

(Hugh Hunt, James Talbot)

$$\begin{aligned}
 (a) \quad p &= \frac{C\omega}{A} [1 + \cot^2 \theta + \operatorname{cosec}^2 \theta]^{-\frac{1}{2}} \\
 &= \frac{C\omega}{A} [\operatorname{cosec}^2 \theta + \operatorname{cosec}^2 \theta]^{-\frac{1}{2}} = \frac{C\omega}{\sqrt{2} A \sin \theta}
 \end{aligned}$$

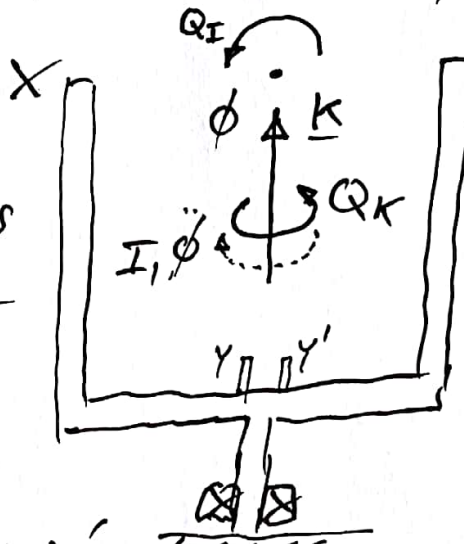


Note that $\cot \theta = 0$ for $\theta = \frac{\pi}{2}$ so the J_1 term vanishes. This is

because rotations around $\theta = \frac{\pi}{2}$ is not associated with rotations of the assembly about \underline{k}

(b) Stand

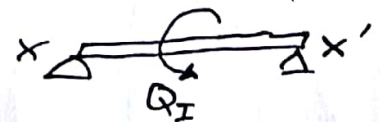
The assembly clicks in at X & X' (but it makes no difference to use Y & Y'). It is free to turn about $X-X'$.

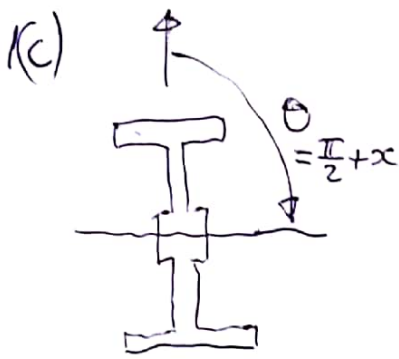


\underline{I} out of page (i.e. in \underline{k} direction for $\theta = \frac{\pi}{2}$)

So this couple is zero. There is a d'Alembert inertial couple $I_1 \ddot{\phi}$ about \underline{k} and is equal to $I_1 \ddot{\phi}$. So $Q_k \underline{k}$ acts on the stand $Q_k = I_1 \ddot{\phi}$

There is an as-yet unknown couple $Q_I \underline{I}$ acting on the stand because $X-X'$ are spaced apart, as if simply supported





rotor, gyro equations (fast spin)

$$Q_1 = A \dot{\Omega}_1 - (A \Omega_3 - C \omega_3) \Omega_2 \quad (1)$$

$$Q_2 = A \dot{\Omega}_2 + (A \Omega_3 - C \omega_3) \Omega_1 \quad (2)$$

$$Q_3 = C \dot{\omega}_3 \quad (\text{constant}) \quad (Q_3 = 0) \quad (3)$$

(d) linearize about $\Theta_0 = \frac{\pi}{2}$

put $\Theta = \frac{\pi}{2} + x$ (x small)

$$\sin \Theta \approx 1$$

$$\cos \Theta \approx -x$$

$$\Omega_1 = -\dot{\phi} \sin \Theta \approx -\dot{\phi}$$

$$\Omega_2 = \dot{\Theta} = \dot{x}$$

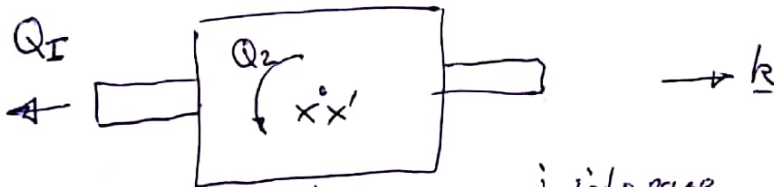
$$\Omega_3 = \dot{\phi} \cos \Theta \approx -\dot{\phi} x = 0$$

Note that, for small oscillations, x & $\dot{\phi}$ are small so ignore terms like x^2 , $x \dot{\phi}$, $\dot{\phi}^2$ etc

$$\text{So } (1) \quad Q_1 \approx -A \ddot{\phi} + C \omega_3 \dot{x} \quad (1)^a$$

$$\& (2) \quad Q_2 \approx A \ddot{x} + C \omega_3 \dot{\phi} \quad (2)^a$$

$$\downarrow Q_H = I_1 \ddot{\phi}$$



$\downarrow Q_H$
Assembly

\downarrow into page

from this, $Q_1 = I_1 \ddot{\phi}$ & $Q_2 = 0$

$\therefore (1)^a$ becomes $(I_1 + A) \ddot{\phi} = C \omega_3 \dot{x}$
integrate $\therefore \phi = \frac{C \omega_3}{I_1 + A} x + \text{const}$

$(1)^b$ becomes $0 = A \ddot{x} + \frac{(C \omega_3)^2}{I_1 + A} x + \text{const}$

This gives SHM at frequency $p^* = \frac{C \omega_3}{A} \left(1 + \frac{I_1}{A}\right)^{-\frac{1}{2}}$

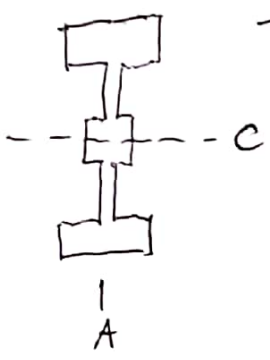
which is correct for $\Theta_0 = \frac{\pi}{2}$ & $J_1 = 0$

Q2 More generally (not expected)

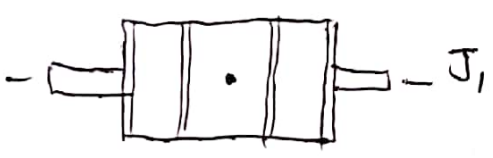
$-\frac{1}{2}$ 1

$$P = \frac{C\omega}{A} \left[1 + \frac{J_1}{A} \cot^2 \theta_0 + \frac{I_1}{A} \operatorname{cosec}^2 \theta_0 \right]$$

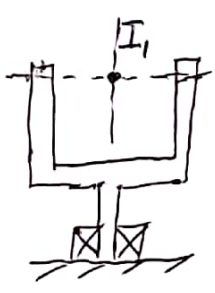
This is the nutation rate for the 3CS lab gyro in its gimbal frame.



The rotor is AAC in assembly-fixed axes \underline{i} , \underline{j} , \underline{k}
 Note that "A" includes the moment of inertia of the gyro assembly

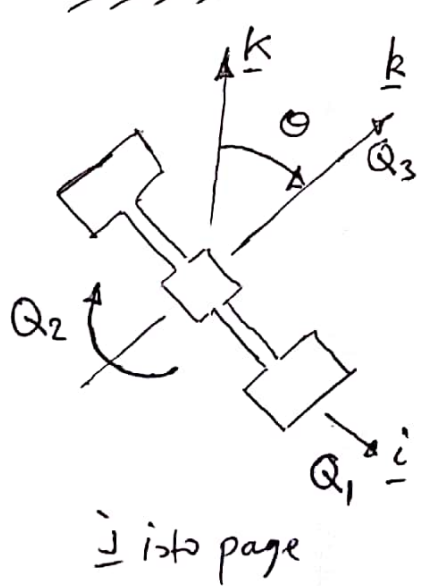


The gyro assembly has moment of inertia J_1 about its axis \underline{k}

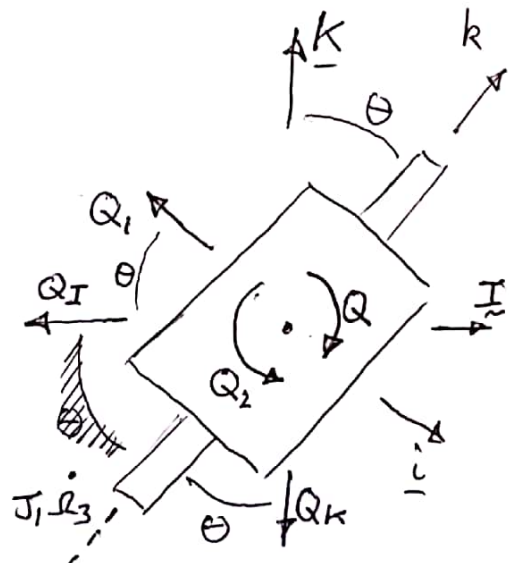


The support stand has moment of inertia I_1 about the vertical axis \underline{k}

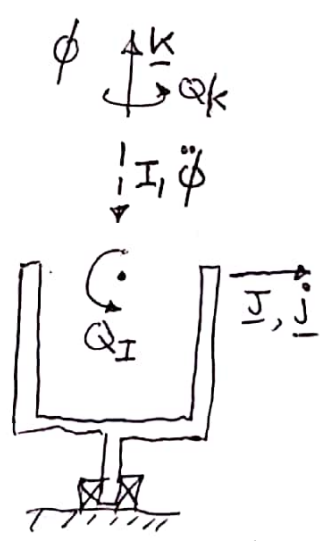
Angle of tilt is θ , Spin is $\omega_3 \underline{k}$



Couples Q_1, Q_2 & Q_3 act on the rotor
 \therefore equal & opposite on assembly



Q_1, Q_2 from stand is $-\underline{i}$ & $-\underline{k}$ directions
 External couple Q_j & \underline{k} axis (\underline{i} out of page)



Frictionless about \underline{j}
 Couples Q_I, Q_K about \underline{i} axis acting on stand

Gyro equations for rotor

Euler angles (2)

$$\begin{array}{l}
 \text{i} \\
 \text{j} \\
 \text{k}
 \end{array}
 \begin{array}{l}
 \textcircled{1} \\
 \textcircled{2} \\
 \textcircled{3}
 \end{array}
 \left. \begin{array}{l}
 Q_1 = A\dot{\Omega}_1 - (A\Omega_3 - C\omega_3)\Omega_2 \\
 Q_2 = A\dot{\Omega}_2 + (A\Omega_3 - C\omega_3)\Omega_1 \\
 Q_3 = C\dot{\omega}_3 = 0 \quad (\text{frictionless about } \underline{k})
 \end{array} \right\}
 \begin{array}{l}
 \Omega_1 = -\dot{\phi} \sin \theta \\
 \Omega_2 = \dot{\theta} \\
 \Omega_3 = \dot{\phi} \cos \theta \\
 \omega_3 = \Omega_3 + \dot{\psi}
 \end{array}$$

∴ $\omega_3 = \text{constant}$

Inertia couples $-I_1 \ddot{\phi} \underline{k}$ and $-J_1 \dot{\Omega}_3 \underline{k}$ act on stand and assembly

so for stand $Q_k = I_1 \ddot{\phi} \quad | \underline{k} \quad \textcircled{7}$

and for assembly

$$\begin{array}{l}
 Q_I \cos \theta + Q_1 - Q_k \sin \theta = 0 \\
 Q_2 - Q = 0 \\
 Q_I \sin \theta + Q_k \cos \theta + J_1 \dot{\Omega}_3 = 0
 \end{array}
 \left. \begin{array}{l}
 \textcircled{4} \\
 \textcircled{5} \\
 \textcircled{6}
 \end{array} \right|$$

In steady state precession $\theta = \theta_0 = \text{const}$
 due to $Q \quad \dot{\phi} = \dot{\phi}_0 = \text{const}$

$$\begin{aligned}
 \therefore \Omega_1 &= -\dot{\phi}_0 \sin \theta_0 = \text{const} \\
 \Omega_2 &= \dot{\theta} = 0 \\
 \Omega_3 &= \dot{\phi}_0 \cos \theta_0 = \text{const}
 \end{aligned}$$

Gyro equation (2) is the only meaningful one

$$\therefore Q_2 = -(A\Omega_3 - C\omega_3)\dot{\phi}_0 \sin \theta_0$$

and for fast spin $Q_2 \approx C\omega_3 \dot{\phi}_0 \sin \theta_0$

and with (5) $Q \approx C\omega_3 \dot{\phi}_0 \sin \theta_0 \quad \textcircled{8}$

Now for nutation perturb the motion

$$\begin{array}{l}
 \theta = \theta_0 + x \quad \dot{\theta} = \dot{x} \quad \ddot{\theta} = \ddot{x} \\
 \phi = \phi_0 + y \quad \dot{\phi} = \dot{y}
 \end{array}
 \quad x, y \text{ small}$$

$$\Omega_1 = -(\dot{\phi}_0 + \dot{y}) \sin(\theta_0 + x) = -(\dot{\phi}_0 + \dot{y})(\sin \theta_0 \cos x + \cos \theta_0 \sin x)$$

and $\sin x \approx x \quad \cos x \approx 1$

$$\begin{aligned} \therefore \Omega_1 &\approx -(\dot{\phi}_0 + y)(\sin \theta_0 + x \cos \theta_0) \\ &\approx -\dot{\phi}_0 \sin \theta_0 - y \sin \theta_0 - x \cos \theta_0 \dot{\phi}_0 \\ \& \ \Omega_2 &\approx \dot{x} \\ \& \ \Omega_3 &\approx (\dot{\phi}_0 + y) \cos(\theta_0 + x) \\ &\approx (\dot{\phi}_0 + y)(\cos \theta_0 \cos x - \sin \theta_0 \sin x) \\ &\approx (\dot{\phi}_0 + y)(\cos \theta_0 - x \sin \theta_0) \\ &\approx \dot{\phi}_0 \cos \theta_0 + y \cos \theta_0 - x \sin \theta_0 \dot{\phi}_0 \end{aligned}$$

3

$$\begin{aligned} \dot{\Omega}_1 &\approx -\dot{y} \sin \theta_0 - x \cos \theta_0 \dot{\phi}_0 \\ \dot{\Omega}_2 &= \ddot{x} \\ \dot{\Omega}_3 &= \dot{y} \cos \theta_0 - x \sin \theta_0 \dot{\phi}_0 \end{aligned}$$

~~(4)~~ $\therefore Q_1 = Q_K \sin \theta - Q_I \cos \theta$

(7) $Q_K = I_1 \ddot{\phi} = I_1 \dot{y}$

(6) $Q_I \sin \theta = -Q_K \cos \theta - J_1 \dot{\Omega}_3$

$$\therefore Q_I \sin(\theta_0 + x) = -I_1 \dot{y} \cos(\theta_0 + x) - J_1 (\dot{y} \cos \theta_0 - x \sin \theta_0 \dot{\phi}_0)$$

$$\begin{aligned} \therefore Q_I (\sin \theta_0 + x \cos \theta_0) &= -I_1 \dot{y} (\cos \theta_0 - x \sin \theta_0) \\ &\quad - J_1 (\dot{y} \cos \theta_0 - x \sin \theta_0 \dot{\phi}_0) \end{aligned}$$

$$\begin{aligned} \therefore Q_I \sin \theta_0 (1 + x \cot \theta_0) &= -I_1 \cos \theta_0 \dot{y} - J_1 \cos \theta_0 \dot{y} + J_1 \sin \theta_0 \dot{\phi}_0 x \\ &= -I_1 \cos \theta_0 \dot{y} - J_1 \cos \theta_0 \dot{y} + J_1 \sin \theta_0 \dot{\phi}_0 x \end{aligned}$$

(note y, x is very small)

$$\begin{aligned} \therefore Q_I &= \frac{(1 - x \cot \theta_0)}{\sin \theta_0} (J_1 \sin \theta_0 \dot{\phi}_0 x - (I_1 + J_1) \cos \theta_0 \dot{y}) \\ &= \frac{1}{\sin \theta_0} (J_1 \sin \theta_0 \dot{\phi}_0 x - (I_1 + J_1) \cos \theta_0 \dot{y}) \end{aligned}$$

$$\begin{aligned} \therefore Q_1 &= I_1 \dot{y} \sin(\theta_0 + x) - \frac{\cos(\theta_0 + x)}{\sin \theta_0} (J_1 \sin \theta_0 \dot{\phi}_0 x - (I_1 + J_1) \cos \theta_0 \dot{y}) \\ &= I_1 \dot{y} (\sin \theta_0 + x \cos \theta_0) - \frac{\cos \theta_0 - x \sin \theta_0}{\sin \theta_0} (J_1 \sin \theta_0 \dot{\phi}_0 x - (I_1 + J_1) \cos \theta_0 \dot{y}) \\ &= I_1 \dot{y} \sin \theta_0 - \cot \theta_0 (J_1 \sin \theta_0 \dot{\phi}_0 x - (I_1 + J_1) \cos \theta_0 \dot{y}) \end{aligned}$$

$$\therefore Q_1 = I_1 \dot{y} \sin \theta_0 - J_1 \cos \theta_0 \dot{\phi}_0 \dot{x} + (I_1 + J_1) \frac{\omega_s^2 \theta_0}{\sin \theta_0} \dot{y} \quad (4)$$

$$\text{note } \sin \theta_0 + \frac{\cos^2 \theta_0}{\sin \theta_0} = \frac{\sin^2 \theta_0 + \cos^2 \theta_0}{\sin \theta_0} = \operatorname{cosec} \theta_0$$

$$\therefore Q_1 = -J_1 \cos \theta_0 \dot{\phi}_0 \dot{x} + (J_1 \cos \theta_0 \cot \theta_0 + I_1 \operatorname{cosec} \theta_0) \dot{y}$$

$$\text{and } (1) \quad Q_1 = -A (\dot{y} \sin \theta_0 + \dot{x} \cos \theta_0 \dot{\phi}_0) + C \omega_3 \dot{x} \quad (\text{fast spin})$$

$$= -A \sin \theta_0 \dot{y} + (C \omega_3 - A \cos \theta_0 \dot{\phi}_0) \dot{x} \quad (\text{fast spin})$$

$$\therefore (C \omega_3 - A \cos \theta_0 \dot{\phi}_0 + J_1 \cos \theta_0 \dot{\phi}_0) \dot{x} \\ = (J_1 \cos \theta_0 \cot \theta_0 + I_1 \operatorname{cosec} \theta_0 + A \sin \theta_0) \dot{y}$$

$$\text{or } (2) \quad Q = A \ddot{x} + C \omega_3 (\dot{\phi}_0 \sin \theta_0 + y \sin \theta_0 - x \cos \theta_0 \dot{\phi}_0)$$

and note steady state response from (8)

$$\therefore A \ddot{x} + C \omega_3 \sin \theta_0 y - C \omega_3 \cos \theta_0 \dot{\phi}_0 x = 0$$

$$\therefore A \ddot{x} + C \omega_3 \left(\frac{\sin \theta_0 (C \omega_3 - A \cos \theta_0 \dot{\phi}_0 + J_1 \cos \theta_0 \dot{\phi}_0)}{J_1 \cos \theta_0 \cot \theta_0 + I_1 \operatorname{cosec} \theta_0 + A \sin \theta_0} - \cos \theta_0 \dot{\phi}_0 \right) x = C \omega_3 y$$

This is SHM at frequency p

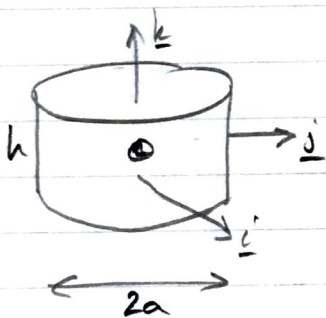
$$\ddot{x} + \underbrace{\left(\frac{C \omega_3}{A} \right)^2 \frac{A \sin \theta_0}{J_1 \cos \theta_0 \cot \theta_0 + I_1 \operatorname{cosec} \theta_0 + A \sin \theta_0}}_{p^2} x = \text{const}$$

$$p^2 = \left(\frac{C \omega_3}{A} \right)^2 \left[\frac{J_1}{A} \cot^2 \theta_0 + \frac{I_1}{A} \operatorname{cosec}^2 \theta_0 + 1 \right]^{-1}$$

$$\therefore p = \frac{C \omega_3}{A} \left[1 + \frac{J_1}{A} \cot^2 \theta_0 + \frac{I_1}{A} \operatorname{cosec}^2 \theta_0 \right]^{-1/2} \quad \underline{\underline{Q.E.D}}$$

②

a)

About G: $I_{zz} = \frac{1}{2}ma^2$

$$I_{xx} = I_{yy} = \left(\frac{a^2}{4} + \frac{h^2}{12}\right)m$$

$$\therefore \text{'AAA'} \Rightarrow \frac{a^2}{4} + \frac{h^2}{12} = \frac{a^2}{2} \quad \therefore h = a\sqrt{3}$$

b) No slip at P $\Rightarrow \underline{\omega} \times (a\underline{i} - \frac{h}{2}\underline{k}) = 0$.

(i)

$$\text{i.e. } \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ \omega_1 & \omega_2 & \omega_3 \\ a & 0 & -h/2 \end{vmatrix} = \underline{i}(-\frac{h}{2}\omega_2) - \underline{j}(-\frac{h}{2}\omega_1 - a\omega_3) + \underline{k}(a\omega_2) = 0$$

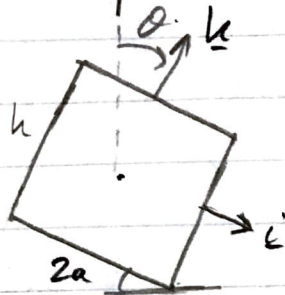
$$\Rightarrow -\frac{h}{2}\omega_2 \underline{i} + (\frac{h}{2}\omega_1 + a\omega_3) \underline{j} - a\omega_2 \underline{k} = 0$$

$$\therefore \omega_2 = 0 \text{ and } \omega_3 = -\frac{h}{2a}\omega_1$$

Δ

$$A-C = \frac{15}{4}ma^2 \therefore \dot{\varphi}^2 \geq 8 \times g \cdot \frac{3\sqrt{3}a}{4} \cdot \frac{15}{4} \mu a^2 \cdot \frac{36}{m^2 a^4} = 810\sqrt{3} \frac{g}{a} \Rightarrow \dot{\varphi} \geq 37.46 \sqrt{\frac{g}{a}}$$

(2) b) Cont. $\uparrow \ddot{\phi}$



$$\omega_1 = -\Omega_1 = -\dot{\phi} \sin \theta$$

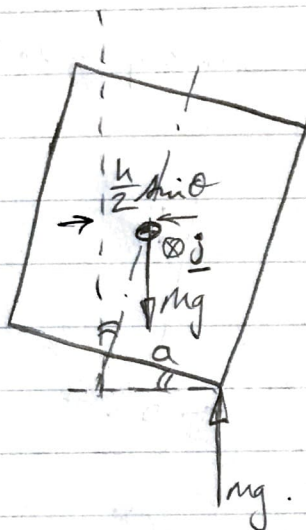
$$\omega_2 = -\Omega_2 = \dot{\theta}$$

$$\Omega_3 = \dot{\phi} \cos \theta$$

$$\therefore \text{no slip} \Rightarrow \omega_3 = -\frac{h}{2a} (-\dot{\phi} \sin \theta)$$

$$= \frac{h}{2a} \dot{\phi} \sin \theta$$

(ii)



$$Q_2 = -mg(a \cos \theta - \frac{h}{2} \sin \theta)$$

$$= mg(\frac{h}{2} \sin \theta - a \cos \theta)$$

(iii) $Q_2 = A \dot{\Omega}_2 + (A \Omega_3 - C \omega_3) \Omega_1$, $\dot{\Omega}_2 = 0$ and 'AAA' body

$$\therefore mg(\frac{h}{2} \sin \theta - a \cos \theta) = (A \dot{\phi} \cos \theta - A \frac{h}{2a} \dot{\phi} \sin \theta)(-\dot{\phi} \sin \theta)$$

$$mg \frac{h}{2} \sin \theta - mga \cos \theta = -A \dot{\phi}^2 \sin \theta \cos \theta + \frac{Ah}{2a} \dot{\phi}^2 \sin^2 \theta$$

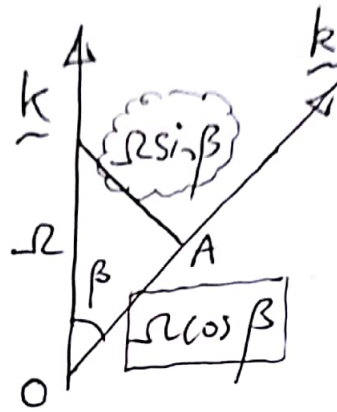
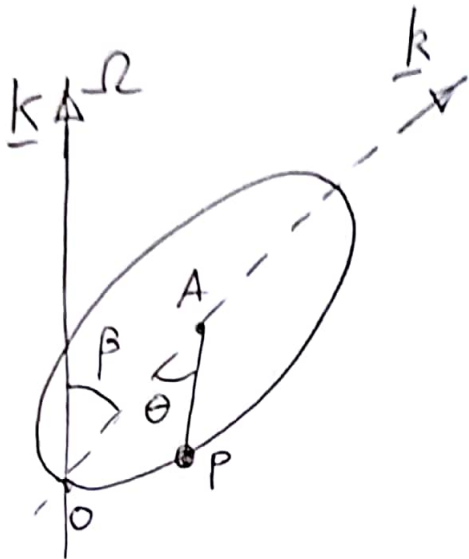
$$mg \frac{h}{2} \sin \theta - 2mga^2 \cos \theta = -2aA \dot{\phi}^2 \sin \theta \cos \theta + Ah \dot{\phi}^2 \sin^2 \theta$$

$$mga(h \sin \theta - 2a \cos \theta) = A \dot{\phi}^2 \sin \theta (h \sin \theta - 2a \cos \theta)$$

$$\Rightarrow \dot{\phi}^2 = \frac{mga}{A \sin \theta}$$

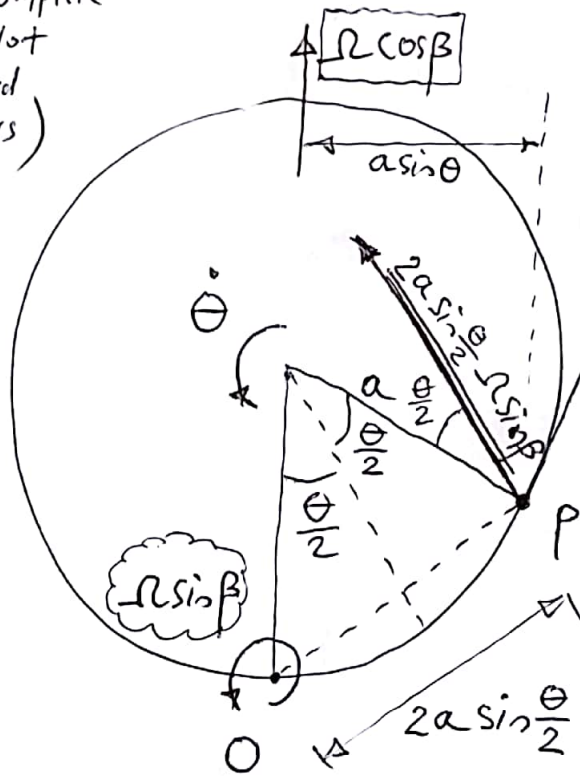
$$\text{But } A = \frac{1}{2} ma^2 \therefore \dot{\phi}^2 = \frac{2g}{a \sin \theta}$$

3(a)



resolve Ω into Ω & out of plane of ring

(Note: This solution is for a complete treatment. Not all is required for full marks (eg page 4))



Double-underlined are the velocity components of P due to Ω & $\dot{\theta}$

$a \sin \theta \Omega \cos \beta$ into page

True view of ring

The three velocity components of P in an orthogonal set are

$$a[\dot{\theta} + \Omega \sin \beta (1 - \cos \theta)] \uparrow$$

$$a \Omega \sin \beta \sin \theta \leftarrow$$

$$a \Omega \cos \beta \sin \theta \cdot \text{into page}$$

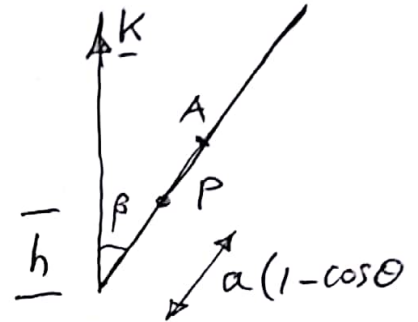
$$\begin{aligned} & 2a \sin \frac{\theta}{2} \Omega \sin \beta \\ & = a \Omega \sin \beta 2 \sin \frac{\theta}{2} \cos \frac{\theta}{2} \\ & = a \Omega \sin \beta \left(\frac{1 - \cos \theta}{\sin \theta} \right) \sin \theta \\ & = a \Omega \sin \beta (1 - \cos \theta) \end{aligned}$$

$$\therefore T = \frac{1}{2} m a^2 \left[\Omega^2 \sin^2 \beta \sin^2 \theta + \Omega^2 \cos^2 \beta \sin^2 \theta + (\dot{\theta} + \Omega \sin \beta (1 - \cos \theta))^2 \right]$$

$$= \frac{1}{2} m a^2 \left[\Omega^2 \sin^2 \theta + (\dot{\theta} + \Omega \sin \beta (1 - \cos \theta))^2 \right]$$

$$\& V = m g h$$

$$= m g a (1 - \cos \theta) \cos \beta$$



$$\frac{\partial T}{\partial \dot{\theta}} = m a^2 (\dot{\theta} + \Omega \sin \beta (1 - \cos \theta))$$

$$\frac{\partial T}{\partial \theta} = m a^2 \left(\Omega^2 \sin \theta \cos \theta + (\dot{\theta} + \Omega \sin \beta (1 - \cos \theta)) \Omega \sin \beta \sin \theta \right)$$

$$= m a^2 \left(\Omega^2 \sin \theta \cos \theta + \dot{\theta} \Omega \sin \beta + \Omega^2 \sin^2 \beta (1 - \cos \theta) \right)$$

$$= m a^2 \sin \theta \left(\Omega^2 [\cos \theta (1 - \sin^2 \beta) + \sin^2 \beta] + \dot{\theta} \Omega \sin \beta \right)$$

$$= m a^2 \Omega \sin \theta \left(\Omega (\cos \theta \cos^2 \beta + \sin^2 \beta) + \dot{\theta} \sin \beta \right)$$

$$\frac{\partial V}{\partial \theta} = m g a \sin \theta \cos \beta$$

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{\theta}} \right) - \frac{\partial T}{\partial \theta} + \frac{\partial V}{\partial \theta} = 0 \quad (\text{Lagrange})$$

$$\therefore \ddot{\theta} + \Omega \sin \beta \dot{\theta} \sin \theta - \Omega \sin \beta \dot{\theta} \sin \theta - \Omega^2 \sin \theta (\cos \theta \cos^2 \beta + \sin^2 \beta) + \frac{g}{a} \sin \theta \cos \beta = 0$$

$$\therefore \ddot{\theta} + \left[\frac{g}{a} \cos \beta - \Omega^2 (\cos \theta \cos^2 \beta + \sin^2 \beta) \right] \sin \theta = 0$$

NB put $\beta = 0$

$$\therefore \ddot{\theta} + \left[\frac{g}{a} - \Omega^2 \cos \theta \right] \sin \theta = 0$$

as in IB Mechanics examples paper

For steady state solutions put $\ddot{\theta} = 0$

$$\therefore \left[\frac{g}{a} \cos \beta - \Omega^2 (\cos \theta \cos^2 \beta + \sin^2 \beta) \right] \sin \theta = 0$$

$$\therefore \sin \theta = 0 \quad \text{if } \boxed{\theta = 0} \text{ or } \textcircled{1}$$

$$\boxed{\theta = \pi} \text{ or } \textcircled{2}$$

$$\text{or } \frac{g}{a} \cos \beta - \Omega^2 (\cos \theta \cos^2 \beta + \sin^2 \beta) = 0$$

$$\therefore \cos \theta = \left(\frac{g \cos \beta}{a \Omega^2} - \sin^2 \beta \right) \frac{1}{\cos^2 \beta}$$

$$\boxed{\cos \theta = \frac{g}{a \Omega^2 \cos \beta} - \tan^2 \beta} \textcircled{3} \text{ only exists if } \cos \theta \leq 1$$

$$\therefore \frac{g}{a \Omega^2 \cos \beta} - \tan^2 \beta \leq 1 \quad \therefore \frac{g \cos \beta}{a \Omega^2} \leq 1$$

Check for stability

$$\textcircled{1} \theta_0 = 0 \quad \therefore \text{put } \theta \text{ small} \quad \begin{array}{l} \sin \theta \approx \theta \\ \cos \theta \approx 1 \end{array}$$

$$\ddot{\theta} + \left[\frac{g}{a} \cos \beta - \Omega^2 (\cos^2 \beta + \sin^2 \beta) \right] \theta = 0$$

$$\therefore \ddot{\theta} + \left[\frac{g}{a} \cos \beta - \Omega^2 \right] \theta = 0$$

$$\text{only stable if } \frac{g \cos \beta}{a \Omega^2} > 1$$

unstable otherwise

$$\text{note that solution } \textcircled{3} \text{ exists for } \frac{g \cos \beta}{a \Omega^2} \leq 1$$

$$\text{or } \Omega^2 \geq \frac{g \cos \beta}{a}$$

② $\Theta_0 = \pi$ put $\Theta = \pi + x$ with small x

$$\sin \Theta = -\sin x \approx -x$$

$$\cos \Theta \approx -1$$

$$\ddot{x} + \left[\frac{g}{a} \cos \beta - \Omega^2 (-\cos^2 \beta + \sin^2 \beta) \right] (-x) = 0$$

$$\therefore \ddot{x} + \left[\frac{g}{a} \cos \beta + \cos 2\beta \right] x = 0$$

always unstable

③ $\cos \Theta_0 = \frac{g}{a \Omega^2 \cos \beta} - \tan^2 \beta$

put $\Theta = \Theta_0 + x$

$$\begin{aligned} \sin \Theta &= \sin \Theta_0 \cos x + \cos \Theta_0 \sin x \\ &= \sin \Theta_0 + x \cos \Theta_0 \end{aligned}$$

$$\begin{aligned} \cos \Theta &= \cos \Theta_0 \cos x - \sin \Theta_0 \sin x \\ &= \cos \Theta_0 - x \sin \Theta_0 \end{aligned}$$

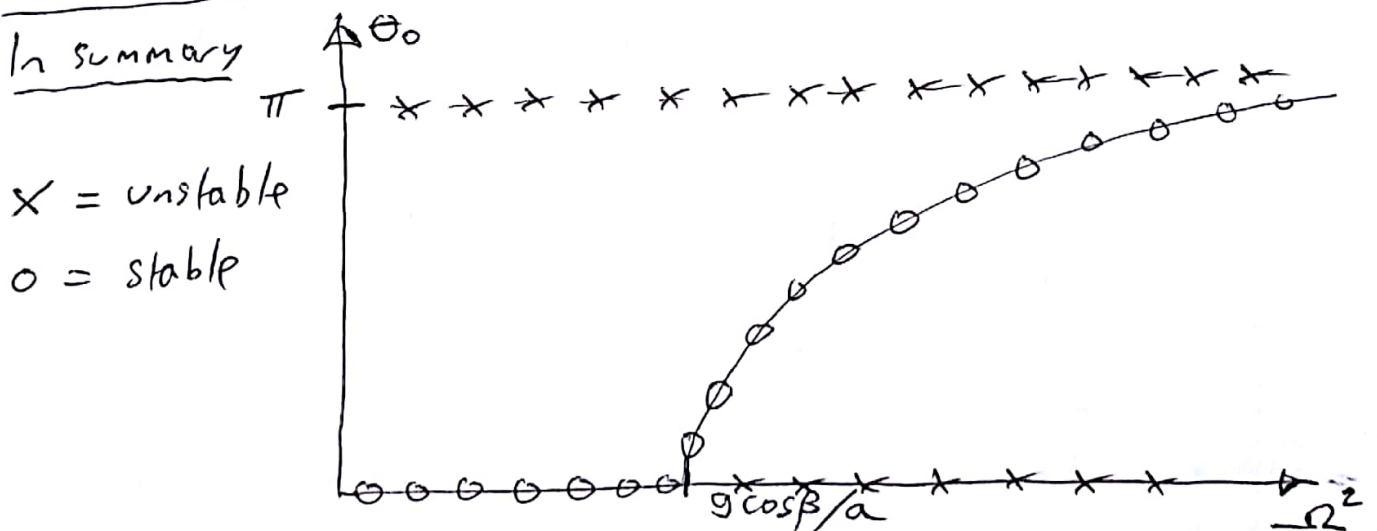
$$\therefore \ddot{x} + \left[\frac{g}{a} \cos \beta - \Omega^2 \left[(\cos \Theta_0 - x \sin \Theta_0) \cos^2 \beta + \sin^2 \beta \right] \right] \left[\sin \Theta_0 + x \cos \Theta_0 \right] = 0$$

$$\therefore \ddot{x} + \left[\frac{g}{a} \cos \beta - \Omega^2 (\cos \Theta_0 \cos^2 \beta + \sin^2 \beta) \right] \left[\sin \Theta_0 + x \cos \Theta_0 \right] + \Omega^2 x \sin \Theta_0 \cos^2 \beta \sin \Theta_0 = 0$$

$$\therefore \ddot{x} + \Omega^2 \sin^2 \Theta_0 \cos^2 \beta x = 0$$

always stable

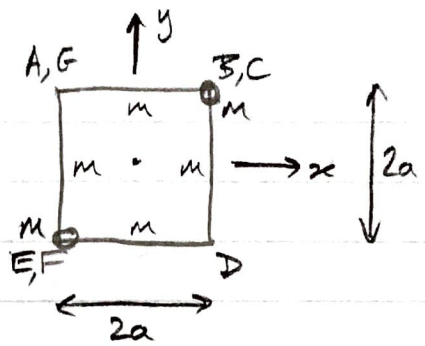
In summary



x = unstable

o = stable

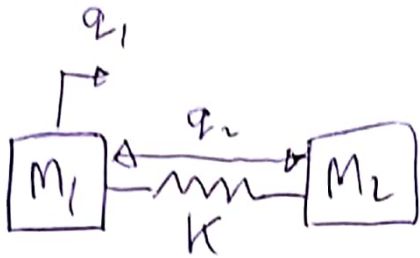
4) a). Top view (down z-axis)



$$\begin{aligned} I_{zz} &= 4 \left(\frac{1}{3} ma^2 + ma^2 \right) + 2 \left(m(a\sqrt{2})^2 \right) \\ &\quad \text{'rods'} \qquad \qquad \qquad \text{'equivalent masses'} \\ &= \frac{16}{3} ma^2 + 4ma^2 \\ &= \frac{28}{3} ma^2 \end{aligned}$$

$$I_{xy} = \int xy \, dm = 2ma^2 \quad (\text{only equivalent masses contribute}).$$

4b)



$$T = \frac{1}{2} M_1 \dot{q}_1^2 + \frac{1}{2} M_2 (\dot{q}_1 + \dot{q}_2)^2$$

$$V = \frac{1}{2} k q_2^2$$

$$p_1 = \frac{\partial T}{\partial \dot{q}_1} = M_1 \dot{q}_1 + M_2 (\dot{q}_1 + \dot{q}_2)$$

$$p_2 = \frac{\partial T}{\partial \dot{q}_2} = M_2 (\dot{q}_1 + \dot{q}_2) \quad \therefore (\dot{q}_1 + \dot{q}_2) = \frac{p_2}{M_2}$$

$$\dot{q}_2 = \frac{p_2}{M_2} - \frac{p_1 - p_2}{M_1}$$

$$p_1 = M_1 \dot{q}_1 + p_2 \quad \therefore \dot{q}_1 = \frac{p_1 - p_2}{M_1}$$

$$\therefore T = \frac{1}{2} M_1 \left(\frac{p_1 - p_2}{M_1} \right)^2 + \frac{1}{2} M_2 \left(\frac{p_2}{M_2} \right)^2$$

$$= \frac{1}{2} \frac{(p_1 - p_2)^2}{M_1} + \frac{1}{2} \frac{p_2^2}{M_2}$$

$$H = \dot{q}_1 \frac{p_1 - p_2}{M_1} + p_2 \left(\frac{p_2}{M_2} - \frac{p_1 - p_2}{M_1} \right) - \frac{1}{2} \frac{(p_1 - p_2)^2}{M_1} - \frac{1}{2} \frac{p_2^2}{M_2} + \frac{1}{2} k q_2^2$$

$$= \frac{(p_1 - p_2)(p_1 - p_2)}{M_1} + \frac{p_2^2}{M_2} - \frac{1}{2} \frac{p_2^2}{M_2} - \frac{1}{2} \frac{(p_1 - p_2)^2}{M_1} + \frac{1}{2} k q_2^2$$

$$= \frac{p_1^2 - p_2^2}{M_1} + \frac{p_2^2}{M_2} - \frac{1}{2} \frac{p_2^2}{M_2} - \frac{1}{2} \frac{(p_1 - p_2)^2}{M_1} + \frac{1}{2} k q_2^2$$

$$\dot{q}_1 = \frac{\partial H}{\partial p_1} = \frac{2p_1}{M_1} - \frac{p_1 - p_2}{M_1} = \frac{p_1 + p_2}{M_1} \quad \checkmark$$

$$\dot{q}_2 = \frac{\partial H}{\partial p_2} = \frac{2p_2}{M_2} - \frac{p_1 - p_2}{M_1} = \frac{2p_2}{M_2} - \frac{p_1}{M_1} + \frac{p_2}{M_1} \quad \checkmark$$

4b cont.

$$\dot{p}_1 = -\frac{\delta H}{\delta q_1} = 0$$

$$\dot{p}_2 = -\frac{\delta H}{\delta q_2} = -kq_2$$

$$H = \frac{1}{2} [p_1 \ p_2] \begin{bmatrix} M_1+M_2 & M_2 \\ M_2 & M_2 \end{bmatrix}^{-1} \begin{bmatrix} p_1 \\ p_2 \end{bmatrix} + \frac{1}{2} k q_2^2$$

$$= \frac{1}{2\Delta} (p_1 \ p_2) \begin{bmatrix} M_2 & -M_2 \\ -M_2 & M_1+M_2 \end{bmatrix} \begin{bmatrix} p_1 \\ p_2 \end{bmatrix} + \frac{1}{2} k q_2^2$$

$$= \frac{1}{2\Delta} (p_1 \ p_2) \begin{bmatrix} M_2 p_1 & -M_2 p_2 \\ -M_2 p_1 & (M_1+M_2) p_2 \end{bmatrix} + \dots$$

$$= \frac{1}{2\Delta} (p_1 (M_2 p_1 - M_2 p_2) + p_2 (-M_2 p_1 + (M_1+M_2) p_2))$$

$$= \frac{1}{2\Delta} \frac{-2p_1 M_2 p_2 + p_1^2 M_2 + p_2^2 (M_1+M_2)}{(M_1+M_2) M_2 - M_2^2}$$

$$\neq M_1 M_2$$

$$\neq \frac{1}{2} = \frac{1}{2} \left(\frac{(p_1 - p_2)^2}{M_1} + \frac{1}{2} \frac{p_2^2}{M_2} \right) \quad \checkmark$$