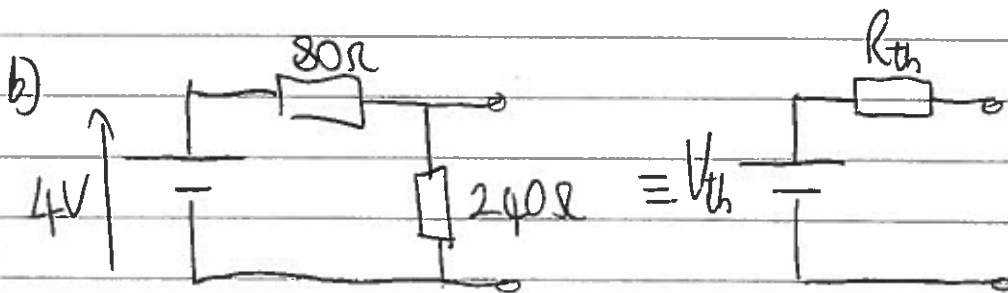


# IA Paper 3 2016

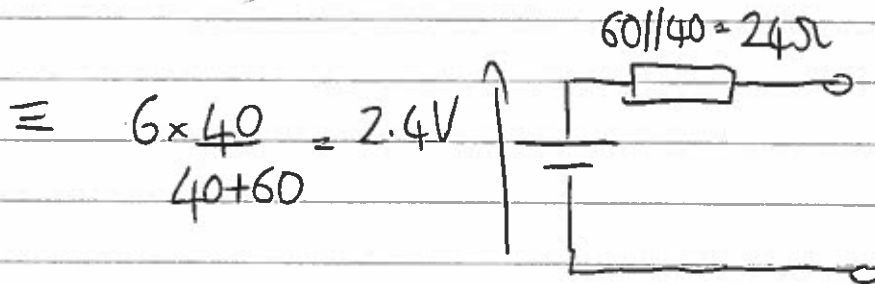
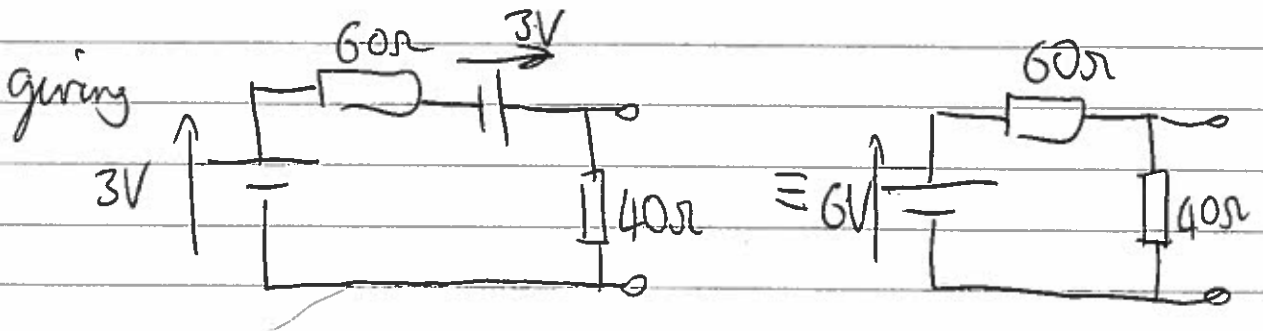
1. a) **Thevenin's theorem:** as far as the load is concerned, a linear circuit may be represented by an ideal voltage source ( $V_{th}$ ) in series with a resistor ( $R_{th}$ ) in which  $V_{th} = V_{oc}$ ,  $R_{th} = V_{oc}/I_{sc}$ .

**Norton's Theorem:** for circuit above, as far as the load is concerned, it can be represented as a current source ( $I_N$ ) in parallel with a resistor  $R_N$  in which  $I_N = I_{sc}$ ,  $R_N = R_{th}$ .

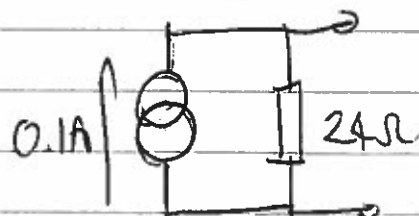
[3]



$$V_{th} = \frac{240}{240+80} \times 4 = 3V, \quad R_{th} = 80\Omega // 240\Omega = 60\Omega$$

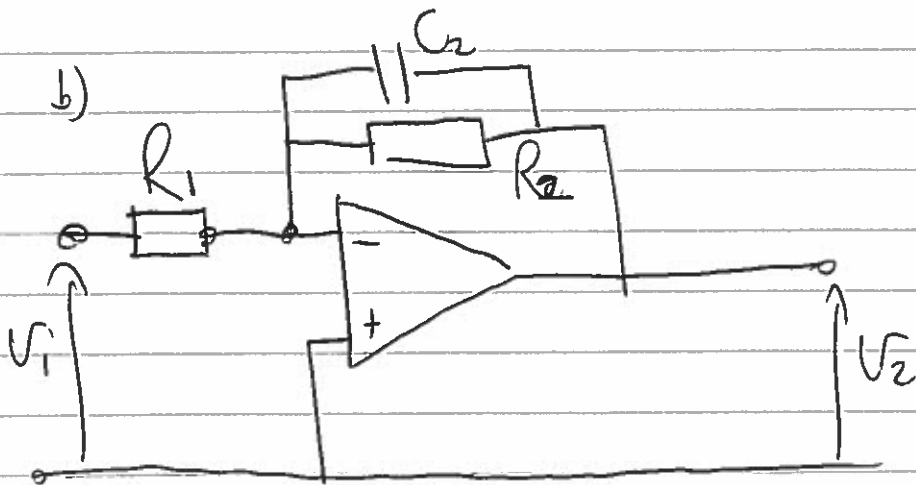


$$I_{sc} = \frac{2.4}{24} = 0.1A = I_N, \quad R_N = R_{th}$$



[7]

a) Ideal op-amp assumed to have infinite open loop gain and input resistance, and zero output resistance. (3)



At low frequency such that  $1/\omega C_2 \gg R_2$ :

$$\frac{V_2}{R_2} + \frac{V_1}{R_1} = 0 \quad \frac{V_2}{V_1} = -\frac{R_2}{R_1}$$

Increasing frequency with decrease gain as capacitor impedance falls

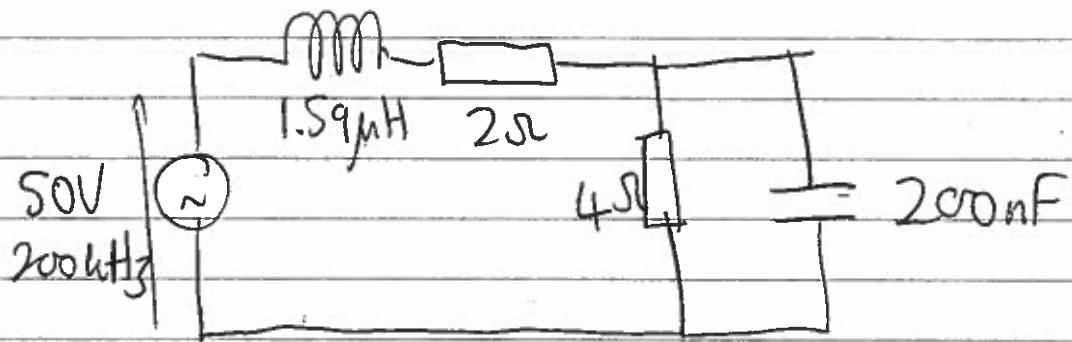
$$R_2 \parallel C_2 = \frac{R_2 \times 1/j\omega C_2}{R_2 + 1/j\omega C_2} = \frac{R_2}{1 + j\omega C_2 R_2}$$

$$\therefore \frac{V_2}{V_1} = -\frac{R_2}{R_1(1 + j\omega C_2 R_2)}$$

-3dB frequency when real & imaginary parts of denominator are equal

$$\therefore \omega_{-3dB} C_2 R_2 = 1 \quad \rightarrow \quad \omega_{-3dB} = \frac{1}{R_2 C_2}$$

3.



$$\bar{Z}_L = j\omega L = j2\pi \times 200 \times 10^3 \times 1.59 \times 10^{-6} = j2 \Omega$$

$$\bar{Z}_C = \frac{1}{j\omega C} = -j \times \frac{1}{2\pi \times 200 \times 10^3 \times 200 \times 10^{-9}} = -j4 \Omega$$

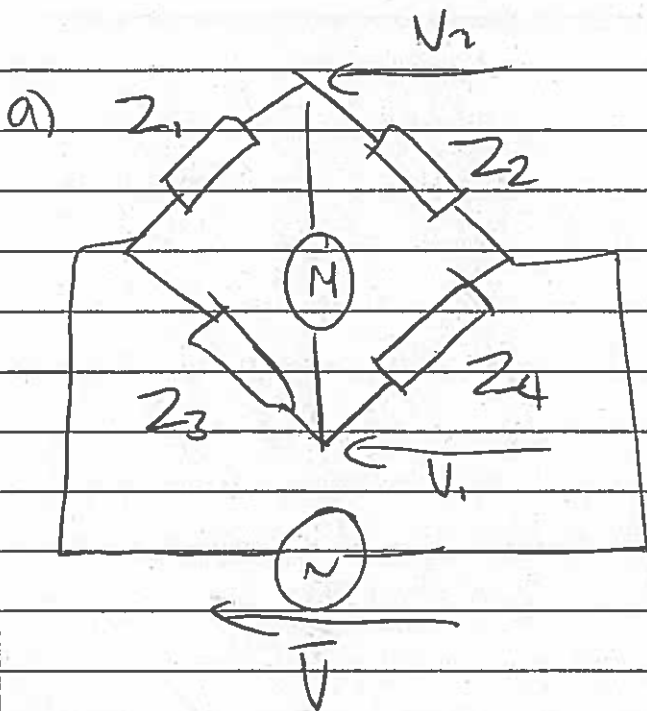
$$4 \Omega \parallel -j4 \Omega = \frac{4 \times (-j4)}{4 - j4} = \frac{-j4}{1 - j} = \frac{-j4(1+j)}{2}$$

$$= (2 - j2) \Omega$$

$$\therefore \bar{Z} = j2 + 2 + 2 - j2 = 4 \Omega$$

$$I = \frac{50}{4} = 12.5 \text{ A } \angle 0^\circ$$

4/



$$V_1 = V_2 \text{ für Balance} \Rightarrow \frac{Z_4}{Z_4 + Z_3} = \frac{Z_2}{Z_2 + Z_1}$$

$$Z_4(Z_2 + Z_1) = Z_2(Z_4 + Z_3)$$

$$\underline{Z_1 Z_4 = Z_2 Z_3}$$

b)

$$Z_1 = R_1, \quad Z_2 = R_2, \quad Z_3 = \frac{R_3 \times \frac{1}{j\omega C}}{R_3 + \frac{1}{j\omega C}}$$

$$= \frac{R_3}{1 + j\omega C R_3}$$

$$Z_4 = R_4 + \frac{1}{j\omega C} = \frac{1 + j\omega C R_4}{j\omega C}$$

Balance:  $R_1 Z_4 = R_2 Z_3$

$$\Rightarrow R_1 \left( \frac{1 + j\omega C R_4}{j\omega C} \right) = \frac{R_2 R_3}{1 + j\omega C R_3}$$

$$\circ \quad R_1(1 + j\omega C R_4)(1 + j\omega C R_3) = j\omega C R_2 R_3$$

$$R_1[(1 - \omega^2 C^2 R_3 R_4) + j\omega C(R_3 + R_4)] = j\omega C R_2 R_3$$

equate real parts  $R_1(1 - \omega^2 C^2 R_3 R_4) = 0$

$$\omega = \frac{1}{C} \sqrt{\frac{1}{R_3 R_4}}$$

equate imaginary parts

$$R_1(R_3 + R_4) = R_2 R_3$$

$$\frac{R_2}{R_1} = 1 + \frac{R_4}{R_3}$$

c)  $Z_1 = R_1 + \frac{1}{j\omega C_1}$

$$Z_2 = \frac{1}{j\omega C_2}$$

$$Z_3 = R_3$$

$$Z_4 = \frac{R_4}{1 + j\omega C_4 R_4}$$

$$\frac{(1 + j\omega C_1 R_1)}{j\omega C_1} \times \frac{R_4}{1 + j\omega C_4 R_4} = \frac{R_3}{j\omega C_2}$$

$$(1 + j\omega C_1 R_1) R_4 C_2 = R_3 C_1 (1 + j\omega C_4 R_4)$$

real parts:  $R_4 C_2 = R_3 C_1$

imag parts:  $C_1 R_1 R_4 C_2 = R_3 C_1 C_4 R_4$

or  $R_1 C_2 = R_3 C_4$

$$\boxed{\begin{array}{l} R_4 C_2 = R_3 C_1 \\ R_1 C_2 = R_3 C_4 \end{array}}$$

independent of frequency

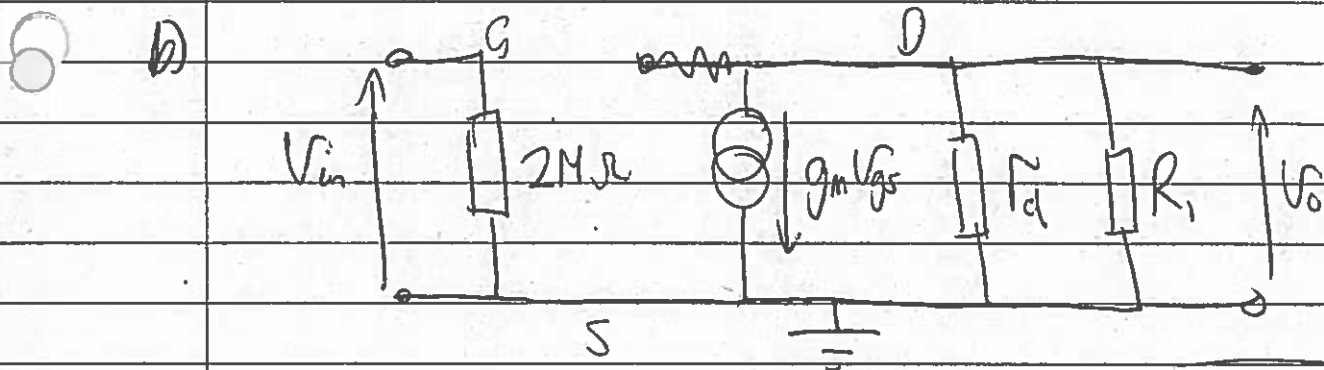
S/a)  $R_2 I_0 = +2V$  (2M $\Omega$  holds  $V_G = 0V$ )

$$R_2 = \frac{+2V}{0.2mA} = \underline{10k\Omega}$$

$$V_{GS} = 8V \text{ so } V_{D=0} = 2+8 = 10V \text{ so } \frac{10 - I_0}{R_1}$$

$$R_1 = \frac{10}{0.2mA} = \underline{50k\Omega}$$

[10]



[5]

c)  $V_{GS} = V_{in}$

$$V_o = -g_m V_{GS} R_d // R_L \text{ so } \frac{V_o}{V_{in}} = -g_m \frac{R_d R_L}{R_d + R_L}$$

$$R_{out} = \frac{V_o}{I_o} \text{ with } V_{in} = 0 \text{ giving } R_d // R_L$$

$$= \frac{R_d R_L}{R_d + R_L}$$

$R_d = 200k\Omega$ ,  $R_L = 50k\Omega$  so  $R_d // R_L = 40k\Omega$

$$G_{mid} = -1 \times 10^{-3} \times 40 \times 10^3 = \underline{-40}$$

$$R_{out} = \underline{40k\Omega}$$



Section B Digital circuits June 2016 Dr T J Flack

6. a) (Short) If the LHS and RHS of the expressions are equal for all 4 combinations of inputs A and B then the theorems are proved.

A	B	$A \cdot B$	$\overline{A \cdot B}$	$\overline{A}$	$\overline{B}$	$\overline{A+B}$
0	0	0	1	1	1	1
0	1	0	1	1	0	1
1	0	0	1	0	1	1
1	1	1	0	0	0	0

Columns  $\overline{A \cdot B}$  and  $\overline{A+B}$  are the same so  $\overline{A \cdot B} = \overline{A+B}$

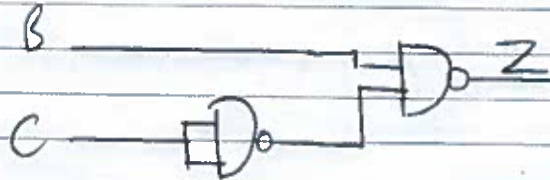
A	B	$A+B$	$\overline{A+B}$	$\overline{A}$	$\overline{B}$	$\overline{\overline{A} \cdot \overline{B}}$
0	0	0	1	1	1	1
0	1	1	0	1	0	0
1	0	1	0	0	1	0
1	1	1	0	0	0	0

Columns  $\overline{A+B}$  and  $\overline{\overline{A} \cdot \overline{B}}$  are the same so  $\overline{A+B} = \overline{\overline{A} \cdot \overline{B}}$

b)  $Z = B \cdot C + A \cdot \overline{B} + \overline{A} \cdot \overline{B}$

$\overline{A} \cdot \overline{B}$	00	01	11	10
B	1	0	0	1
C	1	1	1	1

$\overline{Z} = B \cdot \overline{C} \therefore Z = \overline{B \cdot \overline{C}}$





7 (short) a) 8 data lines  $\Rightarrow$  data stored in bytes

$$\therefore N^{\circ} \text{ bytes} = 2^3 = 8192 \text{ bytes} = 8 \text{ kbytes}$$

A 32 bit processor can address  $2^{32}$  bytes = 4 Gbytes.

Point of interest: First PCs were 16 bit and could address  $2^{16} =$

64 kbytes of memory. When 32 bit computers came out it was

believed that it would never be possible to construct 4 Gbytes of

memory (you can now buy a 64 Gbyte memory stick for  $\sim$  £15!)

A CD holds  $\sim$  1 Gbyte, a DVD  $\sim$  4 Gbytes, Blu-ray  $\sim$  25 Gbytes

and we now have 64 bit computers to facilitate manipulating this order of data.

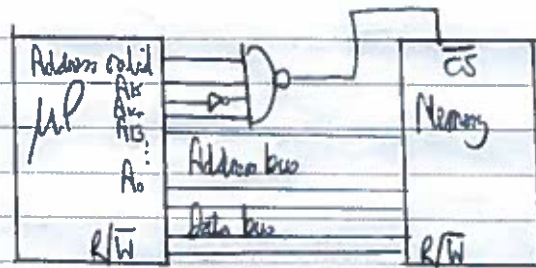
b)  $\overline{CS}$  input allows one of a number of memory devices connected to the

$\mu P$  to be accessed. R/W line dictates whether data is being

written to or read from memory

$$\begin{array}{r} A_{15} \qquad \qquad \qquad A_0 \\ A000 \quad 1 \quad 0 \quad 1 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \quad 0 \\ BFFF \quad 1 \quad 0 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \quad 1 \end{array}$$

$$\overline{CS} = A_{15} \cdot \overline{A_{14}} \cdot A_{13} \text{ Address valid}$$



3 (short) a) Literal instructions operate directly on the supplied 8 bit integer argument. ~~Literal~~ File Register Instructions have the memory location from which to obtain the data to be operated on as their argument.

b) movlw 15; 15 = 0F<sub>hex</sub> into W  
 movwf 0x20; 0F<sub>hex</sub> into 0x20  
 movlw 0xF1; F1<sub>hex</sub> into W  
 addwf 0x20, W; F1 added to 0F, result into W  
 movlw 0xAA; AA<sub>hex</sub> into W  
 movwf 0x20; AA copied into 0x20  
 movlw 255; FF<sub>hex</sub> into W  
 xorwf 0x20; XOR of AA and FF into 0x20;  
 sleep;

i) W 11110001  
 0x20 00001111  
 W (00,00,00,000)

∴ Half-carry (DC) set (DC=1)  
 Carry (C) set (C=1)  
 Result is zero so Z set (Z=1)

0x20 contains 0F<sub>hex</sub>, W contains 00<sub>hex</sub>

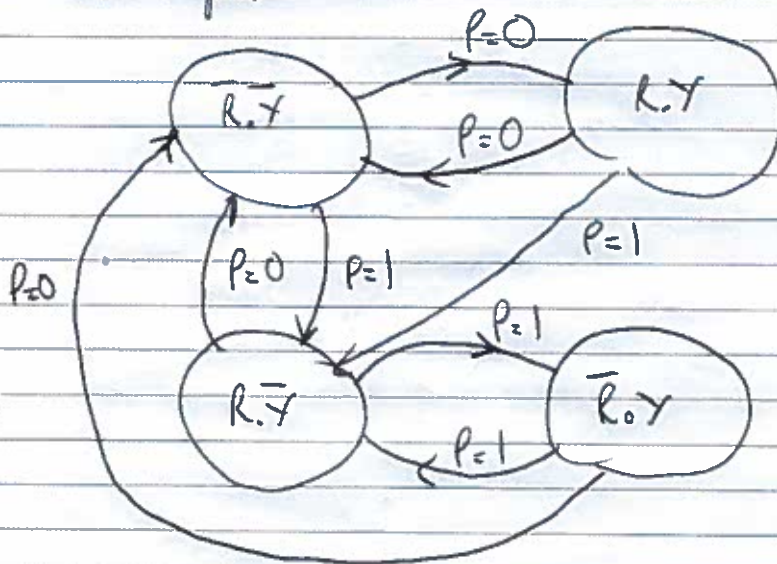
$$\begin{array}{cccccc} \text{i)} & 1 & 0 & 1 & 0 & 1 & 0 & 0 \times 20 \\ & 1 & 1 & 1 & 1 & 1 & 1 & W \\ & 0 & 1 & 0 & 1 & 0 & 1 & 0 \times 20 \end{array}$$

$\therefore C=0, DC=0, Z=0$  since result  $\neq 0$ ,

$0 \times 20$  contains 55 hex, W remains FF hex.

9 (long) a) There are 4 different states:  $\bar{R}\bar{Y}, R\bar{Y}, \bar{R}Y, RY$

State diagram:-



b)  $2^N \geq 4$  where  $N = N^\circ$  of bistables so  $N=2$  i.e. 2 bistables are needed.

c) Denote one bistable  $R$ , with output  $Q_x$ , the other one  $Y$  with output  $Q_y$ . To avoid output logic let  $R=Q_x, Y=Q_y$

P	Present		Next		J <sub>R</sub>	K <sub>R</sub>	J <sub>Y</sub>	K <sub>Y</sub>
	Q <sub>R</sub>	Q <sub>Y</sub>	Q <sub>R</sub>	Q <sub>Y</sub>				
0	0	0	1	1	1	x	1	x
1	0	0	1	0	1	x	0	x
0	1	1	0	0	x	1	x	1
1	1	1	1	0	x	0	x	1
0	1	0	0	0	x	1	0	x
1	1	0	0	1	x	1	1	x
0	0	1	1	0	0	x	x	1
1	0	1	1	1	1	x	x	1

~~J<sub>R</sub>~~  $\overline{P} \overline{Q}_R$

	00	01	11	10
0	1	0	x	x
1	1	1	x	x

$$J_R = P + \overline{Q}_Y$$

~~K<sub>R</sub>~~  $\overline{P} \overline{Q}_R$

	00	01	11	10
0	x	x	1	1
1	x	x	0	1

$$K_R = \overline{P} + \overline{Q}_Y$$

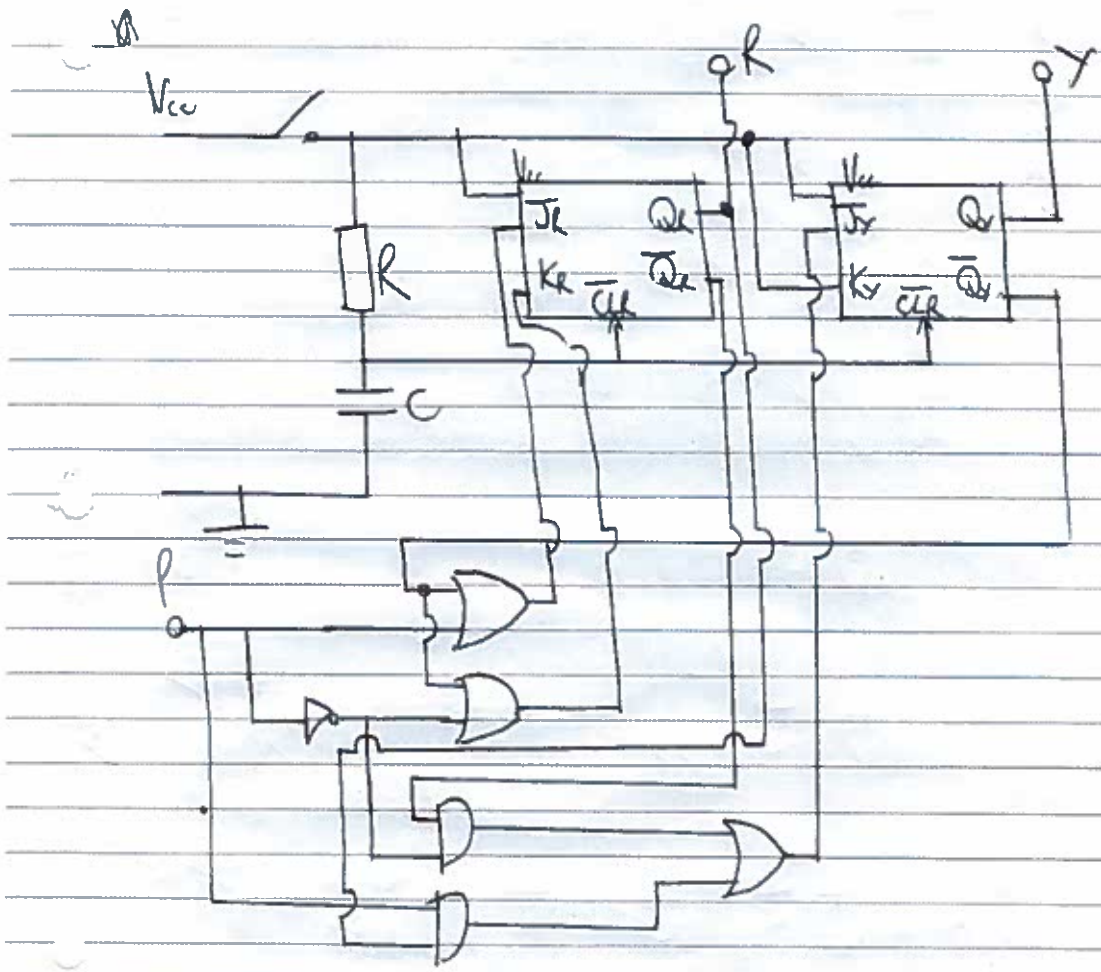
~~J<sub>Y</sub>~~  $\overline{P} \overline{Q}_R$

	00	01	11	10
0	1	x	x	0
1	0	x	x	1

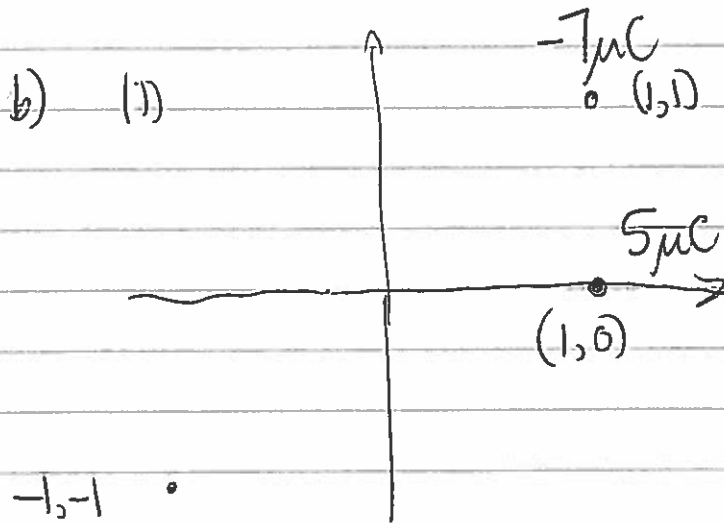
$$J_Y = \overline{P} \cdot \overline{Q}_R + P \cdot Q_R$$

By inspection  $K_Y = 1$

d) To set initial state to  $\overline{R} \cdot \overline{Y}$  use  $\overline{CLK}$  input by making sure  $\overline{CLK}$  is zero ~~to~~ when power is applied using an R-C circuit



10 (a) By Gauss' law, any internal net charge would cause an internal electric field, compelling such charges to repel each other to the surface of the conductor, such that the internal net electric field becomes zero. [2]



Field due to  $5 \mu\text{C}$  charge:  $\vec{E} = \frac{q}{4\pi\epsilon_0 r^2} \hat{r}$

$$r = \sqrt{2^2 + 1^2} = \sqrt{5} \text{ cm} \quad \hat{r} = \frac{-\hat{i}2 - \hat{j}1}{\sqrt{5}}$$

$$\begin{aligned} \text{so } \vec{E}_1 &= \frac{5 \times 10^{-6}}{4\pi \times 8.85 \times 10^{-12} \times (\sqrt{5} \times 10^{-2})^2} \left( \frac{-\hat{i}2 - \hat{j}1}{\sqrt{5}} \right) \\ &= 4.02 \times 10^7 (-2\hat{i} - \hat{j}) \end{aligned}$$

$$7 \mu\text{C} \text{ charge } r = 2\sqrt{2} \text{ cm}, \quad \hat{r} = \frac{\hat{i} + \hat{j}}{\sqrt{2}}$$

$$\vec{E}_2 = \frac{7 \times 10^{-6}}{4\pi\epsilon_0 (2\sqrt{2} \times 10^{-2})^2} \cdot \frac{\hat{i} + \hat{j}}{\sqrt{2}} = 5.56 \times 10^7 (\hat{i} + \hat{j})$$

$$\vec{E}_T = \vec{E}_1 + \vec{E}_2 = -\hat{i} 2.48 \times 10^7 + \hat{j} 1.54 \times 10^7 \text{ Vm}^{-1} \quad [6]$$

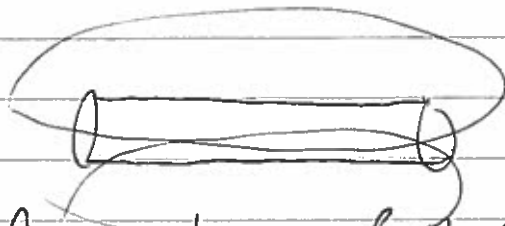
$$ii) \underline{F} = q\underline{E} = 10 \times 10^{-6} (-\underline{i} 2.48 \times 10^7 + \underline{j} 1.54 \times 10^7)$$

$$= -\underline{i} 248 + \underline{j} 154$$

$$|\underline{F}| = \underline{292 N}$$

11 a) Self inductance = Flux linkages of the circuit concerned / I

[2]



b)

Ampere's law  $\oint \underline{H} \cdot \underline{dl} = I_{enc}$

Assume it very large so  $\oint \underline{H} \cdot \underline{dl} = Hl = Inl$

$$B = \mu_0 H \Rightarrow B = \mu_0 In$$

$$\phi = BA = \mu_0 InA \quad \phi' = N\phi = \mu_0 In^2 l A$$

$$\text{so } \frac{\phi'}{I} = L = \mu_0 n^2 A l \quad [3]$$

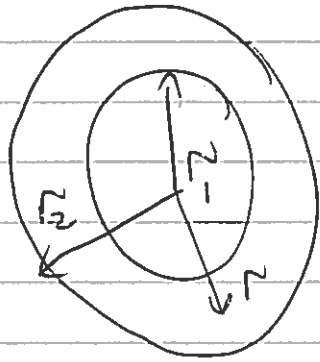
c)  $0 = RI + L \frac{dI}{dt}$  subject to  $I(0) = I_0$

~~$$I(t) = I_0 (1 - e^{-t/\tau}), \quad \tau = L/R \quad [5]$$~~

$$\int \frac{dI}{I} = -\frac{R}{L} dt \quad \ln kI = -\frac{Rt}{L} \quad kI = e^{-t/\tau} \quad \tau = L/R$$

$$t=0, I=I_0 \Rightarrow \frac{1}{k} = I_0 \text{ so } I = I_0 e^{-t/(L/R)} \quad [5]$$

12 a) 1)



Assume charge  $q$  on inner shell,  $-q$  on outer shell.

$$\text{Gauss: } \oint \underline{D} \cdot d\underline{S} = q \Rightarrow D \times 4\pi r^2 = q = \epsilon_0 E \times 4\pi r$$

$$\underline{E} = \frac{q}{4\pi\epsilon_0 r^2} \quad r_1 < r < r_2, \quad E=0 \text{ otherwise}$$

$$V = \int \underline{E} \cdot d\underline{l} = \frac{q}{4\pi\epsilon_0} \int_{r_1}^{r_2} \frac{1}{r^2} dr = \frac{q}{4\pi\epsilon_0} [-r^{-1}]_{r_1}^{r_2}$$

$$= \frac{q}{4\pi\epsilon_0} \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$C = \frac{q}{V} = \frac{4\pi\epsilon_0}{\left( \frac{1}{r_1} - \frac{1}{r_2} \right)} \quad [9]$$

ii) Largest electric field will be at  $r = r_1 = \frac{q}{4\pi\epsilon_0 E^2} = 3 \times 10^6$   
at breakdown.

$$q = 4\pi\epsilon_0 r_1^2 \times 3 \times 10^6 \quad \text{with } r_1 = 1 \text{ cm giving } q = \underline{33.3 \text{ nC}}$$

[3]



$$b) \quad i) \quad \oint \vec{H} \cdot d\vec{l} = NI$$

$$H \times 2\pi r = NI$$

$$H = \frac{NI}{2\pi r} \quad \text{so } B = \frac{\mu_0 \mu_r NI}{2\pi r} \quad \text{in ferrite [4]}$$

$$ii) \quad B = \frac{\mu_0 NI}{2\pi r} \quad \text{in air [4]}$$

$$iii) \quad d\Phi = B h dr$$

$$= \frac{\mu_0 NI}{2\pi r} h dr$$

$$\Phi_{\text{air}} = \int_{r_1}^{r_2} \frac{\mu_0 NI}{2\pi r} h dr$$

$$= \frac{\mu_0 NI h}{2\pi} \ln \frac{r_2}{r_1} = \frac{4\pi \times 10^{-7} \times 200 \times 1 \times 2 \times 10^{-2}}{2\pi} \ln \frac{7}{5}$$

$$= 2.7 \times 10^{-7} \text{ Wb}$$

~~ANS~~

For  $\Phi_{\text{ferrite}}$  need to divide region of integration into three:-

$$\Phi_{\text{ferrite}} = \frac{\mu_0 \mu_r NI}{2\pi} \left[ 0.03 \int_{0.04}^{0.05} \frac{1}{r} dr + 2 \times 0.005 \int_{0.05}^{0.07} \frac{1}{r} dr + 0.03 \int_{0.07}^{0.08} \frac{1}{r} dr \right]$$

$$= \frac{\mu_0 \mu_r N I}{2\pi} \left[ 0.03 \left( \ln \frac{5}{4} + \ln \frac{8}{7} \right) + 0.01 \ln \frac{7}{5} \right]$$

$$= \frac{4\pi \times 10^{-7} \times 500 \times 200 \times 1}{2\pi} \times 0.01406$$

$$= 2.81 \times 10^{-4} \text{ wb}$$

$$\text{iv) } \phi_{\text{total}} = \phi_{\text{air}} + \phi_{\text{ferrite}} = 2.82 \times 10^{-4} \text{ wb}$$

$$L = \frac{N \phi_{\text{total}}}{I} = \frac{200 \times 2.82 \times 10^{-4}}{1} = 56.3 \text{ mH}$$