

EGT2  
ENGINEERING TRIPOS PART IIA

---

Tuesday 25 April 2023 2 to 3.40

---

**Module 3C8**

**MACHINE DESIGN**

*Answer not more than **three** questions.*

*All questions carry the same number of marks.*

*The **approximate** percentage of marks allocated to each part of a question is indicated in the right margin.*

*Write your candidate number **not** your name on the cover sheet.*

**STATIONERY REQUIREMENTS**

Single-sided script paper

**SPECIAL REQUIREMENTS TO BE SUPPLIED FOR THIS EXAM**

CUED approved calculator allowed

Attachment: 3C8 Machine Design data sheet (9 pages).

Engineering Data Book

**10 minutes reading time is allowed for this paper at the start of the exam.**

**You may not start to read the questions printed on the subsequent pages of this question paper until instructed to do so.**

**You may not remove any stationery from the Examination Room.**

1 Figure 1 shows a flywheel connected rigidly to shaft A. Sphere A can slide freely along shaft A, but splines in the sphere and on the shaft ensure they rotate together. Shaft B and sphere B are also splined together. Shafts A and B are supported by bearings (not shown). The shafts are in the same plane and perpendicular to each other. The angle  $\alpha$  of the line passing through the centres of the two spheres can be varied. The two spheres are made of steel and each has radius  $R = 50$  mm. A cage, spring and bearing arrangement (not shown) acts between the centres of the spheres and provides a normal contact force  $N$  between the two spheres. The contact between the spheres is Hertzian with contact modulus  $E^* = 115$  GPa.

- (a) Describe how this system might be used to reduce the fuel consumption of a vehicle powered by an internal combustion engine. [15%]
- (b) Assuming no slip at the contact, derive expressions for the following:
- (i) the entraining velocity magnitude at the contact in terms of  $\omega_B$ ,  $R$  and  $\alpha$ ; [10%]
  - (ii) the ratio of the shaft angular speeds  $\omega_A/\omega_B$  in terms of  $\alpha$ ; [10%]
  - (iii) the spin speed at the contact in terms of  $\omega_B$  and  $\alpha$ . [15%]
- (c) If  $\alpha = 25^\circ$  and  $N = 400$  N, and assuming that the transmitted torque is 25% of the limiting value, determine the efficiency of power transmission from shaft B to shaft A, making clear which information from the data sheet is used. [40%]
- (d) Sketch a possible cage, spring and bearing arrangement that could provide the normal contact force  $N$  between the two spheres. [10%]

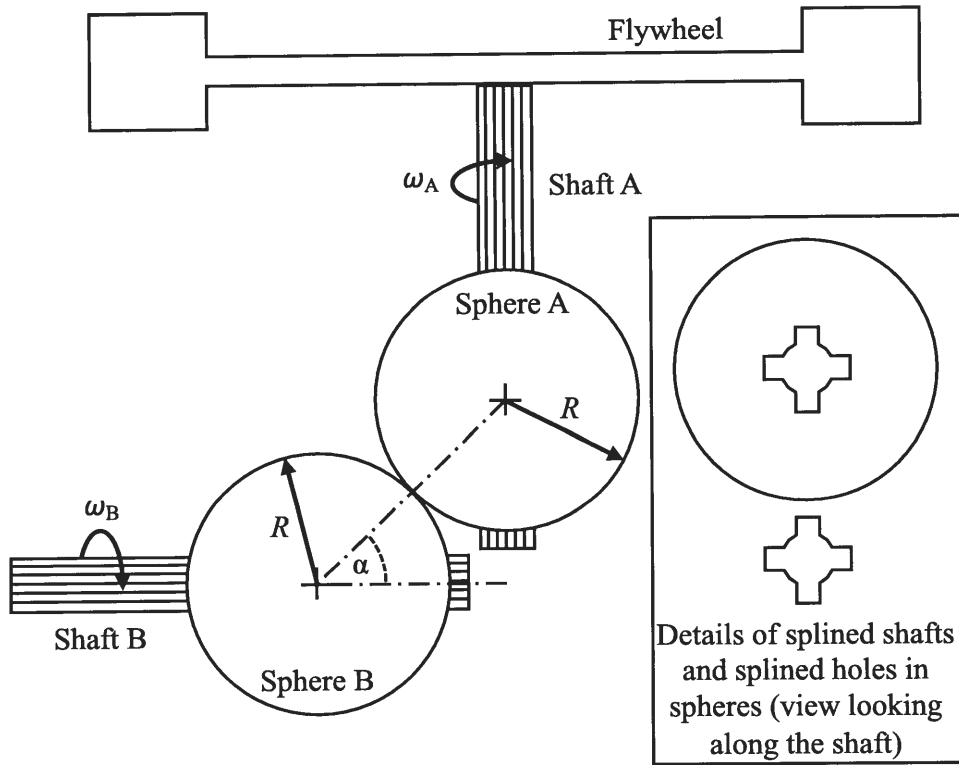


Fig. 1

2 Figure 2 shows a schematic of a compound epicyclic gear system. The input, with speed  $\omega_i$  and torque  $T_i$ , is to the carrier C1. The output, with speed  $\omega_o$ , is from the sun S2. Annulus A1 is fixed, annulus A2 is connected to carrier C1, and sun S1 is connected to carrier C2. The ratios of annulus to sun tooth numbers for the two epicyclics are given by  $R_1$  and  $R_2$ .

(a) Find an expression for the speed ratio  $\omega_o/\omega_i$  in terms of  $R_1$  and  $R_2$ . [30%]

(b) Find an expression for the torque transmitted from S1 to C2 in terms of  $R_1$ ,  $R_2$  and the input torque  $T_i$ . Identify carefully the sign convention used to define the direction of the torque. [30%]

(c) Each carrier has three planet wheels. Each planet wheel is attached to its carrier by two identical cylindrical roller bearings, arranged so that the radial load is shared equally between the two bearings. The annulus to sun tooth ratios are  $R_1 = R_2 = 3$ , input power is 19 kW, input speed  $\omega_i = 1 \text{ rad s}^{-1}$ , pitch circle diameter of A2 is 300 mm. Calculate the required dynamic load rating of a cylindrical roller bearing for a C2 planet wheel that would give a life of two years of continuous operation with 1% probability of failure. No adjustment for oil viscosity is required. Neglect inertial and gravitational forces. [40%]

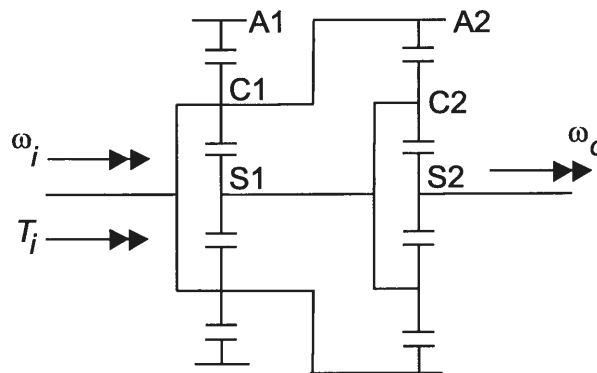


Fig. 2

3 Consider a pair of meshing steel involute spur gears with tooth numbers 25 and 75 and contact modulus  $E^* = 115$  GPa. The nominal pressure angle is  $20^\circ$  and the addendum equals the module. The module of the teeth is 3 mm and the facewidth is 10 mm. The gears are not accurately made, so that load sharing between tooth contacts cannot be assumed.

(a) Find the allowable torque on the smaller gear to avoid failure due to:

(i) tooth fatigue due to bending, with a failure stress of 300 MPa; [15%]

(ii) surface fatigue, with a failure stress of 1100 MPa. [40%]

(b) The centre-to-centre distance of the gears is increased by 0.5 mm from the value corresponding to the nominal pressure angle of  $20^\circ$ .

(i) What is the new pressure angle? [20%]

(ii) Estimate the corresponding percentage change in the allowable torque associated with surface fatigue, as calculated in part (a)(ii). [25%]

4 Figure 3 shows the drive arrangement of a hybrid vehicle. An internal combustion engine drives the carrier of a planetary gearbox, and an electrical motor/generator is connected to the sun wheel which has 20 teeth. The wheels of the car are driven from the annulus, which has 90 teeth, via a speed reduction gear such that the speed of the annulus is 5 times the speed of the wheels. The power output characteristic of the engine is shown in Fig. 4. The vehicle's wheels have a rolling radius of 0.35 m and the load characteristic of the vehicle travelling at constant speed on level ground is  $F = 150 + 0.3V^2$  where  $F$  is the force in Newtons resisting motion and  $V$  is the speed of the vehicle in  $\text{m s}^{-1}$ . By controlling the speed of the motor/generator the speed ratio between the engine and wheels can be adjusted continuously. The motor/generator also allows the storage and retrieval of energy in an electrical battery (not shown).

(a) Determine the ratio of the torque on the annulus to the torque on the carrier, and the ratio of the torque on the sun to the torque on the carrier. State your sign convention clearly. [25%]

(b) Explain why the maximum speed of the vehicle is achieved when the engine operates at maximum torque and not at maximum power. Calculate the maximum speed of the vehicle. [25%]

(c) The engine and motor/generator are controlled to cause the vehicle to accelerate at the maximum rate possible from zero to maximum vehicle speed. Sketch graphs as specified in (i) and (ii) below. Annotate the graphs with salient values. The signs of all quantities, and the corresponding sign conventions, should be stated clearly.

(i) A graph of the speeds of the planetary gearbox (carrier, annulus and sun) as a function of vehicle speed. [25%]

(ii) Graphs of the torque and power of the motor/generator as a function of vehicle speed. [25%]

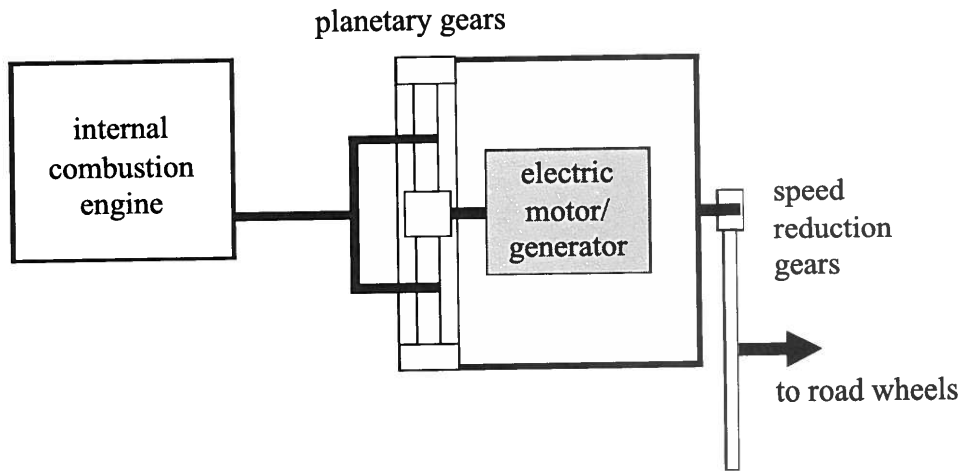


Fig. 3

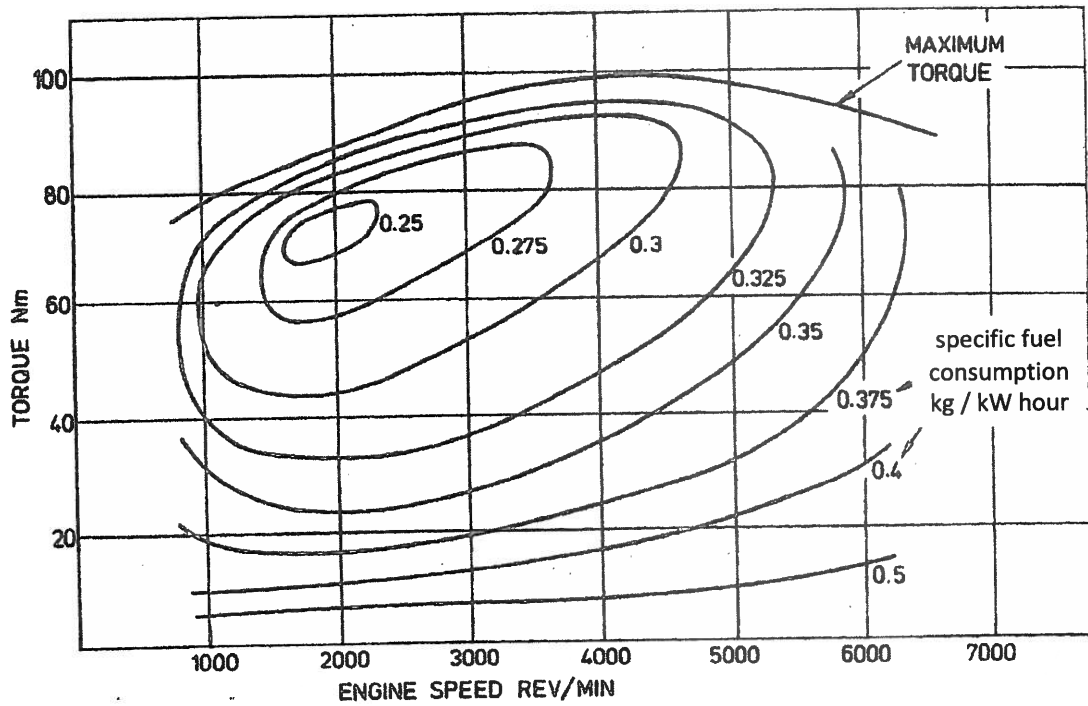


Fig. 4

**END OF PAPER**

Version DJC/5

**THIS PAGE IS BLANK**



# ENGINEERING TRIPOS Part IIA

## Module 3C8 Data Sheet

### ELASTIC CONTACT STRESS FORMULAE

Suffixes 1, 2 refer to the two bodies in contact.

$$\text{Effective curvature } \frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$$

$$\text{Contact modulus } \frac{1}{E^*} = \frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2}$$

where  $R_1, R_2$  are the radii of curvature of the two bodies (convex positive).

where  $E_1, E_2$  and  $\nu_1, \nu_2$  are Young's moduli and Poisson's ratios

	<u>Line contact</u> width $2b$ ; load $P'$ per unit length	<u>Circular contact</u> diameter $2a$ ; load $P$
Semi contact width or contact radius	$b = 2 \left\{ \frac{P'R}{\pi E^*} \right\}^{1/2}$	$a = \left\{ \frac{3PR}{4E^*} \right\}^{1/3}$
Maximum contact pressure ('Hertz stress')	$p_0 = \left\{ \frac{P'E^*}{\pi R} \right\}^{1/2}$	$p_0 = \frac{1}{\pi} \left\{ \frac{6PE^{*2}}{R^2} \right\}^{1/3}$
Approach of centres	$\delta = \frac{2P'}{\pi} \left[ \frac{1-\nu_1^2}{E_1} \left\{ \ln \left( \frac{4R_1}{b} \right) - \frac{1}{2} \right\} + \frac{1-\nu_2^2}{E_2} \left\{ \ln \left( \frac{4R_2}{b} \right) - \frac{1}{2} \right\} \right]$	$\delta = \frac{a^2}{R} = \frac{1}{2} \left\{ \frac{9}{2} \frac{P^2}{E^{*2} R} \right\}^{1/3}$
Mean contact pressure	$\bar{p} = \frac{P'}{2b} = \frac{\pi}{4} p_0$	$\bar{p} = \frac{P}{\pi a^2} = \frac{2}{3} p_0$
	$\tau_{\max} = 0.300 p_0$ at $x = 0, z = 0.79b$	$\tau_{\max} = 0.310 p_0$ at $r = 0, z = 0.48a$ for $\nu = 0.3$
Maximum tensile stress	zero	$\frac{1}{3}(1-2\nu)p_0$ at $r = a, z = 0$

#### Mildly elliptical contacts

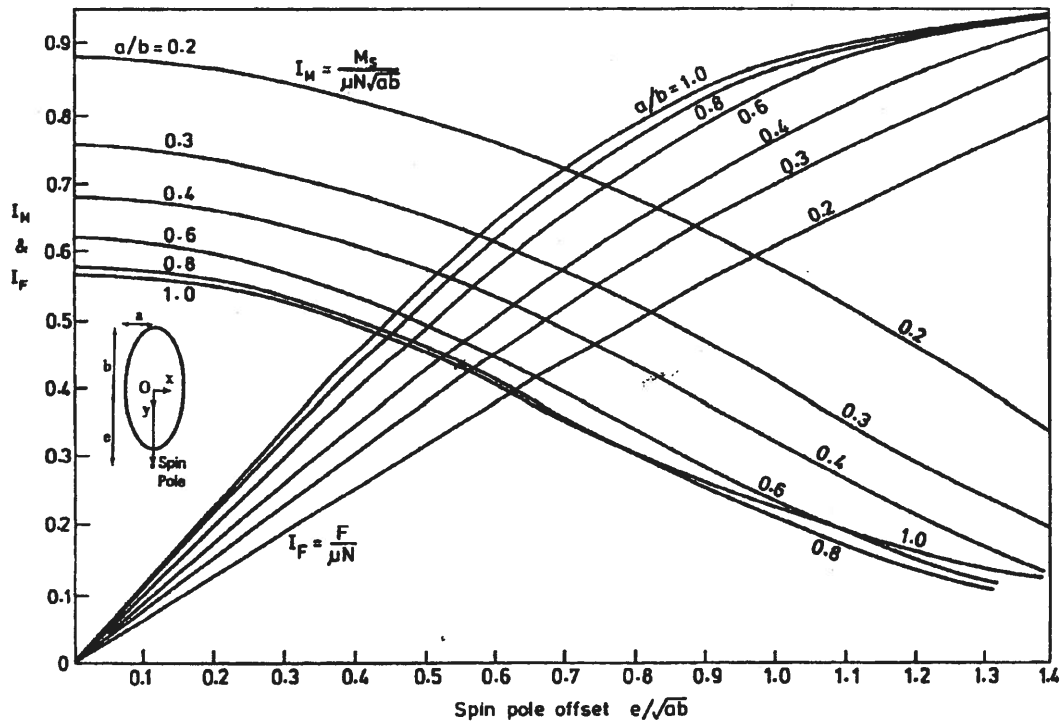
If the gap at zero load is  $h = \frac{1}{2}Ax^2 + \frac{1}{2}By^2$  and  $0.2 < A/B < 5$  then

ratio of semi-axes  $b/a \cong (A/B)^{2/3}$

To calculate the contact area or Hertz stress use the circular contact equations with  $R = (AB)^{-1/2}$  or better  $R_c = [AB(A+B)/2]^{-1/3}$ .

For approach use circular contact equation with  $R = (AB)^{-1/2}$  (not  $R_c$ )

Hertzian contact frictional losses



**INVOLUTE GEARING**

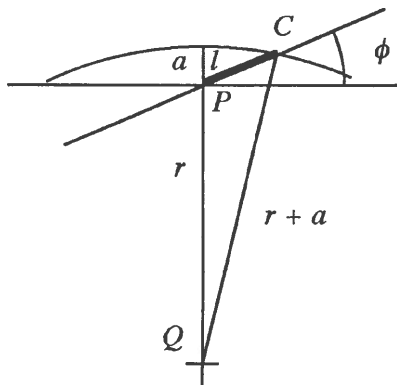
Spur gears

pitch cylinder radii  $r$   
 base cylinder radii  $r_b$   
 addendum cylinder radii  $r_a$   
 number of teeth  $N$   
 addendum  $a = r_a - r$   
 pressure angle  $\phi$

} with suffix 1 or 2

circumferential pitch  $p = 2\pi r/N$   
 base pitch  $p_b = p \cos \phi$   
 module  $m = p/\pi = 2r/N$   
 ratio of contact  $r_c$   
 radius of curvature at pitch point  $\rho = r \sin \phi$

Path of contact



$$l = \{r^2 \sin^2 \phi + a(2r + a)\}^{1/2} - r \sin \phi$$

For a standard 20° spur wheel with  $N$  teeth of module  $m$  this becomes

$$\frac{l}{m} = (0.02924N^2 + N + 1)^{1/2} - 0.1710N$$

### Standard tooth forms

Addendum  $a = m$ , Dedendum  $= \frac{7}{6}m$ , pressure angle  $= 20^\circ$ .

Modules:	0.3 – 1.0 mm in 0.1 mm steps
1.0 – 4.0 mm in 0.25 mm steps	4.0 – 7.0 mm in 0.5 mm steps
7.0 – 16.0 mm in 1.0 mm steps	16.0 – 24.0 mm in 2.0 mm steps
24.0 – 45.0 mm in 3.0 mm steps	45.0 – 75.0 mm in 5.0 mm steps

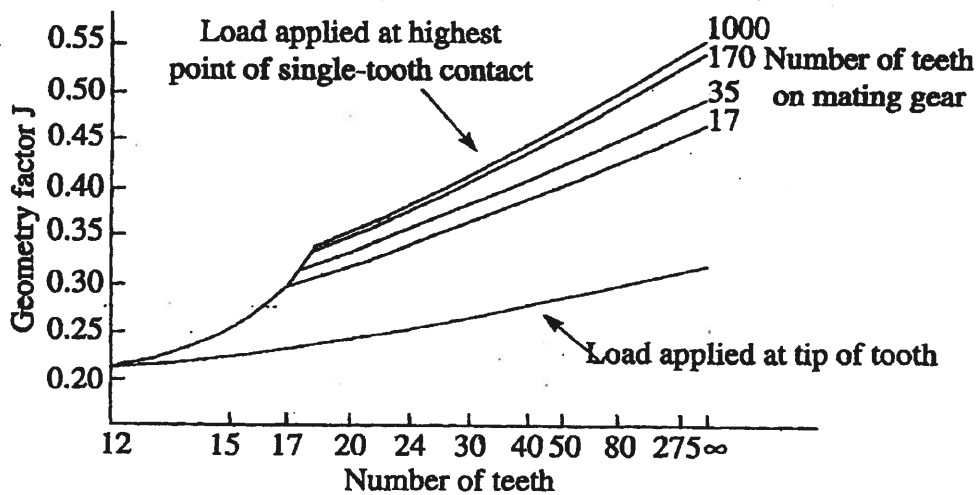
### Friction in spur gears

$$\frac{\text{average friction loss}}{\text{power transmitted}} \approx \mu\pi \left\{ \frac{1}{N_1} + \frac{1}{N_2} \right\}$$

### Tooth failure

Allowable bending stress  $\sigma_b$  according to AGMA guidelines given by  $\sigma_b = \frac{P_T'}{Jm}$

where  $P_T'$  is force per unit face-width acting tangentially to pitch circle and  $J$  given in the figure below for  $20^\circ$  spur gears. Typical values of  $\sigma_b$  shown in table.



### Typical allowable tooth stresses (AGMA)

Material	Condition	Bending fatigue strength $\sigma_b$ (MPa)	Surface fatigue strength $\sigma_s$ (MPa)
Steel	Through hardened and tempered	170-390	590-1200
	Carburised and case hardened	380-480	1250-1550
Cast iron	As cast	69-90	450-590
Nodular iron	Quenched, annealed and tempered	150-300	500-800
Malleable iron	Pearlitic	70-145	500-650

**EPICYCLIC SPEED RULE**

$$\omega_s = (1 + R)\omega_c - R\omega_a \quad \text{where } R = \frac{A}{S}$$

**ROLLING ELEMENT BEARINGS**Fatigue life

$$L = a_1 a_2 a_3 (C/P)^p \quad p = 3 \text{ for ball and } 10/3 \text{ for roller bearings}$$

Fatigue probability %	10	5	4	3	2	1
Life adjust factor $a_1$	1	0.62	0.53	0.44	0.33	0.21

Bearing choice

The information on the following pages concerning loads, viscosities and standard bearing sizes and ratings is extracted from the SKF General Bearing Catalogue and is copied with permission. It is SKF copyright and is not to be further reproduced.

Required viscosities and the effect of viscosity ratio on  $a_{23}$

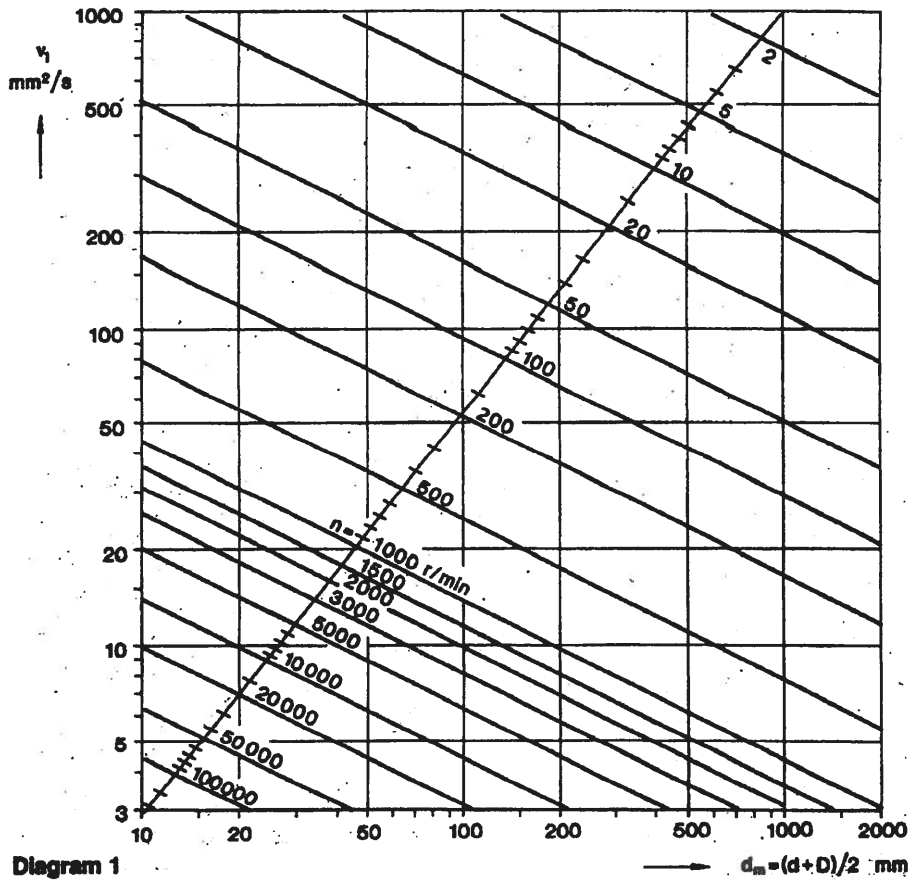


Diagram 1

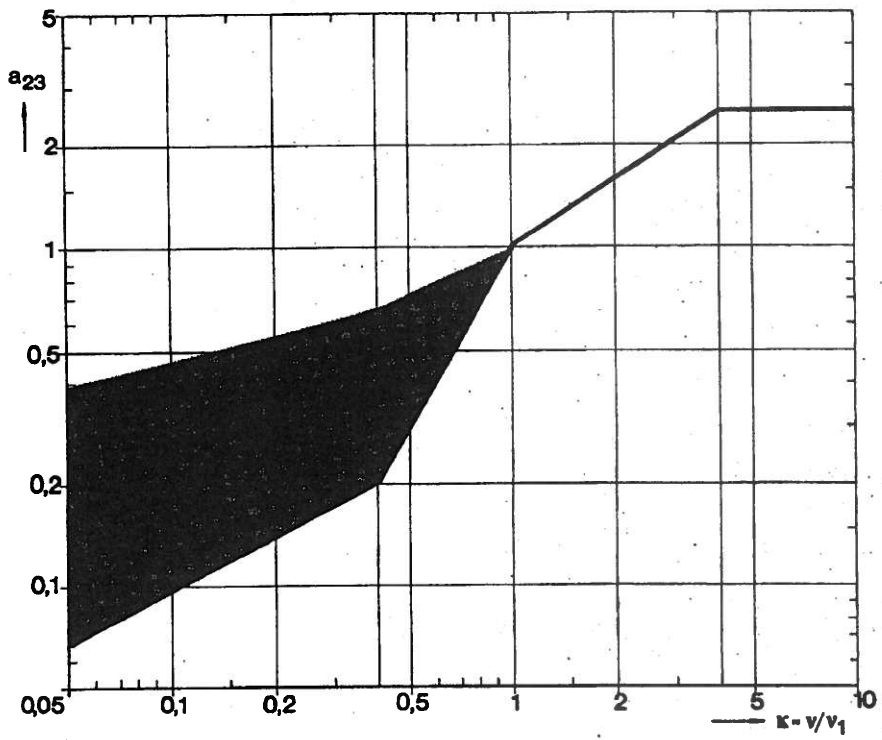
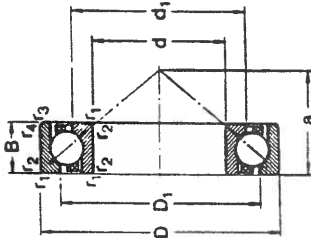
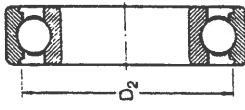
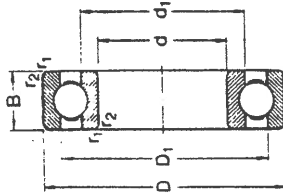


Diagram 3

**Angular contact ball bearings  
single row  
d 10-65 mm**



**Deep groove ball bearings  
single row  
d 35-55 mm**

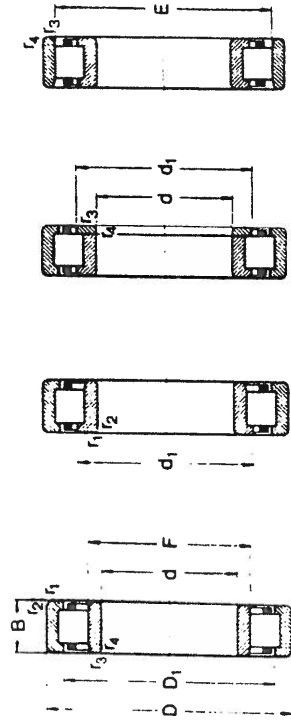


With full outer ring shoulders

With recessed outer ring shoulders

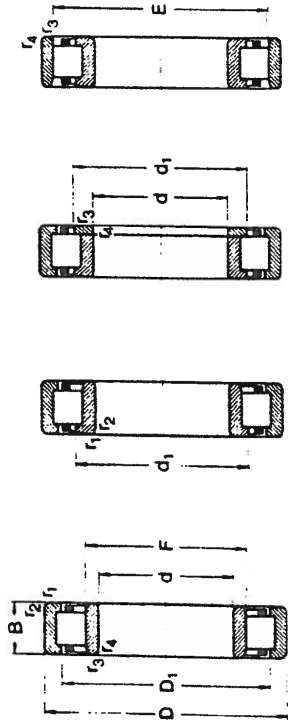
Principal dimensions	Basic load ratings			Fatigue load limit $P_u$	Speed ratings Lubrication grease oil	Mass	Designation	
	d	D	B					C
35	47	7	4.750	3.200	166	13 000	0.030	61807
	55	10	9.560	6.200	290	11 000	0.080	61907
	62	14	12.400	8.150	375	10 000	0.11	16907
	62	9	12.400	8.150	375	10 000	0.16	6007
	72	17	15.900	10.200	440	10 000	0.29	6207
	72	14	15.900	10.200	440	11 000	0.46	6307
	80	21	25.500	19.300	815	8 500	0.95	6407
	80	21	33.200	15 000	815	7 000	0.95	6407
	100	25	55.300	31 000	1 290	8 500	0.95	6407
40	52	7	4.940	3.450	186	11 000	0.034	61808
	52	7	4.940	3.450	186	10 000	0.12	61908
	62	12	13.800	9.300	425	10 000	0.13	18008
	68	9	13.300	9.150	440	9 500	0.19	6008
	68	15	16.800	11.600	490	8 500	0.37	6208
	80	18	30.700	19 000	800	8 000	0.63	6308
	80	23	41.000	24 000	1 020	7 500	0.63	6408
	90	23	41.000	24 000	1 020	6 700	1.25	6408
	110	27	63.700	36.500	1 530	8 000	1.25	6408
45	58	7	6.050	4.300	228	9 500	0.040	61809
	68	12	10.100	6.700	285	9 000	0.14	61909
	75	10	15.600	10.800	520	11 000	0.17	16009
	75	16	20.800	14.600	640	9 000	0.25	6009
	85	19	33.200	21.600	915	9 000	0.41	6209
	100	25	52.700	31.500	1 340	6 700	0.83	6309
	120	29	76.100	45.000	1 900	6 000	1.55	6409
50	65	7	6.240	4.750	250	9 000	0.052	61810
	72	12	14.600	10.400	500	8 500	0.14	61910
	80	10	16.300	11.400	560	10 000	0.18	16010
	80	16	21.600	16 000	710	8 500	0.26	6010
	90	20	35.100	23.200	980	7 000	0.46	6210
	110	27	61.800	38 000	1 600	6 300	1.05	6310
	130	31	87.100	52 000	2 200	5 300	1.90	6410
55	72	9	8.320	6.200	325	8 500	0.063	61811
	80	13	15.900	11 400	560	8 000	0.19	61911
	90	11	19.500	14 000	695	9 000	0.26	16011
	90	18	28.100	21 200	900	7 500	0.39	6011
	100	21	43.600	29 000	1 250	6 300	0.61	6211
	120	29	71.500	45 000	1 900	5 600	1.35	6311
	140	33	99.500	62 000	2 600	5 000	2.30	6411

Cylindrical roller bearings  
single row  
d 40-45 mm



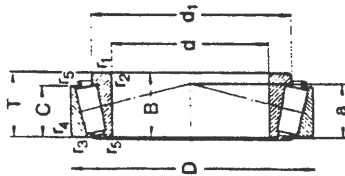
Principal dimensions d	Type NU				Type NUJ				Type NUP				Type N					
	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>		
40	90	23	80 900	78 000	10 200	6 700	8 000	8 000	8 000	0,65	-				-			
(cont.)	90	23	80 900	78 000	10 200	6 700	8 000	8 000	8 000	0,67	-				-			
	90	23	80 900	78 000	10 200	6 700	8 000	8 000	8 000	0,68	-				-			
	90	23	80 900	78 000	10 200	6 700	8 000	8 000	8 000	0,64	-				-			
	90	33	112 000	120 000	15 300	6 300	7 500	7 500	7 500	0,94	-				-			
	90	33	112 000	120 000	15 300	6 300	7 500	7 500	7 500	0,96	-				-			
	90	33	112 000	120 000	15 300	6 300	7 500	7 500	7 500	0,98	-				-			
	110	27	96 800	90 000	11 600	6 000	7 000	7 000	7 000	1,30	-				-			
	110	27	96 800	90 000	11 600	6 000	7 000	7 000	7 000	1,35	-				-			
	110	27	96 800	90 000	11 600	6 000	7 000	7 000	7 000	1,35	-				-			
45	75	16	44 600	52 000	6 300	9 000	11 000	11 000	11 000	0,26	-				-			
	85	19	60 500	64 000	8 150	6 700	8 000	8 000	8 000	0,43	-				-			
	85	19	60 500	64 000	8 150	6 700	8 000	8 000	8 000	0,44	-				-			
	85	19	60 500	64 000	8 150	6 700	8 000	8 000	8 000	0,45	-				-			
	85	19	60 500	64 000	8 150	6 700	8 000	8 000	8 000	0,43	-				-			
	85	23	73 700	81 500	10 600	6 700	8 000	8 000	8 000	0,52	-				-			
	85	23	73 700	81 500	10 600	6 700	8 000	8 000	8 000	0,54	-				-			
	85	23	73 700	81 500	10 600	6 700	8 000	8 000	8 000	0,55	-				-			
	85	23	73 700	81 500	10 600	6 700	8 000	8 000	8 000	0,52	-				-			
	100	25	99 000	100 000	12 900	6 300	7 500	7 500	7 500	0,90	-				-			
	100	25	99 000	100 000	12 900	6 300	7 500	7 500	7 500	0,92	-				-			
	100	25	99 000	100 000	12 900	6 300	7 500	7 500	7 500	0,95	-				-			
	100	25	99 000	100 000	12 900	6 300	7 500	7 500	7 500	0,88	-				-			
	100	36	138 000	153 000	20 000	5 600	6 700	6 700	6 700	1,30	-				-			
	100	36	138 000	153 000	20 000	5 600	6 700	6 700	6 700	1,30	-				-			
	100	36	138 000	153 000	20 000	5 600	6 700	6 700	6 700	1,35	-				-			
	120	29	106 000	102 000	13 400	5 600	6 700	6 700	6 700	1,65	-				-			
	120	29	106 000	102 000	13 400	5 600	6 700	6 700	6 700	1,65	-				-			
	120	29	106 000	102 000	13 400	5 600	6 700	6 700	6 700	1,70	-				-			

Cylindrical roller bearings  
single row  
d 50-55 mm



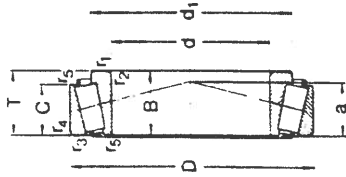
Principal dimensions d	Type NU				Type NUJ				Type NUP				Type N					
	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>	D	B	C	C <sub>0</sub>		
50	80	16	30 800	34 500	4 000	8 500	10 000	10 000	10 000	0,31	-				-			
	90	20	64 400	69 500	8 800	6 300	7 500	7 500	7 500	0,48	-				-			
	90	20	64 400	69 500	8 800	6 300	7 500	7 500	7 500	0,49	-				-			
	90	20	64 400	69 500	8 800	6 300	7 500	7 500	7 500	0,51	-				-			
	90	20	64 400	69 500	8 800	6 300	7 500	7 500	7 500	0,48	-				-			
	90	23	78 100	88 000	11 400	6 300	7 500	7 500	7 500	0,56	-				-			
	90	23	78 100	88 000	11 400	6 300	7 500	7 500	7 500	0,58	-				-			
	90	23	78 100	88 000	11 400	6 300	7 500	7 500	7 500	0,59	-				-			
	110	27	110 000	112 000	15 000	5 000	6 000	6 000	6 000	1,15	-				-			
	110	27	110 000	112 000	15 000	5 000	6 000	6 000	6 000	1,15	-				-			
	110	27	110 000	112 000	15 000	5 000	6 000	6 000	6 000	1,20	-				-			
	110	27	110 000	112 000	15 000	5 000	6 000	6 000	6 000	1,15	-				-			
	130	31	130 000	127 000	16 800	5 000	6 000	6 000	6 000	2,00	-				-			
	130	31	130 000	127 000	16 800	5 000	6 000	6 000	6 000	2,05	-				-			
55	90	18	57 200	69 500	8 300	7 000	8 500	8 500	8 500	0,40	-				-			
	100	21	84 200	95 000	12 200	6 000	7 000	7 000	7 000	0,66	-				-			
	100	21	84 200	95 000	12 200	6 000	7 000	7 000	7 000	0,67	-				-			
	100	21	84 200	95 000	12 200	6 000	7 000	7 000	7 000	0,69	-				-			
	100	21	84 200	95 000	12 200	6 000	7 000	7 000	7 000	0,66	-				-			
	100	25	99 000	118 000	15 300	6 000	7 000	7 000	7 000	0,79	-				-			
	100	25	99 000	118 000	15 300	6 000	7 000	7 000	7 000	0,81	-				-			
	100	25	99 000	118 000	15 300	6 000	7 000	7 000	7 000	0,82	-				-			
	100	25	99 000	118 000	15 300	6 000	7 000	7 000	7 000	0,79	-				-			
	120	29	138 000	143 000	18 600	4 800	5 600	5 600	5 600	1,45	-				-			
	120	29	138 000	143 000	18 600	4 800	5 600	5 600	5 600	1,50	-				-			
	120	29	138 000	143 000	18 600	4 800	5 600	5 600	5 600	1,55	-				-			
	120	29	138 000	143 000	18 600	4 800	5 600	5 600	5 600	1,45	-				-			

Taper roller bearings  
single row  
d 50-65 mm



Principal dimensions	Basic load ratings			Fatigue load limit P <sub>u</sub>	Speed ratings Lubrication grease oil	Mass	Designation	Dimension Series to ISO 355
	d	D	T					
50	110	29,25	125 000	140 000	17 000	3 600	30310	2FB
(cont.)	110	29,25	106 000	120 000	14 300	3 200	31310	7FB
	110	42,25	172 000	212 000	24 500	3 200	32310	2FD
	110	42,25	161 000	216 000	25 000	3 200	32310 B	5FD
55	90	23	78 100	112 000	12 500	4 000	K-JLM 506849/K-JLM 506810	-
	90	23	80 900	118 000	13 200	4 000	32011 X	3CC
	90	27	89 700	137 000	15 300	4 000	33011	3CE
	95	30	110 000	156 000	18 000	3 800	33111	3CE
	100	26,75	89 700	108 000	12 200	3 800	30211	3DB
	100	26,75	106 000	128 000	15 000	3 800	30211 B	3DC
	100	26,75	101 000	127 000	15 300	3 600	32211 B	-
	100	35	138 000	190 000	22 000	3 400	32211	3DE
	110	39	179 000	232 000	26 500	3 000	32211 B	3DE
	115	34	125 000	163 000	19 600	3 000	T2ED 055	2FD
	120	31,5	142 000	183 000	19 600	3 200	T7FC 055	7FB
	120	31,5	121 000	137 000	17 000	2 800	33111	2FD
	120	45,5	198 000	250 000	29 000	3 000	32311	2FD
	120	45,5	190 000	260 000	30 000	2 800	32311 B	5FD
60	95	23	82 500	122 000	13 700	3 800	32012 X	4CC
	95	27	84 200	132 000	15 000	3 600	K-JLM 508746/K-JLM 508710	-
	95	27	91 300	143 000	16 000	3 600	33012	2CE
	100	30	117 000	170 000	19 400	3 600	33112	3CE
	100	30	99 000	140 000	13 400	3 400	30812	3EB
	110	29,75	125 000	160 000	19 000	3 400	32212	3EC
	110	29,75	168 000	236 000	27 000	3 000	33212	3EE
	115	38	168 000	250 000	27 500	3 000	T2EE 040	5ED
	115	38	194 000	260 000	30 000	3 200	T2EE 040	2FE
	125	37	154 000	204 000	24 500	2 600	T7FC 060	7FC
	130	33,5	168 000	198 000	23 600	3 000	30312	2FB
	130	33,5	145 000	168 000	20 400	2 600	33312	2FD
	130	48,5	229 000	290 000	34 500	2 600	32312	2FD
	130	48,5	220 000	305 000	35 000	2 600	32312 B	5FD
65	100	23	84 200	127 000	14 300	3 400	32013 X	4CC
	100	27	86 800	156 000	17 600	3 400	33013	2CE
	110	28	123 000	183 000	21 200	3 200	K-JLM 511946/K-JM 511810	-
	110	34	142 000	208 000	24 500	3 000	33113	3DE
	120	24,75	114 000	134 000	16 300	3 000	30213	3EB
	120	32,75	151 000	193 000	23 200	3 000	32313	3EC
	120	38	181 000	240 000	27 500	3 000	T2ED 065	5ED

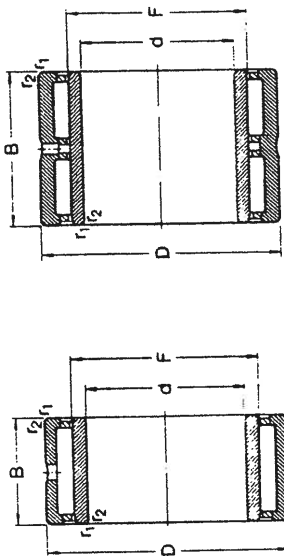
Taper roller bearings  
single row  
d 35-50 mm



Principal dimensions	Basic load ratings			Fatigue load limit P <sub>u</sub>	Speed ratings Lubrication grease oil	Mass	Designation	Dimension Series to ISO 355
	d	D	T					
35	80	22,75	72 100	73 500	8 500	5 000	30307	2FB
(cont.)	80	22,75	61 600	67 000	7 800	4 500	31307	7FB
	80	32,75	95 200	106 000	12 200	4 800	32307	2FE
	80	32,75	93 500	114 000	13 200	4 500	32307 B	5FE
40	68	19	52 800	71 000	7 800	5 300	32008 X	3CD
	75	20	79 200	104 000	11 600	5 000	33108	3CE
	80	19,75	61 600	68 000	7 650	4 800	30208	3DB
	80	24,75	74 800	86 500	9 800	4 300	32208	3DC
	80	32	105 000	132 000	15 300	4 000	32208 B	3DE
	85	33	121 000	150 000	17 300	4 500	T2EE 040	2EE
	90	25,25	85 800	95 000	11 000	4 500	30308	2FB
	90	25,25	73 700	81 500	9 650	4 000	31308	7FB
	90	35,25	117 000	140 000	16 300	4 000	32308	2FD
	90	35,25	108 000	140 000	16 300	4 000	32308 B	5FD
45	75	20	58 300	80 000	8 800	4 800	32009 X	3CC
	80	26	84 200	114 000	12 900	4 500	33109	3CE
	85	20,75	66 000	76 500	8 650	4 500	30209	3DB
	85	24,75	80 900	98 000	11 200	4 500	32209	3DC
	85	32	108 000	143 000	16 300	4 300	32209 B	5DC
	85	32	108 000	143 000	16 300	4 000	33209	3DE
	95	26	89 700	112 000	12 900	4 800	T7FC 045	7FC
	95	36	147 000	186 000	21 200	4 000	T2ED 048	2ED
	100	27,25	108 000	120 000	14 600	4 000	30309	2FB
	100	27,25	91 300	102 000	12 500	3 400	31309	7FB
	100	36,25	140 000	170 000	20 400	3 600	32309	2FD
	100	36,25	134 000	176 000	20 000	3 600	32309 B	5FD
50	80	20	60 500	88 000	9 650	4 500	32010 X	3CC
	80	24	69 300	102 000	11 400	4 500	33010	2CE
	82	21,5	72 100	100 000	11 000	4 500	K-JLM 104948/K-JLM 104810	-
	85	26	85 800	122 000	13 700	4 300	30210	3CE
	90	21,75	76 500	91 500	10 400	4 300	33110	3DB
	90	24,75	82 500	100 000	11 600	4 300	30210 B	3DC
	90	24,75	106 000	140 000	16 300	4 000	32210 B	5DC
	90	28	124 000	160 000	18 300	4 000	K-JM 205149/K-JM 205110	-
	90	32	114 000	140 000	16 300	4 000	K-JM 205149/K-JM 205110 A	-
	90	32	154 000	200 000	22 800	3 800	33210	3DE
	100	36	154 000	200 000	22 800	3 800	T2ED 050	2ED
	105	32	108 000	137 000	16 000	3 200	T7FC 050	7FC



**Needle roller bearings with flanges  
with inner ring  
d 40-65 mm**



Series NA 69

Series NK(S), NA 49

Principal dimensions	Basic load ratings			Fatigue load limit $P_u$	Speed ratings		Mass	Designation
	dynamic	static	$C_0$		Lubrication grease	oil		
d	D	B	C	$C_0$	N	r/min	Kg	
40	55	20	27 500	57 000	7 200	6 300	9 000	NK1 40/20 NK1 40/30 NA 4908 NA 6908 NK(S) 40
	55	30	40 200	83 000	12 000	6 300	9 000	
	62	22	42 900	71 000	9 150	5 600	8 000	
	62	40	67 100	125 000	16 000	5 600	8 000	
	65	22	42 900	72 000	9 150	5 600	8 000	
42	57	20	29 200	61 000	7 650	6 000	8 500	NK1 42/20 NK1 42/30
	57	30	41 800	98 000	12 900	6 000	8 500	
45	62	25	38 000	78 000	10 000	5 600	8 000	NK1 45/25 NK1 45/35
	62	35	49 500	110 000	14 300	5 600	8 000	
	68	22	45 700	78 000	10 000	5 300	7 500	NA 4909
	68	40	70 400	137 000	17 300	5 300	7 500	NA 6909
	72	22	44 600	78 000	10 000	5 000	7 000	NK(S) 45
50	68	25	40 200	88 000	11 200	5 300	7 500	NK1 50/25
	68	35	52 300	122 000	16 000	5 300	7 500	NK1 50/35
	72	22	47 300	85 000	11 000	5 000	7 000	NA 4910
	72	40	73 700	150 000	19 000	5 000	7 000	NA 6910
	80	28	62 700	104 000	13 700	4 500	6 300	NK(S) 50
55	72	25	41 800	96 500	12 200	4 800	6 700	NK1 55/25
	72	35	55 000	134 000	17 600	4 800	6 700	NK1 55/35
	80	25	57 200	106 000	13 700	4 500	6 300	NA 4911
	80	45	89 700	190 000	24 000	4 500	6 300	NA 6911
	85	28	66 000	114 000	15 000	4 300	6 000	NK(S) 55
60	82	25	44 000	95 000	12 000	4 300	6 000	NK1 60/25
	82	35	60 500	146 000	19 000	4 300	6 000	NK1 60/35
	85	25	60 500	114 000	14 600	4 300	6 000	NA 4912
	85	45	93 500	204 000	26 000	4 300	6 000	NA 6912
	90	28	68 200	120 000	15 600	4 000	5 600	NK(S) 60
65	90	25	61 600	120 000	15 300	4 000	5 600	NA 4913
	90	35	82 800	163 000	21 600	4 000	5 600	NK1 65/25 NK1 65/35
	90	45	95 200	212 000	27 000	4 000	5 600	NA 6913
	95	28	70 400	132 000	17 000	3 800	5 300	NK(S) 65