 | 0.224 |
|  | 8.0 | 12.5 | 16.0 | 7.00 | 2.00 | 106 | 32.1 | 2.58 | 1.42 | 26.5 | 16.1 | 36.5 | 21.2 | 85.8 | 27.4 | 0.219 |
| $90 \times 50$ | 3.0 | 6.24 | 7.94 | 27.0 | 13.7 | 84.4 | 33.5 | 3.26 | 2.05 | 18.8 | 13.4 | 23.2 | 15.3 | 76.5 | 22.4 | 0.272 |
|  | 3.6 | 7.40 | 9.42 | 22.0 | 10.9 | 98.3 | 38.7 | 3.23 | 2.03 | 21.8 | 15.5 | 27.2 | 18.0 | 89.4 | 25.9 | 0.271 |
|  | 5.0 | 9.99 | 12.7 | 15.0 | 7.00 | 127 | 49.2 | 3.16 | 1.97 | 28.3 | 19.7 | 36.0 | 23.5 | 116 | 32.9 | 0.267 |
|  | 6.3 | 12.3 | 15.6 | 11.3 | 4.94 | 150 | 57.0 | 3.10 | 1.91 | 33.3 | 22.8 | 43.2 | 28.0 | 138 | 38.1 | 0.264 |
|  | 8.0 | 15.0 | 19.2 | 8.25 | 3.25 | 174 | 64.6 | 3.01 | 1.84 | 38.6 | 25.8 | 51.4 | 32.9 | 160 | 43.2 | 0.259 |
| 100×50 | 3.0 | 6.71 | 8.54 | 30.3 | 13.7 | 110 | 36.8 | 3.58 | 2.08 | 21.9 | 14.7 | 27.3 | 16.8 | 88.4 | 25.0 | 0.292 |
|  | 3.2 | 7.13 | 9.08 | 28.3 | 12.6 | 116 | 38.8 | 3.57 | 2.07 | 23.2 | 15.5 | 28.9 | 17.7 | 93.4 | 26.4 | 0.292 |
|  | 4.0 | 8.78 | 11.2 | 22.0 | 9.50 | 140 | 46.2 | 3.53 | 2.03 | 27.9 | 18.5 | 35.2 | 21.5 | 113 | 31.4 | 0.290 |
|  | 5.0 | 10.8 | 13.7 | 17.0 | 7.00 | 167 | 54.3 | 3.48 | 1.99 | 33.3 | 21.7 | 42.6 | 25.8 | 135 | 36.9 | 0.287 |
|  | 6.3 | 13.3 | 16.9 | 12.9 | 4.94 | 197 | 63.0 | 3.42 | 1.93 | 39.4 | 25.2 | 51.3 | 30.8 | 160 | 42.9 | 0.284 |
|  | 8.0 | 16.3 | 20.8 | 9.50 | 3.25 | 230 | 71.7 | 3.33 | 1.86 | 46.0 | 28.7 | 61.4 | 36.3 | 186 | 48.9 | 0.279 |
| 100x60 | 3.0 | 7.18 | 9.14 | 30.3 | 17.0 | 124 | 55.7 | 3.68 | 2.47 | 24.7 | 18.6 | 30.2 | 21.2 | 121 | 30.7 | 0.312 |
|  | 3.6 | 8.53 | 10.9 | 24.8 | 13.7 | 145 | 64.8 | 3.65 | 2.44 | 28.9 | 21.6 | 35.6 | 24.9 | 142 | 35.6 | 0.311 |
|  | 5.0 | 11.6 | 14.7 | 17.0 | 9.00 | 189 | 83.6 | 3.58 | 2.38 | 37.8 | 27.9 | 47.4 | 32.9 | 188 | 45.9 | 0.307 |
|  | 6.3 | 14.2 | 18.1 | 12.9 | 6.52 | 225 | 98.1 | 3.52 | 2.33 | 45.0 | 32.7 | 57.3 | 39.5 | 224 | 53.8 | 0.304 |
|  | 8.0 | 17.5 | 22.4 | 9.50 | 4.50 | 264 | 113 | 3.44 | 2.25 | 52.8 | 37.8 | 68.7 | 47.1 | 265 | 62.2 | 0.299 |
| 120x60 | 3.6 | 9.66 | 12.3 | 30.3 | 13.7 | 227 | 76.3 | 4.30 | 2.49 | 37.9 | 25.4 | 47.2 | 28.9 | 183 | 43.3 | 0.351 |
|  | 5.0 | 13.1 | 16.7 | 21.0 | 9.00 | 299 | 98.8 | 4.23 | 2.43 | 49.9 | 32.9 | 63.1 | 38.4 | 242 | 56.0 | 0.347 |
|  | 6.3 | 16.2 | 20.7 | 16.0 | 6.52 | 358 | 116 | 4.16 | 2.37 | 59.7 | 38.8 | 76.7 | 46.3 | 290 | 65.9 | 0.344 |
|  | 8.0 | 20.1 | 25.6 | 12.0 | 4.50 | 425 | 135 | 4.08 | 2.30 | 70.8 | 45.0 | 92.7 | 55.4 | 344 | 76.6 | 0.339 |
| $120 \times 80$ | 5.0 | 14.7 | 18.7 | 21.0 | 13.0 | 365 | 193 | 4.42 | 3.21 | 60.9 | 48.2 | 74.6 | 56.1 | 401 | 77.9 | 0.387 |
|  | 6.3 | 18.2 | 23.2 | 16.0 | 9.70 | 440 | 230 | 4.36 | 3.15 | 73.3 | 57.6 | 91.0 | 68.2 | 487 | 92.9 | 0.384 |
|  | 8.0 | 22.6 | 28.8 | 12.0 | 7.00 | 525 | 273 | 4.27 | 3.08 | 87.5 | 68.1 | 111 | 82.6 | 587 | 110 | 0.379 |
|  | 10.0 | 27.4 | 34.9 | 9.00 | 5.00 | 609 | 313 | 4.18 | 2.99 | 102 | 78.1 | 131 | 97.3 | 688 | 126 | 0.374 |
| $150 \times 100$ | 4.0 | 15.1 | 19.2 | 34.5 | 22.0 | 607 | 324 | 5.63 | 4.11 | 81.0 | 64.8 | 97.4 | 73.6 | 660 | 105 | 0.490 |
|  | 5.0 | 18.6 | 23.7 | 27.0 | 17.0 | 739 | 392 | 5.58 | 4.07 | 98.5 | 78.5 | 119 | 90.1 | 807 | 127 | 0.487 |
|  | 6.3 | 23.1 | 29.5 | 20.8 | 12.9 | 898 | 474 | 5.52 | 4.01 | 120 | 94.8 | 147 | 110 | 986 | 153 | 0.484 |
|  | 8.0 | 28.9 | 36.8 | 15.8 | 9.50 | 1087 | 569 | 5.44 | 3.94 | 145 | 114 | 180 | 135 | 1203 | 183 | 0.479 |
|  | 10.0 | 35.3 | 44.9 | 12.0 | 7.00 | 1282 | 665 | 5.34 | 3.85 | 171 | 133 | 216 | 161 | 1432 | 214 | 0.474 |
|  | 12.5 | 42.8 | 54.6 | 9.00 | 5.00 | 1488 | 763 | 5.22 | 3.74 | 198 | 153 | 256 | 190 | 1679 | 246 | 0.468 |

### 11.4. Aluminium sections (extrusions)

When designing with aluminium there is limited use of standard sections since the extrusion process is very versatile and it is possible to achieve a wide variety of section shapes [1]: Standard profiles are covered by British Standard BS1161 [2].

## I-Beams



| $\mathrm{R}=1.5 \mathrm{t}_{1}$ | y |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Size } \\ & (\mathrm{mm}) \end{aligned}$ | Thickness$(\mathrm{mm})$ |  | Mass/unit length (kg/m) | $\begin{gathered} \text { Area of } \\ \text { section } \\ \left(\mathrm{mm}^{2} \times 10^{2}\right) \end{gathered}$ | Centroid <br> (mm) | $\begin{aligned} & \text { Second moments } \\ & \text { of area } \\ & \left(\mathrm{mm}^{4} \times 10^{4}\right) \end{aligned}$ |  | Radii of gyration(mm) |  | Moduli of section$\left(\mathrm{mm}^{3} \times 10^{3}\right)$ |  | $\begin{gathered} \text { Torsion } \\ \text { constant } \\ \left(\mathrm{mm}^{4} \times 10^{4}\right) \end{gathered}$ |
| $\mathrm{a} \times \mathrm{b}$ | $\begin{gathered} \mathrm{web} \\ \mathrm{t}_{1} \\ \hline \end{gathered}$ | flange $\mathrm{t}_{2}$ | W | A | $\mathrm{c}_{\mathrm{x}}$ and $\mathrm{c}_{\mathrm{y}}$ | $\mathrm{I}_{\mathrm{x}}$ | $\mathrm{I}_{\mathrm{y}}$ | $\mathrm{r}_{\mathrm{x}}$ | $\mathrm{r}_{\mathrm{y}}$ | $\mathrm{Z}_{\mathrm{x}}$ | $\mathrm{Z}_{\mathrm{y}}$ | J |
| $60 \times 30$ | 4 | 6 | 1.59 | 5.83 | 0 | 31.6 | 2.76 | 23.3 | 6.89 | 10.5 | 1.84 | 0.753 |
| $80 \times 40$ | 5 | 7 | 2.54 | 9.38 | 0 | 91.6 | 7.63 | 31.2 | 9.02 | 22.9 | 3.82 | 1.69 |
| $100 \times 50$ | 6 | 8 | 3.72 | 13.7 | 0 | 210 | 17.0 | 39.2 | 11.1 | 42.1 | 6.80 | 3.30 |
| $120 \times 60$ | 6 | 9 | 4.77 | 17.6 | 0 | 403 | 32.8 | 47.8 | 13.6 | 67.2 | 10.9 | 4.76 |
| $140 \times 70$ | 7 | 10 | 6.33 | 23.4 | 0 | 725 | 57.9 | 55.7 | 15.7 | 104 | 16.5 | 8.00 |
| $160 \times 80$ | 7 | 11 | 7.64 | 28.2 | 0 | 1170 | 94.6 | 64.5 | 18.3 | 147 | 23.7 | 10.8 |

## Channel Sections


$\mathrm{R}=1.5 \mathrm{t}_{1}$


| $\begin{aligned} & \text { Size } \\ & (\mathrm{mm}) \end{aligned}$ | Thickness <br> (mm) |  | Mass/ <br> unit <br> length <br> (kg/m) | $\begin{gathered} \text { Area } \\ \text { of } \\ \text { section } \\ \left(\mathrm{mm}^{2} \times\right. \\ \left.10^{2}\right) \end{gathered}$ | Centroid (mm) |  | Second moments of area$\left(\mathrm{mm}^{4} \times 10^{4}\right)$ |  | Radii of gyration (mm) |  | Moduli of section $\left(\mathrm{mm}^{3} \times 10^{3}\right)$ |  | Torsion constant $\left(\mathrm{mm}^{4} \times\right.$ $10^{4}$ ) | Shear centre from back of section (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{a} \times \mathrm{b}$ | web $\mathrm{t}_{1}$ | flange $\mathrm{t}_{2}$ | W | A | $\mathrm{c}_{\mathrm{x}}$ | $\mathrm{c}_{\mathrm{y}}$ | $\mathrm{I}_{\mathrm{x}}$ | $\mathrm{I}_{\mathrm{y}}$ | $\mathrm{r}_{\mathrm{x}}$ | $\mathrm{r}_{\mathrm{y}}$ | $\mathrm{Z}_{\mathrm{x}}$ | $\mathrm{Z}_{\mathrm{y}}$ | J | $\mathrm{c}_{\mathrm{c}}$ |
| $60 \times 30$ | 5 | 6 | 1.69 | 6.24 | 0 | 9.87 | 32.2 | 5.03 | 22.7 | 8.98 | 10.7 | 2.50 | 0.690 | 11.7 |
| $80 \times 35$ | 5 | 7 | 2.29 | 8.44 | 0 | 11.3 | 79.8 | 9.57 | 30.8 | 10.6 | 20.0 | 4.04 | 1.12 | 13.8 |
| $100 \times 40$ | 6 | 8 | 3.20 | 11.8 | 0 | 12.4 | 171 | 16.9 | 38.1 | 11.9 | 34.2 | 6.12 | 2.07 | 15.2 |
| $120 \times 50$ | 6 | 9 | 4.19 | 15.5 | 0 | 15.9 | 339 | 36.8 | 46.8 | 15.4 | 56.5 | 10.8 | 3.22 | 19.7 |
| $140 \times 60$ | 7 | 10 | 5.66 | 20.9 | 0 | 18.9 | 625 | 71.5 | 54.7 | 18.5 | 89.2 | 17.4 | 5.51 | 23.6 |
| $160 \times 70$ | 7 | 10 | 6.58 | 24.3 | 0 | 21.8 | 970 | 116 | 63.2 | 21.8 | 121 | 24.0 | 6.41 | 27.6 |
| $180 \times 75$ | 8 | 11 | 8.06 | 29.8 | 0 | 22.7 | 1480 | 159 | 70.5 | 23.1 | 164 | 30.5 | 9.63 | 29.0 |
| $200 \times 80$ | 8 | 12 | 9.19 | 33.9 | 0 | 24.5 | 2110 | 210 | 78.8 | 24.9 | 211 | 37.8 | 12.4 | 31.3 |
| $240 \times 100$ | 9 | 13 | 12.5 | 46.0 | 0 | 30.3 | 4170 | 450 | 95.2 | 31.2 | 345 | 64.6 | 20.2 | 39.2 |

## Lipped Channel Sections



| $* \mathrm{~A}$ | $=$ | $74.00 \mathrm{t}^{2}$ |
| ---: | :--- | :--- |
| R | $=$ | 2 t |
| a | $=$ | 32 t |
| b | $=$ | 16 t |
| $\mathrm{c}_{\mathrm{x}}$ | $=$ | 0 |
| $\mathrm{c}_{\mathrm{y}}$ | $=$ | 5.36 t |
| $\mathrm{c}_{\mathrm{c}}$ | $=$ | 6.91 t |
| $\mathrm{I}_{\mathrm{x}}$ | $=$ | $12371 \mathrm{t}^{4}$ |
| $\mathrm{I}_{\mathrm{y}}$ | $=$ | $2407 \mathrm{t}^{4}$ |
| $\mathrm{r}_{\mathrm{x}}$ | $=$ | 12.93 t |
| $\mathrm{r}_{\mathrm{y}}$ | $=$ | 5.70 t |
| $\mathrm{Z}_{\mathrm{x}}$ | $=$ | $773 \mathrm{t}^{3}$ |
| $\mathrm{Z}_{\mathrm{y}}$ | $=226 \mathrm{t}^{3}$ |  |
| J | $=41.29 \mathrm{t}^{4}$ |  |

*Excludes small areas present at
internal radii ( $4 \times$. .... ${ }^{2}$ )

| $\begin{aligned} & \text { Size } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{gathered} \text { Thickness } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \text { Mass/ } \\ \text { unit } \\ \text { length } \\ (\mathrm{kg} / \mathrm{m}) \end{gathered}$ | Area of section $\left(\mathrm{mm}^{2} \times\right.$ $10^{2}$ ) | Centroid (mm) |  | Secondmoments ofarea$\left(\mathrm{mm}^{4} \times 10^{4}\right)$ |  | Radii of gyration (mm) |  | Moduli of section $\left(\mathrm{mm}^{3} \times 10^{3}\right)$ |  | Torsion constant $\left(\mathrm{mm}^{4} \times\right.$ $10^{3}$ ) | Shear centre from back of section (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{a} \times \mathrm{b}$ | t | W | A | $\mathrm{c}_{\mathrm{x}}$ | $\mathrm{c}_{\mathrm{y}}$ | $\mathrm{I}_{\mathrm{x}}$ | $\mathrm{I}_{\mathrm{y}}$ | $\mathrm{r}_{\mathrm{x}}$ | $\mathrm{r}_{\mathrm{y}}$ | $\mathrm{Z}_{\mathrm{x}}$ | $\mathrm{Z}_{\mathrm{y}}$ | J | $\mathrm{c}_{\mathrm{c}}$ |
| $80 \times 40$ | 2.5 | 1.25 | 4.62 | 0 | 13.4 | 48.3 | 9.40 | 32.3 | 14.2 | 12.1 | 3.53 | 1.61 | 17.3 |
| $100 \times 50$ | 3.13 | 1.96 | 7.23 | 0 | 16.8 | 118 | 23.0 | 40.4 | 17.8 | 23.6 | 6.90 | 3.94 | 21.6 |
| $120 \times 60$ | 3.75 | 2.82 | 10.4 | 0 | 20.1 | 245 | 47.6 | 48.5 | 21.4 | 40.8 | 11.9 | 8.16 | 25.9 |
| $140 \times 70$ | 4.38 | 3.84 | 14.2 | 0 | 23.5 | 453 | 88.2 | 56.6 | 24.9 | 64.8 | 18.9 | 15.1 | 30.2 |

## Equal Bulb Angle Sections



| $* \mathrm{~A}$ | $=54.92 \mathrm{t}^{2}$ |
| ---: | :--- |
| R | $=2 \mathrm{t}$ |
| a | $=\mathrm{b}=20 \mathrm{t}$ |

*Excludes small areas present at internal radii $\left(4 \times 0.086 t^{2}\right)$
$\mathrm{c}_{\mathrm{x}}=6.07 \mathrm{t}$
$c_{y}=6.07 \mathrm{t}$
$I_{x}=2605 t^{4}$
$\mathrm{I}_{\mathrm{y}}=2605 \mathrm{t}^{4}$
$\mathrm{I}_{\mathrm{u}}=4030 \mathrm{t}^{4} \quad \mathrm{Z}_{\mathrm{x}}=187 \mathrm{t}^{3}$
$\mathrm{I}_{\mathrm{v}}=1180 \mathrm{t}^{4}$
$Z_{y}=187 \mathrm{t}^{3}$

$r_{v}=4.64 \mathrm{t} \quad \tan \alpha=$
$\mathrm{u}-\mathrm{u}$ and $\mathrm{v}-\mathrm{v}$ are principal axes
$r_{x}=6.89 \mathrm{t} \quad \mathrm{Z}_{\mathrm{u}}=285 \mathrm{t}^{3}$
$\mathrm{r}_{\mathrm{y}}=6.89 \mathrm{t} \quad \mathrm{Z}_{\mathrm{v}}=138 \mathrm{t}^{3}$
$\mathrm{r}_{\mathrm{u}}=8.57 \mathrm{t} \quad \alpha=45^{\circ}$
$\mathrm{J}=51.32 \mathrm{t}^{4}$

| $\begin{aligned} & \text { Size } \\ & (\mathrm{mm}) \end{aligned}$ | Thick- <br> ness <br> (mm) | Mass/ unit length (kg/m) | Area of section ( $\mathrm{mm}^{2} \times$ $10^{2}$ ) | Centroid <br> (mm) | Second moments of area $\left(\mathrm{mm}^{4} \times 10^{4}\right)$ |  |  | Radii of gyration (mm) |  |  | Moduli of section$\left(\mathrm{mm}^{3} \times 10^{3}\right)$ |  |  | Torsion constant $\left(\mathrm{mm}^{4} \times\right.$ $10^{4}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{a} \times \mathrm{b}$ | t | W | A | $\mathrm{c}_{\mathrm{x}}$ and $\mathrm{c}_{\mathrm{y}}$ | $\mathrm{I}_{\mathrm{x}}$ and $\mathrm{I}_{\mathrm{y}}$ | $\mathrm{I}_{\mathrm{u}}$ | $\mathrm{I}_{\mathrm{v}}$ | $\begin{gathered} \mathrm{r}_{\mathrm{x}} \text { and } \\ \mathrm{r}_{\mathrm{y}} \\ \hline \end{gathered}$ | $\mathrm{r}_{\mathrm{u}}$ | $\mathrm{r}_{\mathrm{v}}$ | $\begin{gathered} \hline Z_{x} \text { and } \\ Z_{y} \\ \hline \end{gathered}$ | $\mathrm{Z}_{u}$ | $\mathrm{Z}_{\mathrm{v}}$ | J |
| $50 \times 50$ | 2.5 | 0.930 | 3.43 | 15.2 | 10.2 | 15.7 | 4.61 | 17.2 | 21.4 | 11.6 | 2.92 | 4.45 | 2.16 | 0.200 |
| $60 \times 60$ | 3 | 1.34 | 4.94 | 18.2 | 21.1 | 32.6 | 9.56 | 20.7 | 25.7 | 13.9 | 5.05 | 7.70 | 3.73 | 0.416 |
| $80 \times 80$ | 4 | 2.38 | 8.79 | 24.3 | 66.7 | 103 | 30.2 | 27.6 | 34.3 | 18.6 | 12.0 | 18.2 | 8.82 | 1.31 |
| $100 \times 100$ | 5 | 3.72 | 13.7 | 30.3 | 163 | 252 | 73.8 | 34.4 | 42.8 | 23.2 | 23.4 | 35.6 | 17.2 | 3.21 |
| $120 \times 120$ | 6 | 5.36 | 19.8 | 36.4 | 338 | 522 | 153 | 41.3 | 51.4 | 27.8 | 40.4 | 61.6 | 29.8 | 6.65 |

[1] Dwight, J.B. (1999), Aluminium Design and Construction, E\&FN Spon, London and New York.
[2] British Standards Institute, (1977), Specification for Aluminium Alloy Sections for Structural Purposes,
BS1161:1977, British Standards Institute, UK.

### 11.5. Glass fibre reinforced plastic (GFRP) sections (pultrusions)*

A wide variety of shapes is also possible with the pultrusion process and each GFRP manufacturer will produce a different standard product range. Typical examples:


I- Beams


Channels


Square Hollow Sections

## I-Beams

| Section <br> Designation | Depth <br> D <br> $(\mathrm{mm})$ | Width <br> B <br> $(\mathrm{mm})$ | Web <br> t <br> $(\mathrm{mm})$ | Flange <br> T <br> $(\mathrm{mm})$ | $\mathrm{I}_{\mathrm{xx}}$ <br> $\left(\mathrm{cm}^{4}\right)$ | $\mathrm{I}_{\mathrm{yy}}$ <br> $\left(\mathrm{cm}^{4}\right)$ | Area <br> $\left(\mathrm{cm}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $53 \times 50$ | 53 | 50 | 7 | 7 | 40.8 | 14.7 | 9.73 |
| $102 \times 51$ | 102 | 51 | 6.35 | 6.35 | 186 | 14.2 | 12.1 |
| $150 \times 150$ | 150 | 150 | 10 | 10 | 1660 | 564 | 43.0 |
| $200 \times 200$ | 200 | 200 | 10 | 10 | 4100 | 1330 | 58.0 |

Channels

| Section <br> Designation | Depth <br> D <br> $(\mathrm{mm})$ | Width <br> B <br> $(\mathrm{mm})$ | Web <br> t <br> $(\mathrm{mm})$ | Flange <br> T <br> $(\mathrm{mm})$ | $\mathrm{I}_{\mathrm{xx}}$ <br> $\left(\mathrm{cm}^{4}\right)$ | $\mathrm{I}_{\mathrm{yy}}$ <br> $\left(\mathrm{cm}^{4}\right)$ | Area <br> $\left(\mathrm{cm}^{2}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $50.8 \times 25.4$ | 50.8 | 25.4 | 3.2 | 3.2 | 11.6 | 1.82 | 3.05 |
| $73 \times 25$ | 73 | 25 | 5.0 | 5.0 | 39.4 | 2.76 | 5.65 |
| $100 \times 40$ | 100 | 40 | 5.0 | 5.0 | 121 | 11.9 | 8.50 |
| $200 \times 50$ | 200 | 50 | 10 | 10 | 1390 | 48.0 | 28.0 |
| $200 \times 60$ | 200 | 60 | 8.0 | 8.0 | 1300 | 68.9 | 24.3 |
| $500 \times 60$ | 500 | 60 | 7.0 | 7.0 | 11800 | 73.9 | 42.4 |

Square Hollow Sections

| Designation |  | Area |  |
| :---: | :---: | :---: | :---: |
| Size | Thickness |  | $\begin{array}{c}\mathrm{t} \\ (\mathrm{mm})\end{array}$ |
| $\left(\mathrm{cm}^{2}\right)$ |  |  | \(\left.\begin{array}{c}\mathrm{I}_{\mathrm{xx}}=\mathrm{I}_{\mathrm{yy}} <br>


\left(\mathrm{cm}^{4}\right)\end{array}\right]\)| $31.8 \times 31.8$ | 3.0 | 3.46 | 4.83 |
| :---: | :---: | :---: | :---: |
| $44.0 \times 44.0$ | 6.0 | 9.12 | 22.5 |
| $51.0 \times 51.0$ | 3.2 | 6.12 | 23.4 |
| $100 \times 100$ | 4.0 | 15.3 | 236 |

[^1]
[^0]:    Areas calculated to 3 significant figures

[^1]:    * The GFRP section details are based on information provided by Fibreforce Composites Ltd, Runcorn, Cheshire.

