۱

(a) 
$$x \in Ut \Rightarrow V(H \in u(Vt) \Rightarrow E[V(Hv(H+T)] \in E[u(Vt)u(Ut+VT)]$$
  
T  
 $T$   
 $Uhu displatement$   
 $R_{UV}(T) = Ae^{-\alpha V(T)}$   
 $S_{UV}(u) \stackrel{t}{2\pi} \int_{-\alpha}^{\alpha} e^{iuT} Ae^{-\alpha V(T)} dT = \frac{A}{2\pi} \left\{ \int_{0}^{\infty} e^{iuT - \alpha VT} dT + \int_{-\alpha}^{0} e^{iuT + \alpha VT} dT \right\}$   
 $= \frac{A}{2\pi} \left\{ \int_{0}^{\infty} e^{iuT - \alpha VT} dT + \int_{-\alpha}^{0} e^{iuT + \alpha VT} dT \right\}$   
 $= \frac{A}{2\pi} \left\{ \frac{1}{iu + \alpha V} - \frac{1}{iu^{2} - \alpha V} \right\} = \frac{A}{\pi} \left\{ \frac{\alpha V}{u^{2} + \alpha^{2} U^{2}} \right\}$  [25%]  
(b) By inspection  $M \ddot{y} + c(\dot{y} - \dot{y}) + k(\dot{y} - \dot{y}) = 0$   
Pat  $\Gamma = y - v$ , idative displatement  
 $\Rightarrow M \ddot{r} + C \dot{r} + kr = M \ddot{v}$ 

Assume  $\Gamma = \Gamma(\omega)e^{i\omega t}$  and  $\sigma = \sigma(\omega)e^{i\omega t}$  to give  $\Gamma(\omega) = \left(\frac{-M\omega^{2}}{-M\omega^{2} + Ci\omega + k}\right)\sigma(\omega) = H(\omega)\sigma(\omega)$   $\Gamma(\omega) = \int_{\Gamma(\omega)}^{\infty} \frac{1}{\Gamma(\omega)} \int$ 

$$= \int_{\Gamma} \int_{\Gamma} \int_{\Gamma} \int_{\Gamma} \left[ H(\omega) \right]^{2} \int_{\sigma} \int_{\sigma} \int_{\Gamma} \int_{\Gamma}$$

Assume broad banded  $\Rightarrow$  Replace with white noise at the resonant frequency  $S_{0} = \frac{H}{TT} \left\{ \frac{M^{2} w_{n}^{5} \alpha V}{w_{n}^{2} + \alpha^{2} V^{2}} \right\}$ From data sheet  $\sigma_{T}^{2} = \frac{TTS_{0}}{Ck} = \sigma_{F}^{2} \cdot k^{2} \sigma_{T}^{2} = TTkS_{0}/C$ Nothing that  $M^{2} w_{n}^{4} = k^{2}$ , then  $\sigma_{F}^{2} = \frac{H}{C} \left\{ \frac{k^{3} \alpha V}{w_{n}^{2} + \alpha^{2} V^{2}} \right\}$  [25%]

(d) from port (b), if 
$$M \rightarrow \infty$$
 then  $H(\omega) \rightarrow 1$  and  $SH(\omega) \rightarrow k^2 SHr(\omega)$   
This Makes sense, because the mass will not move as  $M \rightarrow \omega$  and we  
will have  $\Gamma(H) \cdot \sigma(H)$ . In this case  $\sigma_F^2 : k^2 \sigma_F^2 : \frac{k^2 A}{2}$ 

White noise approximation breaks down because H(w)=1 is very broad and the input spectrum cannot be broader than this! E20%]

2.(a)  

$$\int \frac{1}{2} \frac{y(t)}{1} \qquad fut \quad r : x(t) - y(t)$$

$$\int \frac{1}{2} \frac{y(t)}{1} \qquad fut \quad r : x(t) \quad \alpha(cur \ ir \quad r^{2}d \Rightarrow hucl \ (rossing problem)$$

$$r^{2} : x^{2} - 2xy + y^{2} \Rightarrow \sigma_{r}^{2} : \sigma_{x}^{2} + \sigma_{y}^{2} : \sigma_{r}^{2} + \sigma_{r}^{2} : \frac{1}{2} + 27y^{2} : 9760$$

$$\Rightarrow \sigma_{r}^{2} : 1 \qquad \text{and} \quad \sigma_{r}^{2} : 279.9$$

$$V_{d}^{T} : \frac{1}{2\pi} \left(\frac{\sigma_{r}}{\sigma_{r}}\right) = \frac{1}{2} \frac{y(d)\sigma_{r}}{2} : \left(\frac{1}{2\pi}\right) \left(\frac{299}{1}\right) = \frac{1}{2} \frac{y(5/1)^{2}}{2} : (.779 \times 10^{-6})$$

$$Robability \quad di \ impact = 1 - e^{-V_{d}T} = 1 - e^{-1.779 \times 10^{-6}} \times 3\times60 = 0.0315$$

$$[30\%]$$
(b) Excitation broad banded  $\Rightarrow (ropanse similar fo the response of an oscillator to white noise
from the data sheet  $\sigma_{x}^{-2} : \frac{1150}{Ck}, \quad \sigma_{x}^{-2} : \frac{1150}{Ch} \Rightarrow m.s.$  response  $\sigma(\frac{1}{C})$ 

$$Double damping \Rightarrow \sigma_{r} \to 1/\sqrt{2}$$$ 

 $J_{4}^{\dagger} = (\frac{1}{2\pi})(\frac{299}{1})e^{\frac{5}{2}(\sqrt{2}\times5)^{2}} = 6.63\times10^{-10}$   $P = 1 - e^{-\sqrt{3}T} = 1 - e^{-6.63\times10^{-10}\times3\times60} = 1.19\times10^{-7}$ [35%]
This is a reasonable probability of Failure

(c) From the data sheet 
$$D : V_0^* T \in [1/N(s_1)]$$
;  $N(s) : good s^{-1}$   
 $\int_{0}^{\infty} \frac{1}{N(s_1)} \frac{1}{good} \frac{0.3}{good} \times b$   
 $\int_{0}^{\infty} \frac{1}{N(s_1)} \frac{1}{p(b)} db$   
 $p(ak distribution) = \frac{b}{C_r} = \frac{b}{2} (b/\sigma_r)^2$   
From data sheet  
So  $D : V_0^* T \left(\frac{a.3}{yodd} \frac{0}{\sigma_r^2}\right) \int_{0}^{\infty} b^2 e^{\frac{b}{2} (b/\sigma_r)^2} db$   
 $\frac{1}{2 \times \sqrt{2\pi} \times \sigma_r^3}$   
So  $D : \left(\frac{1}{2\pi}\right) \left(\frac{\sigma_r}{\sigma_r}\right) T \left(\frac{a.3}{yodd}\right) \int_{2}^{\pi} \sigma_r$   
 $= \left(\frac{1}{2\pi}\right) \left(\frac{122}{0.6}\right) 3 \times 60 \left(\frac{0.3}{yodd}\right) \int_{2}^{\pi} \frac{\sigma_r}{2} \times 0.6 = \frac{\sigma_r}{2} \frac{\sigma_r}{2} \frac{\sigma_r}{2} \frac{\sigma_r}{2} \frac{\sigma_r}{2}$   
[35%]

This is too high because a factor of safety of between k and 5 must be applied.

3.(a)

$$= \frac{d}{dt} \begin{pmatrix} x \\ z \end{pmatrix}$$
,  $\begin{pmatrix} z \\ 3\xi z - x + 8\xi z z^{4} \end{pmatrix} = equilibrium point at (0,0)$ 

Consider stability by looking at Molian around (0,0)

$$\frac{1}{dt}\begin{pmatrix} x \\ i \end{pmatrix} : \begin{pmatrix} 0 & 1 \\ -1 & 3E \end{pmatrix} \begin{pmatrix} x \\ i \end{pmatrix}$$
Assume dependency  $e^{\lambda t} \Rightarrow \begin{pmatrix} -\lambda & 1 \\ -1 & 3E^{-\lambda} \end{pmatrix} = 0$ 

$$\Rightarrow -\lambda(3E^{-}\lambda) + 1 = 0 \Rightarrow \lambda^{2} - 3E\lambda + 1 = 0$$

$$\Rightarrow \lambda = \frac{1}{2} \left\{ 3E \pm \int 9E^{2} - \frac{1}{2} \right\} \Rightarrow (orijugate pair with form the positive positive real port positive  $= \frac{1}{2} \frac{$$$

 $3_{8} + \frac{1}{2} \cos 2t + \frac{1}{8} \cos 4t - \frac{1}{16} (1 + 2 \cos 2t + \frac{1}{2} + \frac{1}{2} \cos 4t)$ 

$$\vec{x}_{1} + x_{1} = -3A\varepsilon \sinh + 8\varepsilon A^{s} \left[ \frac{3}{4} \sinh + \frac{1}{2} (\cos 2t \sinh + \frac{1}{4} \cos 4t \sinh t) \right]$$

$$= \left( -3A\varepsilon + \frac{3}{5} \varepsilon A^{s} \right) \sinh + 8\varepsilon A^{s} \left[ \frac{4}{5} \sin 3t - \frac{1}{5} \sin 3t \right]$$

$$= \left( -3A\varepsilon + \varepsilon A^{s} \right) \sinh + 8\varepsilon A^{s} \left[ \frac{3}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

$$= \left( -3A\varepsilon + \varepsilon A^{s} \right) \sinh + 8\varepsilon A^{s} \left[ \frac{3}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

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$$= \left( -3A\varepsilon + \varepsilon A^{s} \right) \sinh + 8\varepsilon A^{s} \left[ \frac{4}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

$$= \left( -3A\varepsilon + \varepsilon A^{s} \right) \sinh + 8\varepsilon A^{s} \left[ \frac{4}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

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$$= \left( -3A\varepsilon + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

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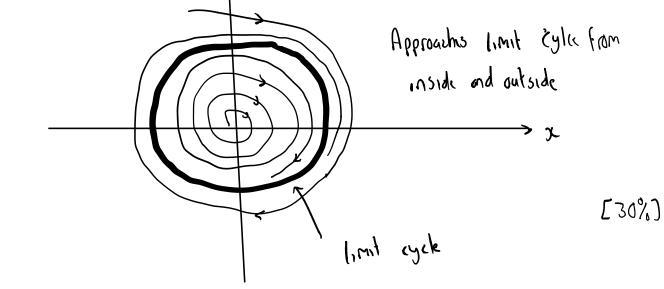
$$= \left( -3A\varepsilon + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$

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$$= \left( -3A\varepsilon + \frac{1}{16} \sin 3t \right]$$

$$= \left( -3A\varepsilon + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t + \frac{1}{16} \sin 3t \right]$$



(c)

4. a) 
$$\bar{x} + p^2 x + p x^3 = k \cos \omega t$$

For describing Function 
$$\int_{0}^{T} \mu x^{3} x x dt = \int_{0}^{T} 0 x x x dt$$
 with  $x \cdot A \cos t$   
 $\Rightarrow \mu A^{4} \int_{0}^{T} (\cos^{4} t) t dt : DA^{2} \int_{0}^{T} \cos^{2} t t dt$   
 $\mu A^{4} \int_{0}^{T} [\frac{1}{2}(1 + \cos t)]^{2} dt + \frac{1}{2} 20A^{2}T$   
 $\mu A^{4} \int_{0}^{T} [\frac{1}{2} + \frac{1}{2} \cos t t + \frac{1}{2} \cos^{2} t t] dt = \frac{1}{2} 20A^{2}T$   
 $\Rightarrow \tau \mu A^{4} [\frac{1}{2} + \frac{1}{2}] \cdot \frac{1}{2} OA^{2}T \Rightarrow D = \frac{3}{4} \mu A^{2}$ 

$$\Rightarrow (-\omega^2 + \beta^2 + 3(\gamma R^2) A \cdot k$$
 [30%]

b) 
$$\overline{a} + \frac{b^2 x + \mu \lambda^3}{s} + \frac{b^2 x +$$

= 
$$\frac{1}{10} + (\frac{1}{10} + 3\frac{1}{10} + 3\frac{1}{10}) = 0$$
 [20%]

c) 
$$\lambda_0 \cdot A \cos \omega t \Rightarrow \tilde{\omega} \cdot (\dot{p}^2 + 3NA^2 \cos^2 \omega t) \omega \cdot 0$$
  

$$\Rightarrow \tilde{\omega} \cdot (\dot{p}^2 + 3\chi_{P}A^2 + 3\chi_{P}A^2 \cos 2\omega t) \omega \cdot 0$$

$$\Rightarrow \frac{\tilde{\omega} + (\dot{p}^2 + \varepsilon \cos n t) \omega \cdot 0}{\tilde{\omega} + (\dot{p}^2 + \varepsilon \cos n t) \omega \cdot 0} \leftarrow Mathicu equalisn$$

$$\rho^2 : \dot{p}^2 + 3\chi_{P}A^2 \quad \varepsilon : 3\chi_{P}A^2 \quad \Lambda \cdot 2\omega$$

First order approximation  $\ddot{u} + P^2 u = 0$   $\Rightarrow u_0 = A \cos Pt$ Second order approximation  $\ddot{u}_1 + P^2 u_1 = -\epsilon A \cos \Omega t \cos Pt$   $= -\frac{\epsilon A}{2} \left[ \cos(\Omega + P)t + \cos(\Omega - P)t \right]$ Resonance when  $P = \Lambda + P \Rightarrow$  not a physical solution  $\sigma e = \Omega - P \Rightarrow \Lambda + 2P$ 

In the present case  $2W^2 2\sqrt{b^2 + 3/2}NA^2$  $\Rightarrow U^3 \sqrt{b^2 + 3/2}NA^2$ 

[50%]

### 4C7: Examiner's comments:

### Q1 Spectral analysis of vehicle dynamics

No major conceptual difficulties were evident, and the question was generally answered well.

# Q2 Circuit board impact and fatigue

Parts (a) and (b), concerning crossing-rates and the probability of impact, were well done. In Part (c), concerning fatigue damage, only one of the 17 students who attempted the question obtained the correct numerical answer. A common error was to use a Gaussian distribution for the stress peaks, instead of a Rayleigh distribution.

# Q3 Limit cycle oscillations

Part (a) was very well done, but the detailed algebra (trigonometry) in section (b) defeated many students. Most students made a reasonable attempt at the phase plane portrait in Part (c), even if Part (b) had not been completed.

# **Q4** Mathieu equation

This was the least popular question (8 attempts), although the average mark was reasonably good (60%). Part (b) was not well done, which was surprising given that the target formula was given on the exam paper and the question involved a straight forward substitution followed by the neglect of small terms.