

EGT2  
ENGINEERING TRIPOS PART IIA

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Monday 6 May 2024 2 to 3.40

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**Module 3A6**

**HEAT AND MASS TRANSFER**

*Answer not more than **three** questions.*

*All questions carry the same number of marks.*

*The **approximate** percentage of marks allocated to each part of a question is indicated in the right margin.*

*Write your candidate number **not** your name on the cover sheet.*

**STATIONERY REQUIREMENTS**

Single-sided script paper

**SPECIAL REQUIREMENTS TO BE SUPPLIED FOR THIS EXAM**

CUED approved calculator allowed

Engineering Data Book

**10 minutes reading time is allowed for this paper at the start of the exam.**

**You may not start to read the questions printed on the subsequent pages of this question paper until instructed to do so.**

**You may not remove any stationery from the Examination Room.**

1 Clouds exchange radiative heat with the sun, space and earth. Consider a cloud in steady state, modelled as a thin flat disc for which the lower and upper surfaces have view factors  $F_c = 1$  to earth and space, respectively. The earth is at temperature  $T_e = 285$  K and radiates as a grey body with a spectrally-independent emissivity  $\epsilon_e = 0.95$ . Assume that for the area under the cloud the earth has no direct view of space. The sun emits as a black body at temperature  $T_s = 5800$  K with an irradiation flux  $G_s = 1000$  (in  $\text{W m}^{-2}$ ) incident on the clouds and earth. Space can be considered a black body at  $T_\infty = 0$ .

(a) Draw a diagram of the radiative interaction between the cloud and sun, neglecting any interaction with the earth. Label the solar irradiation  $G_s$  from the sun, transmitted radiation  $G_\tau$ , reflected radiation  $G_\rho$  and the cloud emissive power  $E$ . Your labelling should include dependence on the transmissivity  $\tau_c$ , reflectivity  $\rho_c$ , absorptivity  $\alpha_c$  and emissivity  $\epsilon_c$  of the cloud. Identify also the radiosity for the upper and lower cloud surfaces. [25%]

(b) Consider the radiative flux to earth across a cloud for which the reflectivity is zero for radiation emitted by the earth. Determine expressions for the incident radiative flux and the net radiative flux on the earth beneath the cloud. [20%]

(c) Consider a thin cloud at temperature  $T_c = 240$  K with emissivity  $\epsilon_c = 0.95$ . Its transmissivity is  $\tau_c = 0.95$  for solar irradiation, but it is opaque to infrared radiation and has zero reflectivity at all wavelengths. All emitted radiation from earth and cloud may be considered infrared. Calculate the net radiative heat flux to the earth, both with and without the cloud. [25%]

(d) Thick clouds have  $\epsilon_c = 0.95$  and are opaque at all wavelengths. Consider the surface of the earth at night, with no incident radiation, and assume that thick clouds cover half of that surface. The clouds and uncovered earth both exchange radiative heat with space. Draw a resistor network to represent the heat transfer process and determine the equivalent resistances. Calculate the radiative heat flux from the earth at night. [30%]

2 A hot-wire anemometer is composed of a thin cylindrical wire, of length  $2L$  and diameter  $D$ , fixed at its ends. An electric current is supplied to the wire, providing a constant and uniform heat production rate  $\dot{g}$  per unit volume of wire. Air at ambient temperature  $T_o$  flows perpendicular to the wire, the ends of which are also at  $T_o$ . The thermal conductivities of the wire and the air are  $100$  and  $0.03 \text{ W m}^{-1}\text{K}^{-1}$  respectively. The Prandtl number for air is  $\text{Pr} = 0.7$  and the Nusselt number for a cylinder in cross flow is given by

$$\text{Nu} = (0.35 + 0.67 \text{Re}^{0.52}) \text{Pr}^{0.3}$$

where  $\text{Re}$  is the Reynolds number based on the wire diameter. Radiation may be neglected.

(a) A typical hot wire has a diameter of a few  $\mu\text{m}$  and is used to measure velocities of a few  $\text{m s}^{-1}$ . Show that the wire temperature,  $T$ , may be treated as radially uniform. [15%]

(b) Show that the temperature variation along the wire is governed by

$$\frac{d^2\theta}{dx^2} - m^2\theta = B$$

where  $x$  is the distance from the wire centre and  $\theta = T - T_o$ . Determine  $B$  and  $m$  in terms of the given parameters. [25%]

(c) Show that the general solution to the equation of part (b) is

$$\theta = C_1 e^{mx} + C_2 e^{-mx} + C_3$$

Determine values for  $C_1$ ,  $C_2$  and  $C_3$  in terms of  $m$ ,  $B$  and  $L$ . Hence obtain the complete solution for  $\theta$ . Sketch curves of this solution, indicating how it changes with  $\dot{g}$  and  $mL$  as a function of  $x/L$ . [35%]

(d) Using the governing equation given in part (b), or otherwise, show that the total heat generation rate balances the total rate of heat loss from the wire. [25%]

3 Figure 1 shows the plan view of a building of width  $W$  and height  $H$  subjected to a cross wind with incoming free-stream velocity  $U$ . A geometrically similar model is built with length-scale ratio  $r_L = H/H_m$  (where subscript  $m$  refers to the model) and is tested in a wind tunnel to determine wind forces and heat transfer rates. The measured force on the model,  $F_m$ , increases by a factor of 8 when the test air speed,  $U_m$ , is increased by a factor of 4.

(a) The drag coefficient is known to vary according to

$$C_D \propto \text{Re}^n$$

where  $\text{Re}$  is the Reynolds number based on  $W$ . Determine the index  $n$ . [20%]

(b) Assuming a relation similar to the Reynolds analogy applies – i.e.,

$$\text{St} = \frac{C_D}{2}$$

where  $\text{St}$  is the Stanton number – determine the form of the dependence of Nusselt number on Reynolds number. [10%]

(c) In a particular model test,  $W_m = 0.5$  m,  $H_m = 0.8$  m and  $U_m = 8$  m s<sup>-1</sup>, and  $r_L = 8$ . The measured force on the model is then 7.7 N. Estimate the force on the full-size building if the wind speed is 10 m s<sup>-1</sup>. Estimate also the heat loss from the building when the temperature difference between its surface and the oncoming air is 15°C. Evaluate air properties at 0°C and 1 bar for both the model and the real flow. [40%]

(d) For the case shown in Fig. 1, sketch the expected rate of heat transfer at the surface as a function of distance along the surface ABC. Justify the shape of your curve, identifying any relevant features. How would the curve change as  $U$  increases. [20%]

(e) Discuss briefly the possibility of undertaking the tests in water, highlighting any additional factors that would need to be considered. [10%]

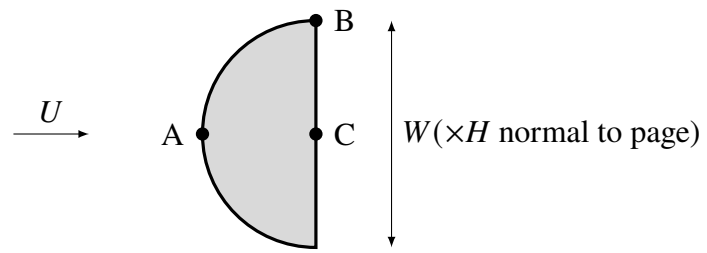


Fig. 1

4 A spherical water droplet of initial radius  $R_0$  and surface temperature  $T_s$  is suspended in stagnant humid air of density  $\rho$ . Mass transfer between the droplet and surrounding air may be considered a quasi-steady process such that conservation of water vapour within the humid air is governed by

$$\mathbf{u} \cdot \nabla(\rho Y) = \nabla \cdot (D \nabla \{\rho Y\})$$

where  $\mathbf{u}$  is the convection velocity,  $Y$  is the mass fraction of water vapour and  $D$  is the diffusion coefficient.

(a) Assuming spherical symmetry, show that the evaporation rate for a droplet of radius  $R$  is given by

$$\dot{m} = 4\pi\rho DR \ln\left(\frac{1 - Y_\infty}{1 - Y_s}\right)$$

where  $Y_s$  and  $Y_\infty$  are the mass fractions of water vapour at the droplet surface and far from the droplet respectively. [35%]

(b) Determine an expression for the rate of change of  $R^2$  in terms of the given parameters and the liquid density,  $\rho_l$ . Sketch the resulting variation of  $R$  with time, and the corresponding mass transfer rate for the case where  $T_s$  is constant. [30%]

(c) Assume now that  $T_s$  and the corresponding water saturation pressure,  $p_{\text{sat}}$ , vary according to

$$\frac{T_s - T_{s,0}}{T_\infty - T_{s,0}} = 1 - e^{-t/\tau} \quad \text{and} \quad \frac{p_{\text{sat}}(T_s) - p_{\text{sat}}(T_\infty)}{p_a} = K \frac{T_s - T_\infty}{T_\infty}$$

where  $\tau$ , is a time constant,  $p_a$  is ambient pressure and the subscripts 0 and  $\infty$  denote initial and far-field values respectively. Assume also that  $Y \ll 1$  everywhere, such that the molecular weight of the air is approximately that of dry air.

Obtain an expression for  $dR^2/dt$  as a function of the given quantities and the molecular weights of dry air and water vapour,  $W_a$  and  $W_v$  respectively. Comment on the nature of the mass transfer in this case. [35%]

**END OF PAPER**

**Answers**

1 (a) -, (b) -, (c)  $717 \text{ W m}^{-2}$  (with clouds) and  $645 \text{ W m}^{-2}$  (without clouds).

2 (a) -, (b) -, (c) -, (d) - .

3 (a)  $n = -0.5$  , (b)  $\text{Nu}_L \propto \text{Re}_L^{0.5}$ , (c)  $F = 243 \text{ N}$ ,  $Q = 364 \text{ kW}$ , (d) - , (e) -

4 (a) -, (b) -, (c) -, (d) - .