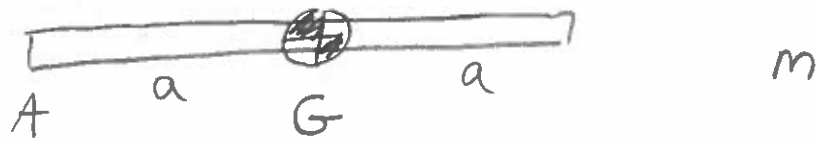
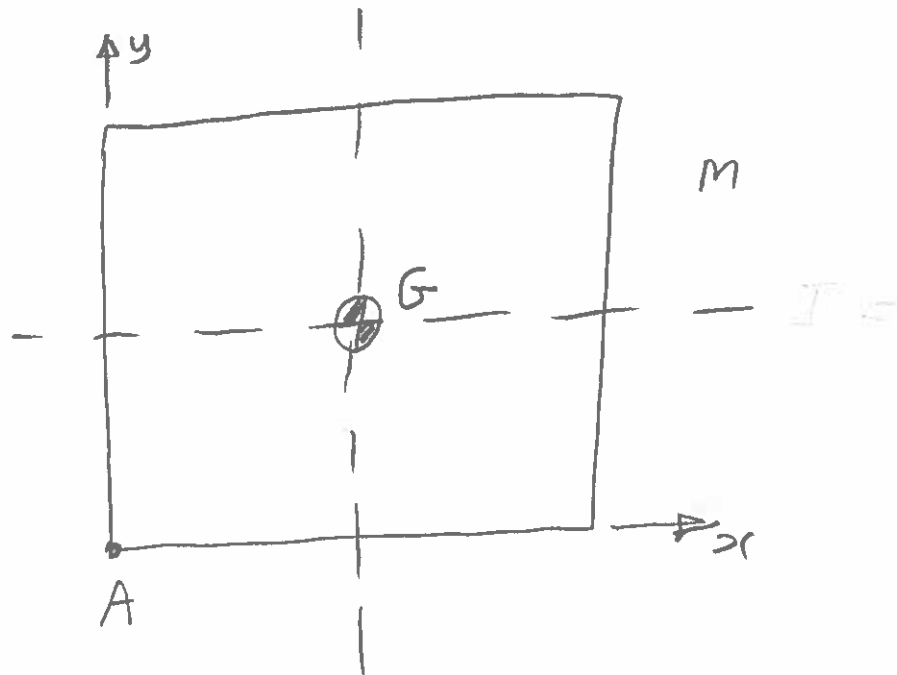


1/(a)
Use



$$I_G = \frac{1}{3} m a^2$$

$$I_A = \frac{4}{3} m a^2$$



$$I_G = \frac{2}{3} m a^2 \quad \text{by perpendicular axis theorem}$$

$$I_A = \frac{8}{3} m a^2 \quad \text{by parallel axis theorem}$$

$$\begin{aligned} I_{xy} &= \int_0^{2a} \int_0^{2a} xy \, dm \\ &= \int_0^{2a} x \, dx \int_0^{2a} y \, dy \frac{M}{4a^2} \\ &= \frac{(2a)^2}{2} \frac{(2a)^2}{2} \frac{M}{4a^2} = Ma^2 \end{aligned}$$

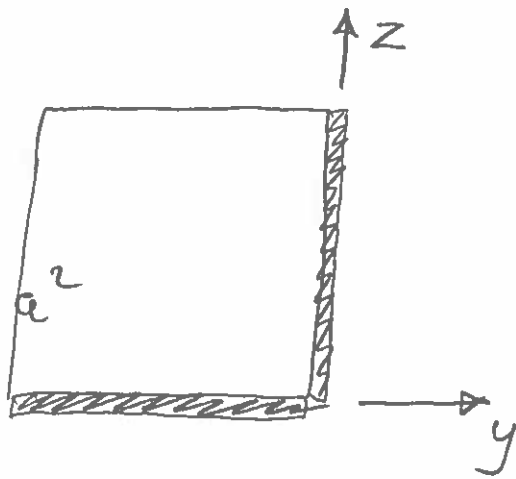
Now assemble according to the various views, noting sign of " I_{xy} "

1(a) cont

(2)

View along x

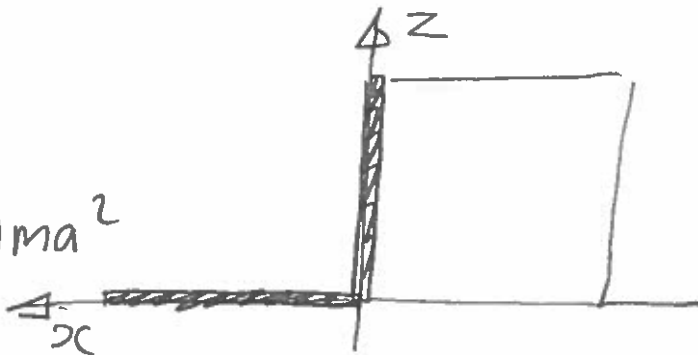
$$I_{xx} = \left(\frac{4}{3} + \frac{4}{3} + \frac{8}{3} \right) ma^2$$
$$= \frac{16}{3} ma^2$$



$$I_{yz} = \int_{-2a}^0 y dy \int_0^{2a} z dz \frac{m}{4a^2} = -ma^2$$

View along y

$$I_{yy} = \left(\frac{4}{3} + \frac{4}{3} + \frac{8}{3} \right) ma^2$$
$$= \frac{16}{3} ma^2$$

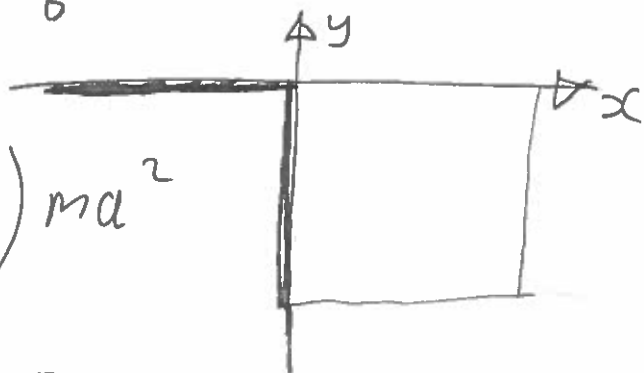


$$I_{xz} = \int_{-2a}^0 x dx \int_0^{2a} z dz \frac{m}{4a^2} = -ma^2$$

View along z

$$I_{zz} = \left(\frac{4}{3} + \frac{4}{3} + \frac{8}{3} \right) ma^2$$
$$= \frac{16}{3} ma^2$$

$$I_{xy} = \int_0^{2a} x dx \int_{-2a}^0 y dy \frac{m}{4a^2} = -ma^2$$



Put these into inertia matrix form:

(a) cont $I = \frac{ma^2}{3} \begin{bmatrix} 16 & +3 & +3 \\ +3 & 16 & +3 \\ +3 & +3 & 16 \end{bmatrix}$ (3)

(b) try $\underline{u}_1 = \begin{bmatrix} 1 \\ -1 \\ 0 \end{bmatrix}$, $I \underline{u}_1 = \frac{ma^2}{3} \begin{bmatrix} 13 \\ -13 \\ 0 \end{bmatrix}$
 $= \frac{13ma^2}{3} \underline{u}_1$
 $\therefore \lambda_1 = \frac{13ma^2}{3}$

try $\underline{u}_2 = \begin{bmatrix} 1 \\ 1 \\ -2 \end{bmatrix}$, $I \underline{u}_2 = \frac{ma^2}{3} \begin{bmatrix} 13 \\ 13 \\ -26 \end{bmatrix}$
 $= \frac{13ma^2}{3} \underline{u}_2$
 $\therefore \lambda_2 = \frac{13ma^2}{3}$

Q1 (cont) Orthogonality $\underline{u}_3 = \underline{u}_1 \times \underline{u}_2$

(4)

$$= \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ 1 & -1 & 0 \\ 1 & 1 & -2 \end{vmatrix} = \begin{bmatrix} 2 \\ 2 \\ 2 \end{bmatrix}$$

or $\underline{u}_3 = (1, 1, 1)$

$$[\text{I}] \underline{u}_3 = \frac{ma^2}{3} \begin{bmatrix} 22 \\ 22 \\ 22 \end{bmatrix} = \frac{22ma^2}{3} \underline{u}_3 \quad \therefore \lambda_3 = \frac{22}{3} ma^2$$

(c) G is at $\left[0 \quad \frac{-2a}{3} \quad \frac{2a}{3}\right]$ and note that $[0 \quad -1 \quad 1]$ is principal at 0

$$\text{(check: } [\text{I}] \begin{bmatrix} 0 \\ -1 \\ 1 \end{bmatrix} = \frac{ma^2}{3} \begin{bmatrix} 0 \\ -13 \\ 13 \end{bmatrix} = \frac{13ma^2}{3} \begin{bmatrix} 0 \\ -1 \\ 1 \end{bmatrix}$$

which is consistent with the body being "AAC")
(Another check is that $\begin{bmatrix} 0 \\ -1 \\ 1 \end{bmatrix}$ is \perp $\begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$)

So it's easy to use parallel axis theorem twice

along the $[0 \quad -1 \quad 1]$ axis to get to P
at $[0 \quad -a \quad a]$

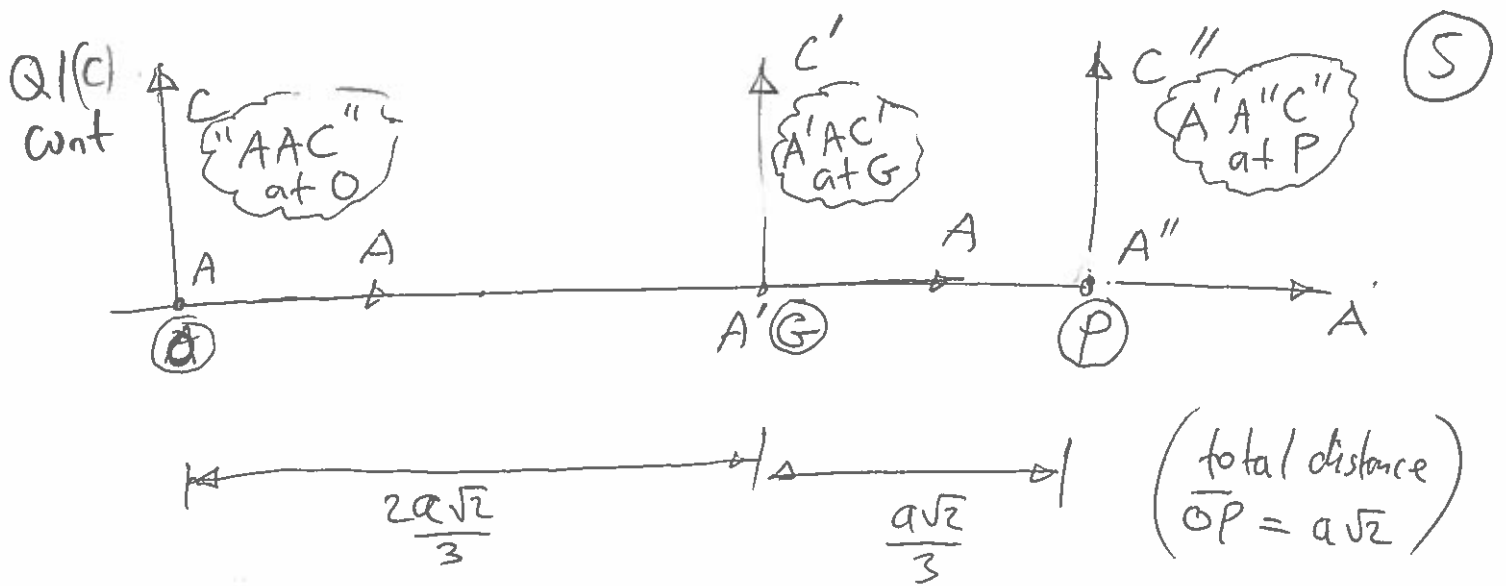
First $O \rightarrow G$ using $\vec{GO} = \begin{bmatrix} 0 & \frac{2a}{3} & -\frac{2a}{3} \end{bmatrix}$

then $G \rightarrow P$ using $\vec{GP} = \begin{bmatrix} 0 & -\frac{a}{3} & \frac{a}{3} \end{bmatrix}$

but do this along $[0 \quad -1 \quad 1]$

$O \rightarrow G$ distance $\frac{2\sqrt{2}a}{3}$

$G \rightarrow P$ distance $\frac{a\sqrt{2}}{3}$



One principal axis $A = \frac{13}{3} ma^2$ is unchanged

C and A first go to C' and A' by subtracting

$$3M \left(\frac{2a\sqrt{2}}{3} \right)^2 \quad \text{then to } C'' \text{ and } A'' \text{ by}$$

$$\text{adding } 3M \left(\frac{a\sqrt{2}}{3} \right)^2$$

$$\text{So } C'' = C + 3M \left(-\left(\frac{2a\sqrt{2}}{3} \right)^2 + \left(\frac{a\sqrt{2}}{3} \right)^2 \right)$$

$$= C - 2Ma^2$$

$$= \left(\frac{22}{3} - 2 \right) Ma^2 = \frac{16}{3} Ma^2$$

$$\text{and } A'' = A - 2Ma^2$$

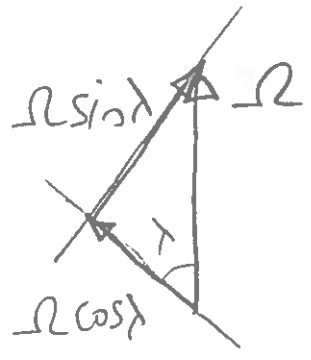
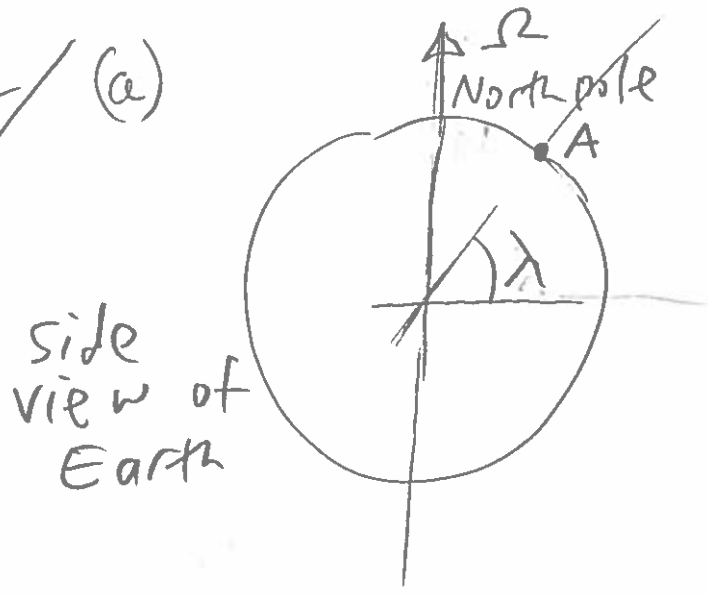
$$= \left(\frac{13}{3} - 2 \right) Ma^2 = \frac{7}{3} Ma^2$$

So principal moments of inertia at P

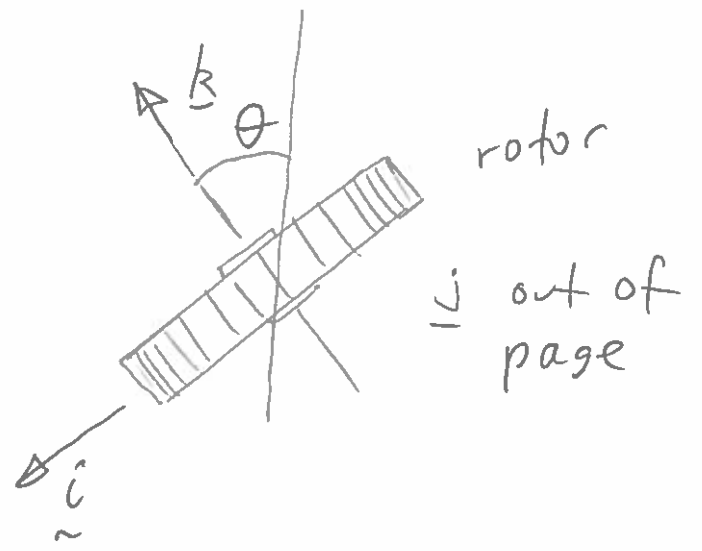
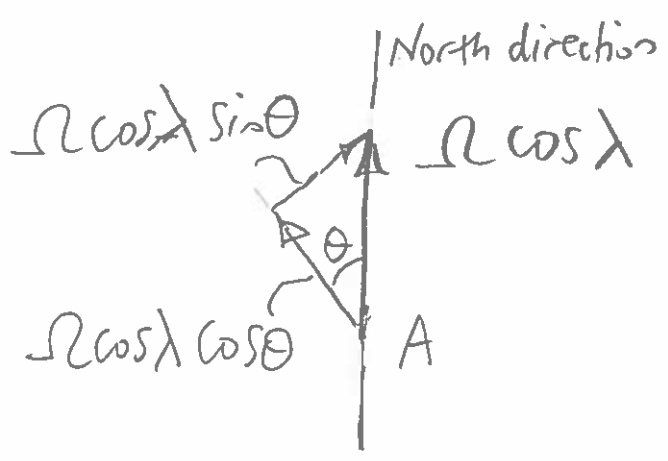
$$\text{are } \left(\frac{7}{3}, \frac{13}{3} \text{ and } \frac{16}{3} \right) Ma^2$$

$$\begin{array}{ccc} \uparrow & \uparrow & \uparrow \\ A'' & A & C'' \end{array}$$

2/ (a)



Top view at A (observing point)



Angular velocity of Earth in $\underline{i} \underline{j} \underline{k}$ frame is

$$-\Omega \cos \lambda \sin \theta \underline{i} + \Omega \sin \lambda \underline{j} + \Omega \cos \lambda \cos \theta \underline{k}$$

Hence $\Omega_1 = -\Omega \cos \lambda \sin \theta$

$$\Omega_2 = \Omega \sin \lambda + \dot{\theta}$$

$$\Omega_3 = \Omega \cos \lambda \cos \theta$$

2(b) Use Gyroscope equations noting
that gimbal is free to turn about
j axis hence $Q_2 = 0$

(7)

Gyro equation "z"

$$A \dot{\Omega}_2 + (A \Omega_3 - C \omega_3) \Omega_1 = Q_2$$

Note: Earth angular velocity is constant

$$\therefore \dot{\Omega}_2 = \ddot{\Theta} \quad \text{and for fast spin}$$

$$C \omega_3 \gg A \Omega_3 \quad \text{and } \omega_3 \approx \omega$$

$$\therefore A \ddot{\Theta} + C \omega \Omega \cos \lambda \sin \Theta \approx 0$$

(c) steady state solution when $\Theta = \text{const}$

$$\therefore \sin \Theta = 0$$

$$\therefore \Theta = 0 \quad \text{or } \pi$$

$$\text{Try } \Theta \approx 0 \quad \therefore \ddot{\Theta} + \frac{C \omega \Omega \cos \lambda}{A} \Theta \approx 0$$

This is SHM hence stable
(use this result in (d))

Try $\Theta = \pi + x$ for small x

$$\therefore \sin \Theta \approx -\sin x \approx -x$$

$$\text{and } \ddot{\Theta} = \ddot{x}$$

8

2(c) cont So

$$\ddot{\alpha} - \frac{C\omega\Omega\cos\lambda}{A} \alpha = 0$$

This leads to $e^{\alpha t}$ solutions
hence unstable.

The stable solution around $\alpha = 0$
means that the gyro compass
oscillates around true north.

The device needs some damping
to make it settle down to $\alpha = 0$

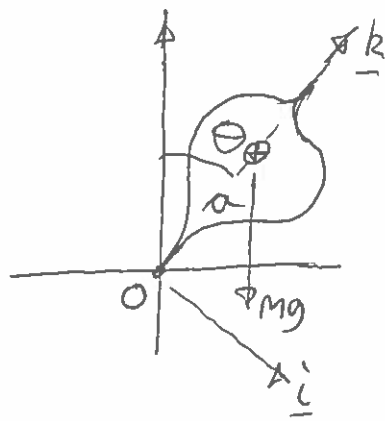
(d) From (c) take SHM
solution

\therefore natural frequency (in rad/s)

$$\text{is } \sqrt{\frac{C\omega\Omega\cos\lambda}{A}} \quad \text{for}$$

small oscillations about true north

Q3(a)



$$\underline{Q} = mga \sin \theta \underline{j}$$

$$\omega_1 = \Omega_1 = -\dot{\phi} \sin \theta \quad (9)$$

$$\omega_2 = \Omega_2 = \dot{\theta}$$

$$\omega_3 = \dot{\phi} \cos \theta$$

$$\omega_3 = \Omega_3 + \dot{\psi} \\ = \text{absolute angular velocity}$$

Use gyro equation (2)

$$"A \dot{\omega}_2 + (A \Omega_3 - C \omega_3) \omega_1 = Q_2" (= mga \sin \theta) \quad (1)$$

But note A, A, C given at G so need to use parallel axis theorem $(A+ma^2), (A+ma^2), C$ for moments of inertia at O

(i) steady state fast spin (1) becomes

$$C \omega_3 \dot{\phi} \sin \theta = mga \sin \theta \quad \therefore \boxed{\dot{\phi} = \frac{mga}{C \omega_3}}$$

$$T = \frac{2\pi}{\dot{\phi}}$$

(ii) steady state not fast spin (1) becomes

$$((A+ma^2) \dot{\phi} \cos \theta - C \omega_3) \dot{\phi} \sin \theta + mga \sin \theta = 0$$

$$\text{Small } \theta \quad \therefore (A+ma^2) \dot{\phi}^2 - C \omega_3 \dot{\phi} + mga = 0$$

$$\text{solution only if } "b^2 - 4ac" \geq 0 \quad \therefore (C \omega_3)^2 \geq 4(A+ma^2) mga$$

$$\therefore \omega_3 \geq \sqrt{\frac{4(A+ma^2) mga}{C^2}} \quad \text{for stable spin}$$

3(b) (i)

Definition of generalised momentum

(10)

$$p_j = \frac{\partial T}{\partial \dot{q}_j} = \frac{\partial}{\partial \dot{q}_j} \left[\frac{1}{2} \sum m_j \dot{q}_j^2 \right]$$

$$= m_j \dot{q}_j \quad \text{as expected for a particle}$$

(ii) Lagrange $\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_j} \right) - \frac{\partial T}{\partial q_j} + \frac{\partial V}{\partial q_j} = 0$

$$\therefore m_j \ddot{q}_j + \frac{\partial V}{\partial q_j} = 0$$

(iii) $H = T + V$

$$= \frac{1}{2} \sum \frac{p_j^2}{m_j} + V(q_1, q_2, \dots, q_j, \dots)$$

So $\frac{\partial H}{\partial p_j} = \frac{p_j}{m_j} = \dot{q}_j$ shown

and $\frac{\partial H}{\partial q_j} = \frac{\partial V}{\partial q_j} = -m_j \ddot{q}_j$ (from (ii))

$$= -\frac{d}{dt} (m_j \dot{q}_j)$$

$$= -\dot{p}_j \quad \text{shown}$$

(11)

$$3b(iv) \quad H = T + V = \text{const}$$

need to show $\frac{dH}{dt} = 0$

$$\frac{d}{dt}(H) = \sum_j \left[\frac{\partial H}{\partial p_j} \dot{p}_j + \frac{\partial H}{\partial q_j} \dot{q}_j \right]$$

$$= \sum_j \left[\dot{q}_j \dot{p}_j - \dot{p}_j \dot{q}_j \right]$$

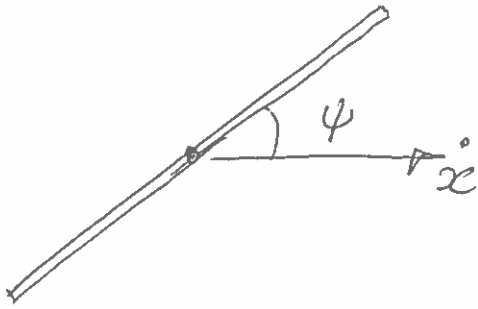
$$= 0$$

So H is const

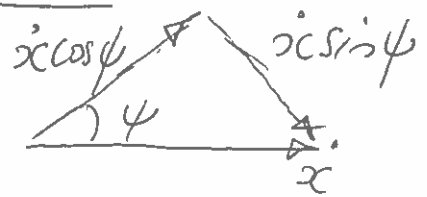
$$\therefore T + V = \text{const}$$

4(a)

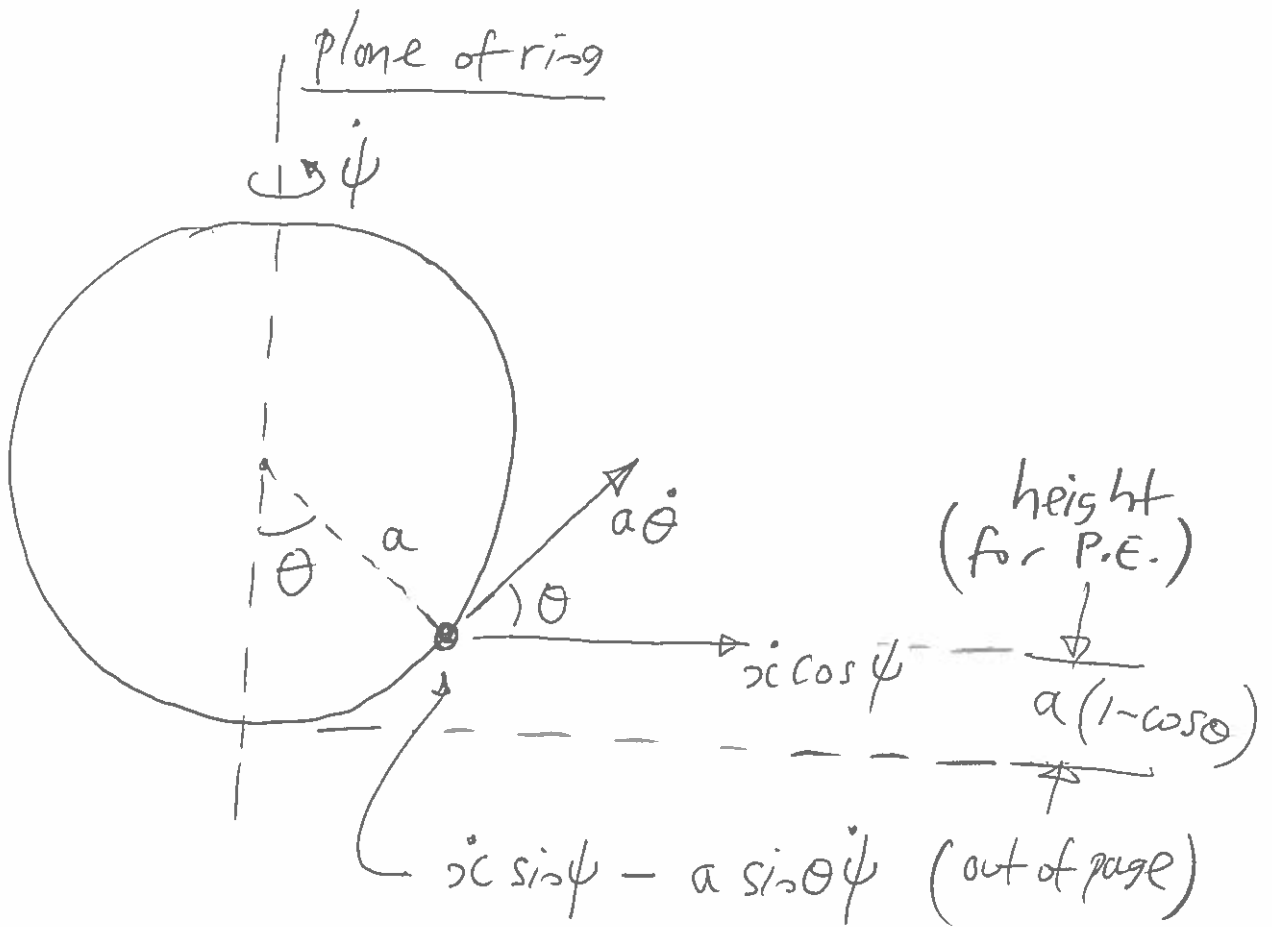
12



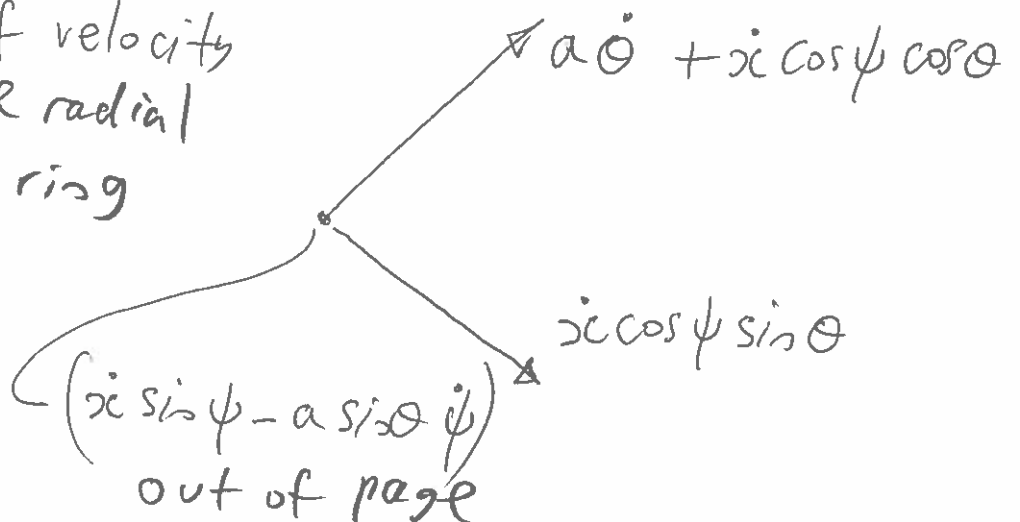
Top view



resolve \dot{x} into plane of ring



Components of velocity tangential & radial and \perp to ring



hence.

$$4(a) \quad T_{\text{bead}} = \frac{1}{2} m \left((a \dot{\theta} + \dot{x} \cos \psi \cos \theta)^2 + (\dot{x} \cos \psi \sin \theta)^2 + (\dot{x} \sin \psi - a \sin \theta \dot{\psi})^2 \right)$$

$$= \frac{1}{2} m \left(a^2 \dot{\theta}^2 + \dot{x}^2 \cos^2 \psi + 2 a \dot{x} \dot{\theta} \cos \psi \cos \theta + (a \sin \theta \dot{\psi} - \dot{x} \sin \psi)^2 \right)$$

as requested

$$\text{Total } T = \frac{1}{2} M \dot{x}^2 + T_{\text{bead}}$$

(b) Generalized momentum: T depends on θ & ψ but not on x so it is possible to define a generalized momentum in x

$$p = \frac{\partial T}{\partial \dot{x}} = (M+m) \dot{x} + m a \dot{\theta} \cos \psi \cos \theta - m a \dot{\psi} \sin \psi \sin \theta$$

$$(c) \quad V = m g a (1 - \cos \theta) + \frac{1}{2} k x^2$$

$$\frac{\partial V}{\partial x} = k x \quad \frac{\partial V}{\partial \theta} = m g a \sin \theta$$

$$\frac{\partial T}{\partial \dot{x}} = (M+m) \dot{x} + m a \dot{\theta} \cos \psi \cos \theta - m a \dot{\psi} \sin \psi \sin \theta$$

$$\frac{\partial T}{\partial x} = 0$$

$$\frac{\partial T}{\partial \dot{\theta}} = m a^2 \dot{\theta} + m a \dot{x} \cos \psi \cos \theta$$

$$\frac{\partial T}{\partial \theta} = -m a \dot{x} \sin \theta \cos \psi + m a \omega \dot{\psi} (a \sin \theta \dot{\psi} - \dot{x} \sin \psi)$$

(13)

4c cont
Lagrange for x

(14)

$$\frac{d}{dt} \left((M+m)\dot{x} + ma\dot{\theta} \cos\psi \cos\theta - ma\dot{\psi} \sin\psi \sin\theta \right) + kx = 0$$

and note that $\dot{\psi} = \text{const} (= -\Omega)$

$$\therefore (M+m)\ddot{x} + ma\ddot{\theta} \cos\psi \cos\theta - ma\dot{\theta}^2 \cos\psi \sin\theta - ma\dot{\theta} \dot{\psi} \sin\psi \cos\theta + kx = 0 \quad \text{①}$$

Lagrange for θ

$$\frac{d}{dt} \left[ma^2 \dot{\theta} + ma\dot{x} \cos\psi \cos\theta \right] + ma\dot{x} \dot{\theta} \cos\psi \sin\theta - ma^2 \dot{\psi}^2 \sin\theta \cos\theta + ma\dot{x} \dot{\psi} \sin\psi \cos\theta + mga \sin\theta = 0$$

$$\therefore a\ddot{\theta} + \dot{x} \cos\psi \cos\theta - a\dot{\psi}^2 \sin\theta \cos\theta + g \sin\theta = 0 \quad \text{②}$$

and there is no equation for ψ
 other than $\dot{\psi} = \text{const} = -\Omega$

4(c) cont

(15)

For "static" solutions

$$x = \text{const}$$

$$\theta = \text{const}$$

$$\therefore \dot{x} = \ddot{x} = 0$$

$$\dot{\theta} = \ddot{\theta} = 0$$

\therefore (1) is satisfied

and (2) gives $-a \dot{\psi}^2 \sin\theta \cos\theta + g \sin\theta = 0$

$$\therefore (g - a \dot{\psi}^2) \sin\theta = 0$$

for which there are two solutions

$$\theta = 0 \quad \text{and} \quad \theta = \pi$$

For small oscillations the θ equation becomes

$$\theta \approx 0 \quad a \ddot{\theta} + \cos\psi \ddot{x} + (g - a \dot{\psi}^2) \theta = 0$$

$$\theta = \pi + z \quad a \ddot{z} - \cos\psi \ddot{x} - (g + a \dot{\psi}^2) z = 0$$



Stiffness term

For small θ , stiffness is positive for $g - a \dot{\psi}^2 > 0$

for θ around π , stiffness is always negative

So the $\Theta = 0$ solution is
 the only stable one and then
 only for $g - a\dot{\psi}^2 > 0$

(d) put (1) & (2) into matrix form

$$\begin{bmatrix} M+m & ma \cos \psi \\ \cos \psi & a \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{\Theta} \end{bmatrix} + \begin{bmatrix} 0 & -m a \dot{\psi} \sin \psi \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{\Theta} \end{bmatrix} + \begin{bmatrix} k & 0 \\ 0 & g - a\dot{\psi}^2 \end{bmatrix} \begin{bmatrix} x \\ \Theta \end{bmatrix} = 0$$

with $\psi = \Omega t$ $\dot{\psi} = \Omega$

Note time-varying mass matrix
 and damping matrix

HEM Hunt
 May 2016