367-2015

1) 
$$\phi = \frac{5}{\sqrt{2}} \cos(\alpha \pi)(1 + \alpha y)e^{-\alpha y}$$
,  $\alpha = \frac{2\pi}{\sqrt{2}}$ 

$$\frac{\partial^2 \phi}{\partial n^2} = - \epsilon_0 \cos(\alpha x) \left( (1 + x y) e^{-x y} \right)$$

$$\frac{\partial \phi}{\partial y} = \frac{60}{\chi^2} \cos(\chi n) \left[\chi e^{-\chi y} - \chi (1 + \chi y) e^{-\chi y}\right]$$







 $\frac{1}{2} = \frac{1}{2} = \frac{1}$ 

 $\overline{G}_{yy} = -\overline{G}_{G}(\alpha x) \left[ (1+\alpha y) e^{-\alpha y} \right]$ Eny = - 50 sm(xx) [xy e-xy]

Check for compatibulity  $f^{2} \in \pi n + \epsilon_{yy} = -2 \in coo(kn) e^{-ky}$   $\frac{\partial^{2} f}{\partial n^{2}} = 2 \in coo(kn) e^{-ky}$   $\frac{\partial^{2} f}{\partial y^{2}} = -2 \in coo(kn) e^{-ky}$   $\frac{\partial^{2} f}{\partial y^{2}} = -2 \in coo(kn) e^{-ky}$   $= -2 \in coo(kn) e^{-ky}$ 

Check boandary conditions  

$$G_{ny} = 0$$
 on  $y = 0$   $V$   
 $G_{yy}$  on  $y = 0 = 3 - G cos(dn)$   $V$ 



$$k = \frac{p}{2}$$

$$k = c_{0} (y) e^{-x} y$$

$$Max \quad dt \quad y = \frac{1}{2}$$

$$\Rightarrow c_{0} = \frac{p}{2}$$

$$(c) \quad Mohris \quad wick \quad bugget \quad dt \quad ay = 1$$

$$von \quad Mais \quad wick \quad bugget \quad at \quad ay = 1$$

$$von \quad Mais \quad wick \quad bugget \quad dt \quad ay = 1$$

$$(c_{1} - c_{2})^{2} + (c_{2} - c_{3})^{2} + (c_{3} - c_{1})^{2} - 6k^{2}$$

$$c_{1} - c_{2})^{2} + (c_{2} - c_{3})^{2} + (c_{3} - c_{1})^{2} - 6k^{2}$$

$$\Rightarrow D^{2} + (c_{nx} + c_{yy} + \frac{p}{2})^{2} + (c_{nx} + c_{yy} - \frac{p}{2})^{2} - 6k^{2}$$

$$\Rightarrow D^{2} + (c_{nx} + c_{yy} + \frac{p}{2})^{2} + (c_{nx} + c_{yy} - \frac{p}{2})^{2} - 6k^{2}$$

$$D = D^{2} + 2(c_{nx} + c_{yy})^{2} + 2(\frac{p}{2})^{2} - 6k^{2}$$

$$D = c_{1} + c_{2} = 0 \quad a_{1} = a_{2} = 0$$

$$\frac{460}{2^2} = -6k^2$$
  
 $\frac{3}{4} = -6k^2$   
 $\frac{3}{4} = k$   
 $\frac{3}{4} = k$   
 $\frac{3}{4} = -k$   
 $\frac{50}{4} = -\frac{\sqrt{3}}{4} = k$ 

len.

2(a)

$$\frac{\partial \phi}{\partial r} = \frac{2Mr}{a^2} + \frac{N}{r}$$
$$\frac{\partial^2 \phi}{\partial r} = \frac{2M}{a^2} - \frac{N}{r^2}$$

$$\frac{\partial^2 \phi}{\partial r^2} = \frac{2M}{a^2} - \frac{N}{r^2}$$

$$6_{rr} = \frac{2M}{a^2} + \frac{N}{r^2}$$

$$6_{00} = \frac{2M}{a^2} - \frac{N}{r^2}$$

Matches Lones with choice 
$$A = \frac{3M}{\alpha^2}$$
,  $B = -N$ 

(h)  

$$r \rightarrow \infty$$
  $G_{rr} = 5_{0} = G_{00}$   
 $f = amme \quad hole \quad g \quad pradius \quad a$   
 $at r = a \quad , \quad G_{rr} = 0$   
 $G_{rr} = A - B \quad , \quad G_{00} = A + B \quad r^{2}$   
 $A = 5_{0} \quad B = 5_{0}a^{2}$   
 $G_{rr} = G_{0} \left(1 - \left(\frac{a}{r}\right)^{2}\right)$   
 $G_{00} = S_{0} \left(1 + \left(\frac{a}{r}\right)^{2}\right)$   
 $G_{00} = S_{0} \left(1 + \left(\frac{a}{r}\right)^{2}\right)$ 

SCF = 2

 $a \frac{\partial \phi}{\partial r} = a^2 \frac{\sigma}{\sigma} \cos 2\theta \left( - \left(\frac{r}{a}\right) + \left(\frac{a}{r}\right)^3 \right)$ 

 $(\mathcal{C})$ 

$$\frac{a^2}{\partial r^2} = -a^2 = -a^2$$

$$\frac{1}{r} \frac{\partial \phi}{\partial \phi} = \alpha \epsilon_0 \sin 2\phi \left[ \left( \frac{r}{a} \right) - \frac{2\alpha}{r} + \left( \frac{\alpha^3}{r^3} \right) \right]$$

$$\frac{\partial^2 \phi}{\partial a^2} = a^2 = a^2 = a^2 = (a^2)^2 - 4 + 2(\frac{a}{r})^2$$

$$G_{\mu} = G_{\mu} \cos 20 \left[ -1 + \left( \frac{a}{r} \right)^4 - 4 \left( \frac{a}{r} \right)^2 + 2 + 2 \left( \frac{a}{r} \right)^4 \right]$$

$$r=\alpha$$
,  $\epsilon_{rr}=0$   $V$   
 $r=\infty$ ,  $\epsilon_{rr}=\epsilon_{0}$   $corrow$ 

$$\begin{aligned} & 6_{00} = -6_{0} \cos 20 \left( 1 + 3 \left( \frac{a}{r} \right)^{4} \right) \\ & r \to \infty \qquad 6_{00} = -6_{0} \cos 20 \\ & 6_{r0} = 6_{0} \sin 20 \left[ -1 - 2 \left( \frac{a}{r} \right)^{2} + 3 \left( \frac{a}{r} \right)^{4} \right] \end{aligned}$$

$$F = a \quad \epsilon_{ra} = 0 \quad \Rightarrow \text{ satisfies BC on hole}$$

$$Permetty$$

$$\epsilon_{rr} = \epsilon_{0} \cos 20$$

$$\epsilon_{oe} = -\epsilon_{o} \cos 20$$

$$\epsilon_{o} = -\epsilon_{o} \cos 20$$

at edge of hole 
$$= jn \ 0 = \frac{\pi}{2}$$
  
 $= 500 = 450$   
 $= 500 = 450$ 

$$3_{(\alpha)} \qquad u = Cr + \underline{D} \\ r$$

$$G_{rr} = \frac{du}{dr} = C - \underline{D}_{r2}$$

$$G_{o\alpha} = \frac{u}{r} = C + \underline{D}_{r2}$$

$$G_{uddbm} \approx G_{oo} = \frac{d}{dr} (r - G_{rr})$$

$$G_{rr} = \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ f_{rr} + \overline{v} - f_{oa} \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C - \frac{D}{r^{2}} + \overline{v} (C + \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C + \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= \frac{\overline{E}}{1 - \overline{v}^{2}} \left[ C + \frac{D}{r^{2}} + \overline{v} (C - \frac{D}{r^{2}}) \right]$$

$$= C' + \frac{D}{r^{2}}$$

$$\frac{d}{dr} \left( r - C' - \frac{D}{r} \right) = C' + \frac{D}{r^{2}} = G_{oa}$$

$$\frac{d}{dr} \text{ satisfy s equilibrum.}$$

$$\frac{dv}{(1)} \text{ outra readus unconstraind} \Rightarrow \frac{dv}{rr}\Big|_{r=2u} = 0$$

$$C^{1} = \frac{D^{1}}{4a^{2}}$$

$$D^{1} = 4a^{2}C^{1}$$

$$(1-\overline{v})\frac{D\overline{E}}{1-\overline{v}^{2}} = 4a^{2} \frac{\overline{E}(1+\overline{v})}{1-\overline{v}^{2}}C \qquad \overline{z} + \frac{1+\overline{v}}{1-v}$$

$$D = 4a^{2}(1+\overline{v}) = \frac{1}{1-v}$$

$$1-\overline{v} = 1-\frac{v}{1-v}$$

$$1-\overline{v} = 1-\frac{v}{1-v}$$

$$D = \frac{4a^2}{1-2\nu} C = \frac{1-2\nu}{1-\nu}$$

$$= 7 u = Cr + 4a^2C + 1 - 2v r$$

$$at r = a$$
,  $u = 0.01a$ 

$$0.01q = C \left[ a (120) + 4a \right]$$
  
 $1 - 2y$ 

$$C = 0.01 \left( \frac{1-2\nu}{5-2\nu} \right)$$

$$D = 4a^2 \quad 0.01 \\ 5-2v$$

at r=2a

$$u = \frac{0.01}{5-2\nu} \left[ (1-2\nu) 2a + \frac{4a^2}{2a} \right]$$
  
= 0.04a  $\left( \frac{1-\nu}{5-2\nu} \right) + \frac{0.02a}{(5-2\nu)}$ 

(ii) 
$$u(2\alpha) = 0$$
  
 $0 = C_{2\alpha} + \frac{D}{\alpha \alpha} \implies D = -4\alpha^{2}C$   
 $r=\alpha, \alpha = 0.01\alpha$   
 $0.01\alpha = C_{\alpha} - \frac{4\alpha^{2}C}{\alpha} = -3C\alpha$   
 $C = \frac{0.01}{3}, D = \frac{0.04\alpha^{2}}{3}$   
 $C = \frac{0.01}{3}, D = \frac{0.04\alpha^{2}}{3}$   
 $C = \frac{0.01}{3} \begin{bmatrix} -\frac{1}{1-37} - \frac{0.01}{1+77} \end{bmatrix}$   
 $= -\frac{0.01E}{3} \begin{bmatrix} -\frac{1}{1-37} - \frac{1}{1+77} \end{bmatrix}$   
 $(r-v)(1-2v)$   
 $i = r-2v+4v^{2}$   
 $i = -\frac{0.01}{3} \begin{bmatrix} E}{(1-v)} \begin{bmatrix} \frac{1-70}{1-2}v + \frac{1}{1-77} \end{bmatrix}$   
 $= -\frac{0.01}{3} \begin{bmatrix} E}{(1+v)(1-v)} \begin{bmatrix} \frac{2-4v+2v^{2}}{1-2v} \end{bmatrix}$   
 $= -0.01E_{3}^{2} \in (\frac{1-v^{2}}{1+77})$ 

4(a)

$$\hat{\varepsilon}_{rr} = \frac{du}{dr} = -\frac{A}{r^2}$$
$$\hat{\varepsilon}_{oe} = \frac{du}{r} = \frac{A}{r^2}$$
$$\hat{\varepsilon}_{zz} = 0$$

 $W = 600 \dot{E}00 + 6rr \dot{E}rr$ =  $(600 - 6rr) \dot{A}$  $r^2$ 

But since  $\tilde{\epsilon}_{rr} = -\tilde{\epsilon}_{oo} =>$  acture yield ortern is

$$= \frac{b}{dt} = \int \frac{d}{dt} \frac{d}{dt} = 2\pi dt = 2$$

work done by pressure = RTia puff=a = RTTa p A

=> 
$$2\pi pA = 2\pi A Gy lm(\frac{b}{a})$$
  
 $p = Gy lm(\frac{b}{a})$ 

$$(h)$$

$$\dot{w} = 8 \int_{0}^{T/4} \int_{-\infty}^{C} \sigma_{1A} r dr d\alpha$$

$$= 8 \sigma_{1A} \int_{0}^{T/4} \ln\left(\frac{*c}{2\alpha \cos \alpha}\right) d\alpha$$

$$= 8 \epsilon_{TA} \left[ \frac{T}{4} ln\left(\frac{c}{aa}\right) - \int_{0}^{T} ln(coo) do \right]$$

$$\dot{w} = 86_{T}A \left[\frac{\pi}{4}lm\left(\frac{c}{2a}\right) + 0.086\right]$$

$$p = 4 = 8 = 7 A \left[ \frac{\pi}{4} \ln \left( \frac{c}{2a} \right) + 0.086 \right]$$

$$p = 4 = \frac{4}{\pi} \left[ \frac{\pi}{4} \ln \left( \frac{c}{2a} \right) + 0.086 \right]$$

# **Comments on questions**

## Q1 Airy stress function in a half-space & application of yield criteria

A question that was reasonably well-attempted. Most students struggled on part (c) in attempting to use the von-Mises criterion to predict first yield. They were unable to determine the location at which yielding initiated in this half-space.

### Q2 Airy stress functions in polar co-ordinates

Generally the students had no problems with this question with a number of candidates being awarded 100% on this question. Some students struggled in the co-ordinate rotation to determine the SCF under pure shear.

# Q3 Axi-symmetric elastic fields

While most candidates answered part (a) well they struggled with both subsections of part (b). They struggled to correctly apply the boundary conditions as specified in the question.

# Q4 Upper bound plastic collapse calculation

A very unpopular question. The assessor is surprised at this given that part (a) was basically covered in the lecture notes and was a direct application of the upper bound method. Of the 6 students who attempted it 2 were awarded 100% on the question.