

1) a) i) The ability to infer the value of the state given measurements of the input and output.

Feedback  $H$  corrects state estimate.

ii) Useful if not all states are measured OR measurements of states are noisy.

$$\dot{\hat{x}} = A\hat{x} + Bu + H(C\hat{x} - Cy) \quad u = -Kx$$

$$\Rightarrow \begin{bmatrix} \dot{\hat{x}} \\ \dot{\hat{x}} \end{bmatrix} = \begin{bmatrix} A & BK \\ -HC & A+HC-BK \end{bmatrix} \begin{bmatrix} \hat{x} \\ \hat{x} \end{bmatrix}$$

b) i) 
$$\begin{vmatrix} \lambda+2 & -4 & -1 \\ 0 & \lambda-1 & 0 \\ 2 & -3 & \lambda \end{vmatrix} = (\lambda+2)(\lambda-1)\lambda - 1 \cdot -2(\lambda-1) = 0$$

$$\lambda^3 + \lambda^2 - 2\lambda + 2\lambda - 2 = 0$$

$\lambda = 1$  is solution by inspection

$$\Rightarrow (\lambda-1)(\lambda^2 + 2\lambda + 2) = 0$$

$$(\lambda+1)^2 + 1$$

$$\Rightarrow \lambda = 1, -1 \pm j$$

for e.v. 
$$\begin{bmatrix} 3 & -4 & -1 \\ 2 & -3 & 1 \end{bmatrix} \begin{bmatrix} x \\ y \\ 1 \end{bmatrix} = 0$$

$$3x - 4y = 1$$

$$2x - 3y = -1$$

$$-8y + 9y = 5 \Rightarrow y = 5$$

$$\Rightarrow x = 7 \Rightarrow v = \begin{bmatrix} 7 \\ 5 \\ 1 \end{bmatrix}$$

$$Q = \begin{bmatrix} 10 & -13 & -5 \\ -10 & 12 & 10 \\ 0 & 2 & -10 \end{bmatrix}$$

$$\text{row 1} + \text{row 2} + \frac{\text{row 3}}{2} = 0$$

$\Rightarrow$  not observable

iii)  $A \begin{bmatrix} 7 \\ 5 \end{bmatrix} = 0 \Rightarrow$  unstable subspace is unobservable.

2 a) For any  $x_e$  there exists a corresponding  $u_e$  to maintain equilibrium.  $u_e = 3x_e + x_e^3$

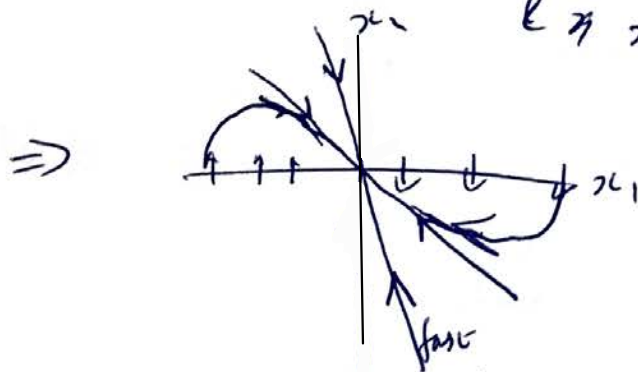
$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -x_1 - 3x_2 \end{aligned}$$

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= u - 4x_2 - 3x_1 - x_1^3 \\ \frac{\partial \dot{x}_2}{\partial x_1} &= -3 - 3x_1^2 \\ \Rightarrow \dot{x}_2 &= u - 4x_2 - 3 - 3x_1^2 \end{aligned}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -3-3x_1^2 & -4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

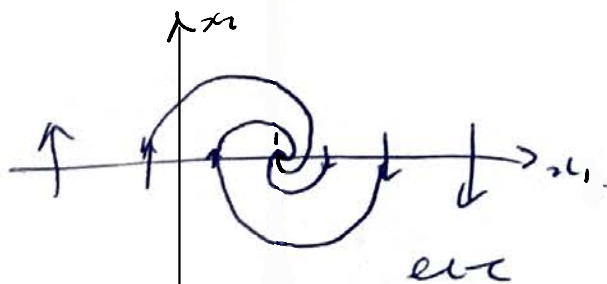
$u = 0$   $\Rightarrow x_e = 0$   $\& \lambda^2 + 4\lambda + 3 = (\lambda + 1)(\lambda + 3)$   
 $\lambda = -1, -3$

eigenvectors:  $\begin{bmatrix} 0 & 1 \\ -3 & -4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -x_1 \\ -x_2 \end{bmatrix}$   
 $x_2 = -x_1$   $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$   
 $x_2 = -3x_1$   $\begin{bmatrix} 1 \\ -3 \end{bmatrix}$



$x_2 = 0 \Rightarrow \dot{x}_1 = 0$   
 $\dot{x}_2 = -3x_1$

$u_e = 4 \Rightarrow x_e = 1$   $\lambda^2 + 4\lambda + 6 = (\lambda + 2)^2 + 2 = 0$   
 $\lambda = -2 \pm \sqrt{2}j$



c) justified as long as  $u$  is small,

$$(a) \quad \frac{d}{dt} \begin{bmatrix} z \\ \dot{z} \\ \theta \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 3\Omega^2 & 0 & 0 & 2\Omega R_0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -\frac{2\Omega}{R_0} & 0 \end{bmatrix} \begin{bmatrix} z \\ \dot{z} \\ \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} u_2 \\ u_0 \end{bmatrix}$$

$$(b) \quad AB = \begin{bmatrix} 1 & 0 \\ 0 & 2\Omega R_0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}$$

Full rank matrix

(c)  $y = \theta$  make the system observable:

$$\dot{y} = \dot{\theta}$$

$$\ddot{y} = 2\Omega R_0 \dot{\theta} (+ 3\Omega^2 y + u_2)$$

$$\dddot{y} = -\frac{4\Omega^2}{R_0} \theta (+ u_0 + 3\Omega^2 \dot{y} + \dot{u}_2)$$

$\Rightarrow$   $x$  in terms of  $y$  and its derivatives.

Note: ~~no other choice works.~~

\*  ~~$\theta$  (resp  $\dot{\theta}$ ) cannot be reconstructed from  $\dot{\theta}$  (resp  $\ddot{\theta}$ )~~

\* ~~Differentiating  $\theta$  only provides  $\dot{\theta}$ .~~

Also  $y = \theta$  makes system observable

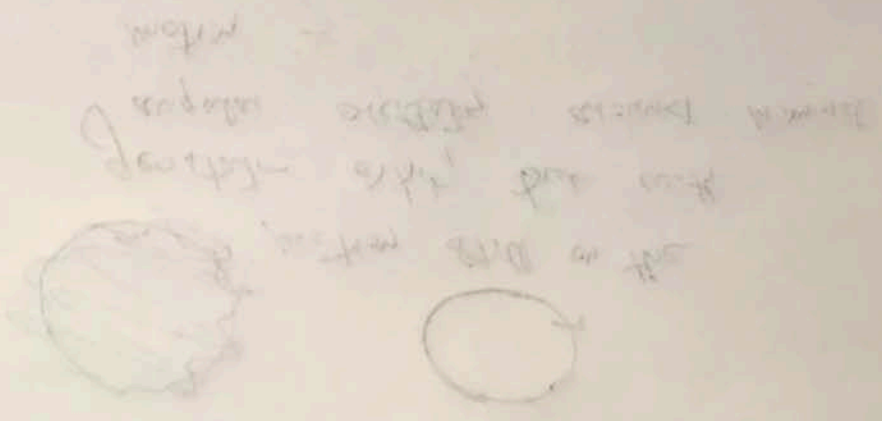
But not  $\dot{\theta}$  since  $\theta$  cannot be reconstructed from  $\dot{\theta}$ .

$$(d) \quad u_2 = -2\Omega R_0 \dot{\theta} - 3\Omega^2 z - k_p z - k_d \dot{z}$$

leads to  $\ddot{z} + k_p z + k_d \dot{z} = 0$   
which is stable if  $k_p > 0, k_d > 0$

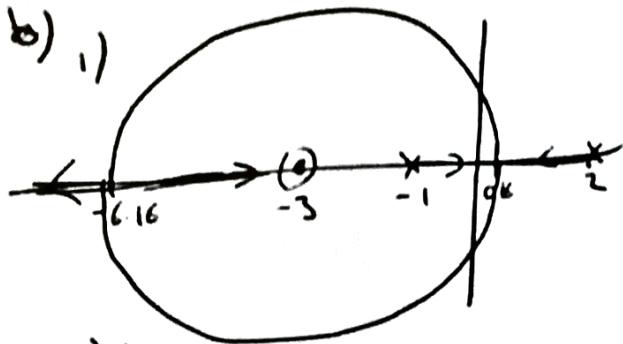
The resulting motion is still on  
the geostationary orbit but with an angular  
oscillation around the nominal orbit.

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$$4) G(s) = \frac{s+3}{(s-2)(s+1)}$$

a)  $1 + K.L(s) = 0$  etc  
 principle for  $s$ , is  $K$   
 Jan real and positive



$$\frac{dG}{ds} \propto (s+3)(2s-1) - (s-2)(s+1)$$

$$= 2s^2 + 5s - 3 - s^2 + s + 2$$

$$= s^2 + 6s - 1$$

roots are  $-6.16, 0.16$

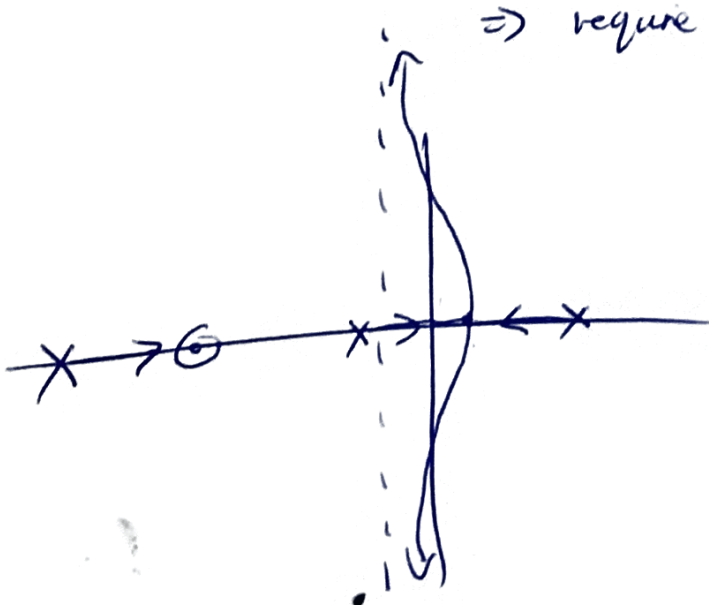
$K =$   
 (for zero breaking)

$$\frac{5.16 \times 8.16}{3.16} = 13.33$$

$\Rightarrow$  stable for  $K > 13.33$   
 2 real poles

ii) asymptotes are  $\frac{2 - 1 + 0 + 3 - \frac{1}{\tau_i}}{4 - 2}$

$\Rightarrow$  require  $4 - \frac{1}{\tau_i} < 0$   
 $\tau_i < 0.25 \text{ sec}$



Q1 was a popular question and generally well answered. In part b (iii), very few candidates identified that the unstable vector (calculated in part b (i)) was in the null space of the observability matrix (calculated in part b (ii)).

Q2 was a question on linearization and the plotting of state-space trajectories, and was generally well answered with a large number of complete or close to complete answers. Many candidates gave overly long and general answers to part c) though, missing the fact that it simply required  $u$  to be small for this system.

Q3 was a straightforward question and generally well answered. In part c), most candidates embarked a long calculation to choose the poles of the feedback system. Only few candidates observed that stabilising only the radial position had a straightforward solution.

Q4 was a popular question on root locus, and was matched by a large number of close to complete answers. The worst answered part was a) – the "single" key principle behind the construction of a root locus diagram is the angle condition (ie choose an  $s$  and check if it is a closed loop pole for some  $k$ ).