

(1.1)

$$(i) \quad -EAu'' = -\alpha u$$

Multiply by test function  $v$  and integrate

$$-\int_0^L EA v u'' dx + \int_0^L \alpha v u dx$$

Integration by parts:

$$\int_0^L EA v' u' dx - v EA u' \Big|_0^L + \int_0^L \alpha v u dx$$

Since  $u=0$  at  $x=0$ ,  $v(0)=0$ , using this

and insert the Neumann (force) boundary condition:

$$\int_0^L (EA u' v' + \alpha u v) dx = v F \Big|_{x=L}$$

(ii) To integrate exactly, term  $\alpha v u$  has highest degree.

Use Gauss quadrature, which with  $n$  points can

integrate a polynomial of degree  $2n-1$  exactly. Therefore:

- P1 element: use 2 points (integrand is polynomial degree 2)
- P2 element: use 3 points (integrand is polynomial degree 2)

(iii) In a finite element implementation, ~~zero~~ <sup>set</sup> rows and columns for degree of freedom associated with Dirichlet boundary condition and set 1 on corresponding diagonal terms. Or remove the associated rows and columns from the system.

1.2

(i)



Left-hand side

$$\int_0^{L/3} (EA v' u' + \alpha uv) dx = v^-(u^+ - \bar{u}) k \Big|_{L/3}$$

Right-hand side

$$\int_{L/3}^L (EA v' u' + \alpha uv) dx = -v^+(u^+ - \bar{u}) k \Big|_{L/3} + VF/L$$

Combining:

$$\int_0^L (EA u' v' + \alpha uv) + k(v^+ - v^-)(u^+ - \bar{u}) \Big|_{x=L/3} = VF/L$$

(ii) If  $\alpha = k = 0$ , system would be singular.

Q2

(a) (i) A priori error estimate:  $\|e\| \leq (Ch)^{p+1} / |u|_r$

$h_1$ : cell size original <sup>mesh</sup> ~~mesh~~  
 $h_2$ : cell size refined mesh

To halve error:  $\frac{h_1^{p+1}}{2} = h_2^{p+1}$

$p$ : polynomial degree

↑ exact soln

$$\therefore h_2 = \frac{h_1}{2^{(\frac{1}{p+1})}}$$

linear elements ( $p=1$ ):  $h_2 = \frac{1}{\sqrt{2}} h_1$

quadratic element ( $p=2$ ):  $h_2 = \frac{1}{\sqrt[3]{2}} h_1$

Same in 2D & 3D.

(ii) 3D:  $n \propto \frac{1}{h^3} \therefore \text{cost } O\left(\frac{1}{h^6}\right)$

$$n_2 = \frac{1}{h_2^3} = \frac{2}{h_1^3} \therefore \text{cost } O\left(\frac{4}{h_1^6}\right)$$

$\therefore$  Cost increase by factor of 4

(iii) A priori estimate rely on sufficiently smooth exact solution. If not smooth enough, increasing element degree will not reduce error

Q 2 (cont)

(5) (i) Assembly cost is proportional to number of elements. Number of elements ( $n$ ) is proportional to number of elements.

$\therefore$  cost will double

(ii) In 3D, increase cell count by factor of 8 correspond to halving cell size,  
$$h_2 = \frac{h_1}{2}$$

$\therefore$  Critical time step  $\propto h^2$ ,  $\therefore$  time step must be reduced by 4.

Cost per time step increases by factor of 8, and 4 times the number of steps required.

$\therefore$  Increase in cost is  $4 \cdot 8 = \underline{32}$

(iii) The time step restriction of  $\Delta t \propto \tau^2$  is very strong. Implicit method, which can be constructed to have no time step restriction, would be better.

3.1

(a)  $x = 2 + \xi(5-2) + \eta(3-2) = 2 + 3\xi + \eta$   
 $y = 1 + \xi(3-1) + \eta(4-1) = 1 + 2\xi + 3\eta$

for  $\xi = \frac{1}{3}, \eta = \frac{1}{3}$

P : 
$$\begin{cases} x = 2 + 1 + \frac{1}{3} = \frac{10}{3} \\ y = 1 + \frac{2}{3} + 1 = \frac{8}{3} \end{cases}$$

(b) 
$$\underline{J} = \begin{pmatrix} 3 & 2 \\ 1 & 3 \end{pmatrix}, \det(\underline{J}) = 7$$
 the area of the triangle is  $A = \frac{7}{2}$

(c) 
$$\frac{\partial N_i}{\partial \xi} = \frac{\partial N_i}{\partial x} \cdot \frac{\partial x}{\partial \xi} + \frac{\partial N_i}{\partial y} \cdot \frac{\partial y}{\partial \xi}$$

$$\frac{\partial N_i}{\partial \eta} = \frac{\partial N_i}{\partial x} \cdot \frac{\partial x}{\partial \eta} + \frac{\partial N_i}{\partial y} \cdot \frac{\partial y}{\partial \eta}$$

$$\begin{pmatrix} \frac{\partial N_1}{\partial \xi} \\ \frac{\partial N_1}{\partial \eta} \end{pmatrix} = \begin{pmatrix} \frac{\partial N_1}{\partial x} & \frac{\partial N_1}{\partial y} \\ \frac{\partial N_2}{\partial x} & \frac{\partial N_2}{\partial y} \end{pmatrix} \begin{pmatrix} \frac{\partial x}{\partial \xi} \\ \frac{\partial y}{\partial \xi} \end{pmatrix}$$

$$\begin{pmatrix} \frac{\partial N_1}{\partial \xi} \\ \frac{\partial N_1}{\partial \eta} \end{pmatrix} = \begin{pmatrix} 3 & 2 \\ 1 & 3 \end{pmatrix}^{-1} \begin{pmatrix} \frac{\partial N_1}{\partial x} \\ \frac{\partial N_1}{\partial y} \end{pmatrix} = \frac{1}{7} \begin{pmatrix} 3 & -2 \\ -1 & 3 \end{pmatrix} \begin{pmatrix} \frac{\partial N_1}{\partial x} \\ \frac{\partial N_1}{\partial y} \end{pmatrix}$$

$$= \begin{pmatrix} \frac{3}{7} & -\frac{2}{7} \\ -\frac{1}{7} & \frac{3}{7} \end{pmatrix} \begin{pmatrix} \frac{\partial N_1}{\partial x} \\ \frac{\partial N_1}{\partial y} \end{pmatrix}$$

3.2

$$(d) N_5 = 4\eta\xi$$

$$x = 2 + 3\xi + \eta \quad (1)$$

$$y = 1 + 2\xi + 3\eta \quad (2)$$

$$3 \times (1) - (2) \quad 3x - y = 5 + 7\xi$$

$$\xi = \frac{1}{7}(3x - y - 5)$$

$$2 \times (1) - 3 \times (2) \quad 2x - 3y = -1 - 7\eta$$

$$\eta = \frac{1}{7}(3y + 1 - 2x)$$

$$\text{Hence } N_5 = \frac{4}{49}(3x - y - 5)(3y + 1 - 2x)$$

$$(e) N_4 = 4\xi(1 - \xi - \eta)$$

$$\frac{\partial N_4}{\partial \xi} = 4 - 8\xi - 4\eta, \quad \frac{\partial N_4}{\partial \eta} = -4\xi$$

$$\begin{aligned} \frac{\partial N_4}{\partial x} &= \frac{\partial N_4}{\partial \xi} \frac{\partial \xi}{\partial x} + \frac{\partial N_4}{\partial \eta} \frac{\partial \eta}{\partial x} = \frac{2}{7}(4 - 8\xi - 4\eta) - \frac{2}{7} \times 4\xi \\ &= \frac{12}{7} - \frac{32}{7}\xi - \frac{12}{7}\eta \end{aligned}$$

$$\int_K \frac{\partial N_4}{\partial x} \cdot \frac{\partial N_4}{\partial x} dx dy = \int_{\hat{K}} \frac{\partial N_4}{\partial x} \cdot \frac{\partial N_4}{\partial x} \det(J) d\xi d\eta.$$

$$= \left( \frac{\partial N_4}{\partial x} \right)^2 \left( \frac{1}{3}, \frac{1}{3} \right) \times 7 \times \frac{1}{2} = 0.508$$

$$\frac{\partial N_4}{\partial x} \left( \frac{1}{3}, \frac{1}{3} \right) = -0.381$$

4.1

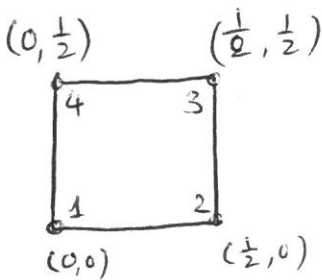
(a) Let the square is noted as  $\Omega$  and  $v$  a test function where  $v=0$  at  $\partial\Omega$ .

$$\int_{\Omega} v \nabla^2 u \, dx dy = - \int_{\Omega} v \, dx dy$$

Integrate by part

$$\int_{\Omega} \nabla u \nabla v \, dx dy = \int_{\partial\Omega} \frac{\partial u}{\partial n} v \, dl + \int_{\Omega} v \, dx dy.$$

(b)  $N_1^e = 4(\frac{1}{2} - x)(\frac{1}{2} - y)$   
 $N_2^e = 4x(\frac{1}{2} - y)$   
 $N_3^e = 4xy$   
 $N_4^e = 4(\frac{1}{2} - x)y$



(i)  $B^e = \begin{bmatrix} \frac{\partial N_1^e}{\partial x} & \frac{\partial N_1^e}{\partial y} \\ \frac{\partial N_2^e}{\partial x} & \frac{\partial N_2^e}{\partial y} \\ \frac{\partial N_3^e}{\partial x} & \frac{\partial N_3^e}{\partial y} \\ \frac{\partial N_4^e}{\partial x} & \frac{\partial N_4^e}{\partial y} \end{bmatrix} = \begin{bmatrix} -2+4y & 2-4y & 4y & -4y \\ -2+4x & -4x & 4x & 2-4y \end{bmatrix}$

(ii)  $K_{11} = \int_0^{\frac{1}{2}} \int_0^{\frac{1}{2}} \frac{\partial N_1}{\partial x} \frac{\partial N_1}{\partial x} + \frac{\partial N_1}{\partial y} \frac{\partial N_1}{\partial y} \, dx dy = \int_0^{\frac{1}{2}} \int_0^{\frac{1}{2}} (2+4y)^2 + (-2+4x)^2 \, dx dy =$

$K_{12} = \int_0^{\frac{1}{2}} \int_0^{\frac{1}{2}} (-2+4y)(2-4y) + (2-4x)(4x) \, dx dy = -\frac{1}{3}$

$K_{13} = \int_0^{\frac{1}{2}} \int_0^{\frac{1}{2}} (-2+4y)(4y) + (-2+4x)(4x) \, dx dy = -\frac{2}{3}$

$K_{14} = K_{12} = -\frac{1}{3}$  (by symmetry).

We can complete the matrix conductant mat by symmetry.

$$K^e = \frac{1}{3} \begin{bmatrix} 4 & -1 & -2 & -1 \\ & 4 & -1 & -2 \\ & & 4 & -1 \\ & & & 4 \end{bmatrix}$$

4.2

$$(b) \text{ (iii) } f_3 = \int_0^{\frac{1}{2}} \int_0^{\frac{1}{2}} 4xy \, dx \, dy = 4 \int_0^{\frac{1}{2}} x \, dx \int_0^{\frac{1}{2}} y \, dy = 4 \left. \frac{x^2}{2} \right|_0^{\frac{1}{2}} \left. \frac{y^2}{2} \right|_0^{\frac{1}{2}} = \frac{1}{16}$$

by symmetry  $f_1 = f_2 = f_4 = \frac{1}{16}$ .

(c) The only unknown is at node 5. The equation for node 5 is

$$-\frac{2}{3}u_1 - \frac{2}{3}u_2 - \frac{2}{3}u_3 - \frac{2}{3}u_4 + \frac{16}{3}u_5 - \frac{2}{3}u_6 - \frac{2}{3}u_7 - \frac{2}{3}u_8 - \frac{2}{3}u_9 = 4 \times \frac{1}{16}$$

$-\frac{2}{3}$	$-\frac{1}{3}$	$-\frac{1}{3}$	$-\frac{2}{3}$
$-\frac{1}{3}$	$\frac{4}{3}$	$\frac{4}{3}$	$-\frac{1}{3}$
$-\frac{1}{3}$	$\frac{4}{3}$	$\frac{4}{3}$	$-\frac{1}{3}$
$-\frac{2}{3}$	$-\frac{1}{3}$	$-\frac{1}{3}$	$-\frac{2}{3}$

Applying boundary condition  $u_1 = \dots = u_4 = 0$

$$u_6 = \frac{1}{4}, \quad u_7 = u_8 = u_9 = 0,$$

$$\cancel{u_5 = \frac{3}{64}} \quad \frac{16}{3}u_5 - \frac{2}{3} \times \frac{1}{4} = 4 \times \frac{1}{16}$$

$$u_5 = \frac{9}{64}$$