

EGT1  
ENGINEERING TRIPOS PART IB

---

Thursday 10 June 2021 13:30 to 15:40

---

**Paper 6**

**INFORMATION ENGINEERING**

*This is an **open-book** exam.*

*Answer not more than **four** questions.*

*Answer not more than **two** questions from each section.*

*All questions carry the same number of marks.*

*The **approximate** number of marks allocated to each part of a question is indicated in the right margin.*

*Write your candidate number **not** your name on the top sheet.*

**STATIONERY REQUIREMENTS**

Write on single-sided paper.

**SPECIAL REQUIREMENTS TO BE SUPPLIED FOR THIS EXAM**

You have access to the Engineering Data Book, online or as your hard copy.

**10 minutes reading time is allowed for this paper at the start of the exam.**

**The time allowed for scanning/uploading answers is 20 minutes.**

**Your script is to be uploaded as a single consolidated pdf containing all answers.**

## SECTION A

Answer not more than **two** questions from this section.

- 1 (a) Consider the following open-loop transfer functions:

$$G_1(s) = \frac{\alpha(1 + 100s)}{(1 + 0.2s + s^2)} \quad G_2(s) = \frac{\beta(1 - s)}{(1 + 20s)} \quad G_3(s) = \frac{\gamma(1 + 100s)}{(1 + 2s + s^2)}$$

$$G_4(s) = \frac{\eta s}{(1 + s)(1 + 100s)} \quad G_5(s) = \frac{\kappa(1 + s)}{(1 + 20s)}$$

where  $\alpha \leq \beta \leq \gamma \leq \eta \leq \kappa$  are constants. Their Bode diagrams are shown in Fig. 1 below, with random labels (a-e) placed on each gain curve, and with random labels (f-k) placed on each phase curve.

- (i) Match each gain curve to its corresponding transfer function, reporting your answers in “letter =  $G_{\text{number}}$ ” format. Justify your answer. [4]
- (ii) Match each phase curve to its corresponding transfer function, reporting your answers in “letter =  $G_{\text{number}}$ ” format. Justify your answer. [4]

- (b) The rest of this question focuses on  $G_4(s)$  above, now with  $\eta = 10^4$ .

Let  $\bar{x}(s) = G_4(s)\bar{u}(s)$  in the Laplace domain. Express this relationship as a differential equation in the time domain. [4]

- (c) In order to track a desired output  $x_d(t)$ ,  $G_4$  is regulated by the negative feedback loop shown in Fig. 2, involving a proportional controller  $k_p$  and a sensor with transfer function  $\frac{1}{1+s}$ .

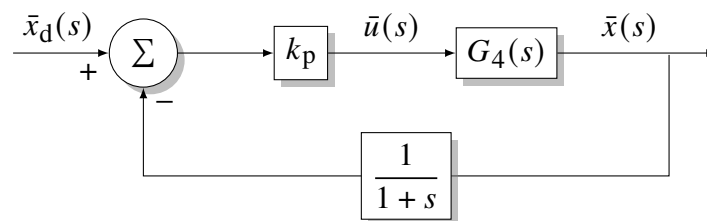


Fig. 2

- (i) Set  $k_p = 1$ . The phase part of the Bode diagram of the return ratio is given in Fig. 3 below. Draw the gain diagram (asymptotes only). [5]
- (ii) What is the phase margin? Justify your answer. [4]
- (iii) Find the value of  $k_p$  that achieves a phase margin of 45 degrees. [4]

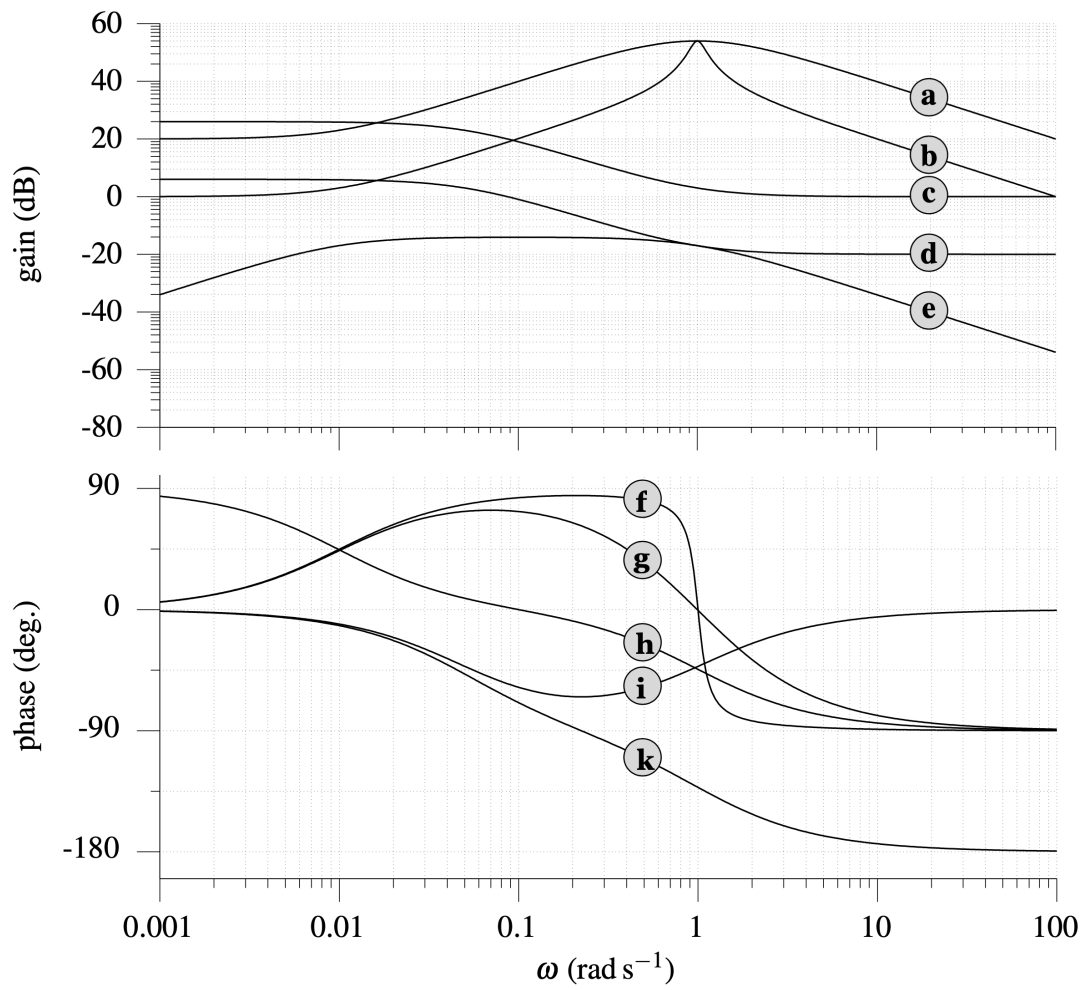


Fig. 1

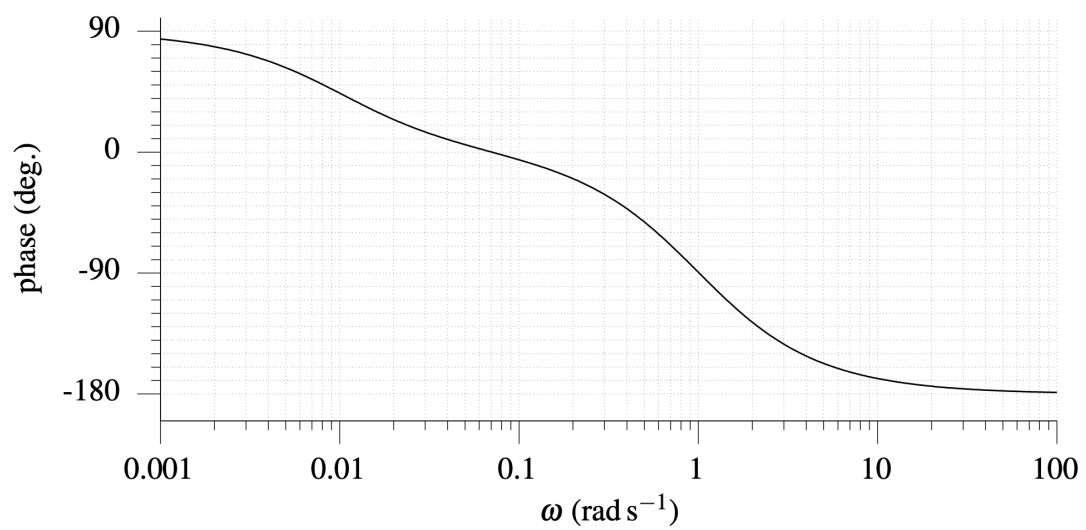


Fig. 3

2 A linear system with transfer function  $G(s)$  is controlled in a unity gain negative feedback loop with pre-compensator  $K(s)$ , as depicted in Fig. 4.

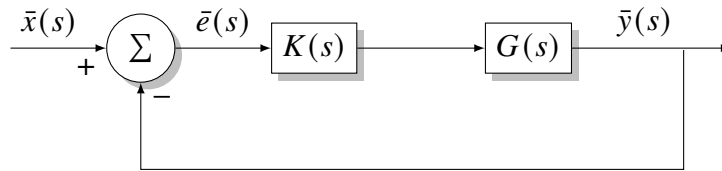


Fig. 4

The Nyquist diagram of the open loop with  $K(s) = 1$  is shown as a *solid line* in Fig. 5 below, for the whole range of positive frequencies.

- (a)  $G(s)$  has no zeros. How many poles does it have? [3]
- (b) What is the closed-loop transfer function from  $\bar{x}(s)$  to  $\bar{e}(s)$ ? [3]
- (c) Consider a simple compensator  $K(s) = k_p$ . Derive the value of  $k_p$  that achieves a 2% steady-state error in step response. Show your working out. [5]
- (d) The Nyquist diagram of  $30G(s)$  is shown in Fig. 5 as a *dashed* line. Use this to estimate the phase margin when  $k_p$  has the value found in (c). [5]
- (e) A proportional integral controller  $K(s) = (s + \alpha)/s$  is used instead, where  $\alpha$  is some constant. A part of the Nyquist diagram of  $K(s)G(s)$  is shown in Fig. 5 as a *dashed-dotted* line for positive frequencies. Here,  $K(s)$  is such that the diagram asymptotes onto the  $y$ -axis as  $\omega$  tends to zero.
- (i) What can you say about the steady-state error in step response, and why? [4]
- (ii) Knowing that  $G(j\omega) \approx 1 - 20j\omega$  for small positive  $\omega$ , derive the value of  $\alpha$ . [5]

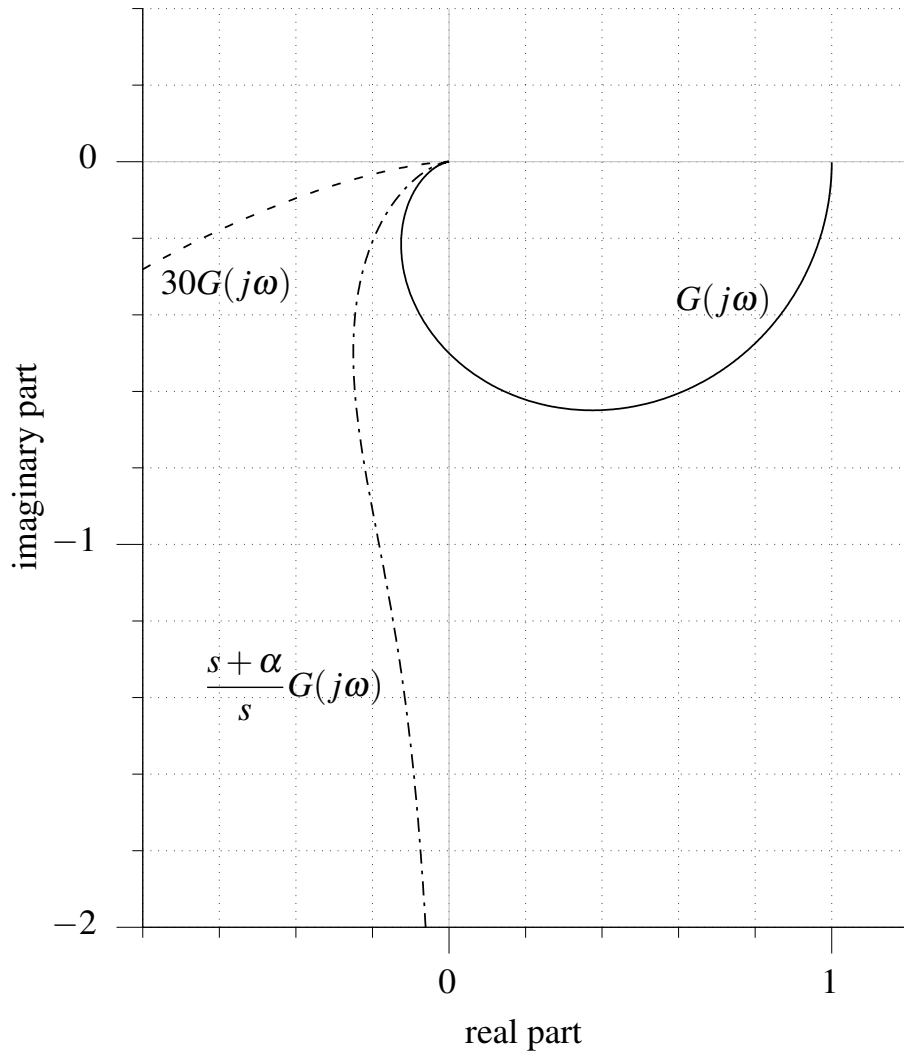


Fig. 5

3 Collaborative robots use elastic joints to improve safety. Consider the following model of a single-link manipulator

$$I\ddot{\theta} + c\dot{\theta} + k(\theta - u) = \tau \quad (1)$$

where  $\theta(t)$  is the angular position of the link,  $u(t)$  is the angular position of the driving motor (both measured in radians), and  $\tau$  is the external torque acting on the link (measured in N m). The motor is connected to the link through a torsional spring with constant  $k = 4$  N m rad<sup>-1</sup>. In the following,  $I = 1$  kg m<sup>2</sup> rad<sup>-1</sup> and  $c = 4$  kg m<sup>2</sup> s<sup>-1</sup> rad<sup>-1</sup> (damping).

For position control, the motor angle  $u$  is set by a proportional derivative controller

$$\bar{u}(s) = (k_p + k_d s) [\bar{\theta}_d(s) - \bar{\theta}(s)]$$

where  $\theta_d$  is the desired link position (reference).

(a) From Eq. 1, derive the open-loop transfer function  $G(s)$  from  $\bar{u}(s)$  to  $\bar{\theta}(s)$  and show that the robot is stable for any  $c > 0$  and  $k > 0$ . [3]

(b) Derive the expression in the time domain of the open-loop response of the robot for a step input  $u$  and for  $\tau = 0$ . [4]

(c) Sketch the open-loop response in (b) and show how this response would change for smaller/larger values of the spring constant  $k$ . Justify your answer. [4]

(d) Proceed now to tune the controller gains. Set  $k_p = 100$ .

(i) Draw the block diagram of the closed-loop system. [2]

(ii) Select the derivative gain  $k_d$  to avoid oscillations in closed loop, by enforcing a damping ratio of 1. Show your working out. [4]

(iii) Show that, in closed loop, the steady state deviation of the output  $\theta$  to a unit step torque  $\tau$  is less than 1%. [4]

(e) Suppose that  $\tau = -\gamma\dot{\theta} + \tau_{\text{ext}}$  for some  $\gamma > 0$  (additional dissipation). Discuss how this affects the transient behaviour of the closed-loop system and its steady state response to unit step torque  $\tau_{\text{ext}}$ . [4]

**SECTION B**

Answer not more than **two** questions from this section.

4 (a) Let  $f(t)$  have Fourier transform  $F(\omega) = 2a/(a^2 + \omega^2)$  with  $a > 0$ . Derive the Fourier transform of  $f(\alpha t)$ , that is, the time-scaled version of  $f(t)$  for  $\alpha \neq 0$ . [4]

(b) State the convolution theorem for the Fourier transform, and hence (or otherwise) derive the Fourier transform  $Z(\omega)$  of the triangular pulse  $z(t)$  in Fig. 6. For this, note that  $z(t) = \int_{-\infty}^{\infty} y(\tau)y(t - \tau) d\tau$ , where  $y(t)$  is the rectangular pulse also shown in Fig. 6. [4]

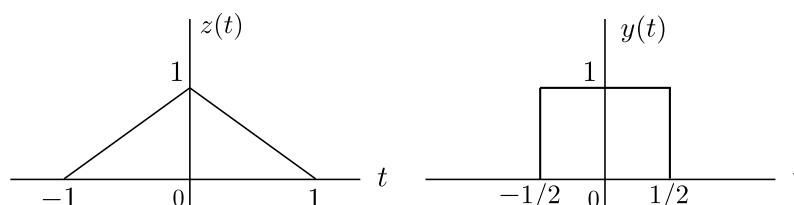


Fig. 6

(c) Consider the signal  $x(t)$  depicted below in Fig. 7. Using the results from parts (a) and (b), or otherwise, derive its Fourier transform  $X(\omega)$ . [4]

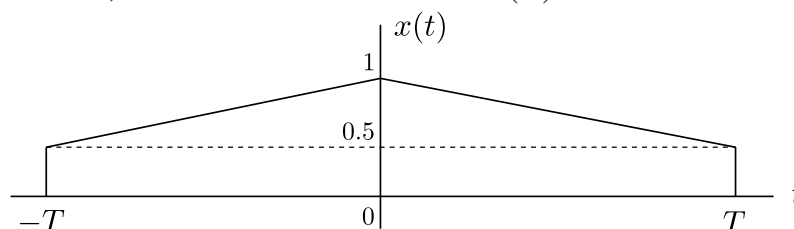


Fig. 7

(d) Given that the Fourier transform of  $p(t) = e^{-2|t|}$  is  $P(\omega) = 4/(4 + \omega^2)$ ,

(i) use the linearity and duality properties, or otherwise, to derive the Fourier transform of  $g(t) = 1/(4 + t^2)$ , [4]

(ii) use your solution to part (d)(i) and the frequency shift theorem, or otherwise, to derive the Fourier transform of  $m(t) = \sin(2t)/(4 + t^2)$ . [3]

(e) Using Parseval's Theorem and the hints below, or otherwise, derive the energy of the signal  $s(t) = \cos(t)\text{sinc}(t)$ . [6]

**Hints:** the Fourier transform of  $\text{sinc}(t)$  is a rectangular pulse of width 2 and height  $\pi$ , and the Fourier transform of  $\cos(t)$  is  $\pi[\delta(\omega + 1) + \delta(\omega - 1)]$ .

5 (a) Consider a train of  $\delta$ -functions located at intervals of duration  $T$ , with the following Fourier series representation:

$$\delta_p(t) = \frac{1}{T} \sum_{n=-\infty}^{\infty} e^{jn2\pi t/T}.$$

This train is used to sample a signal  $x(t)$  with Fourier transform  $X(\omega) = e^{-2|\omega|}$ .

(i) Recall that the Fourier transform of  $e^{j\omega_0 t} x(t)$  is  $X(\omega - \omega_0)$ . Derive the Fourier transform of the sampled signal. Explain if the original signal can be reconstructed from the sampled one. [3]

(ii) Using Parseval's theorem, find the cutoff frequency of an ideal unit gain lowpass filter that keeps 80% of the energy of the original signal. [4]

(iii) Apply the low pass filter from (a)(ii) to  $x(t)$  and sample the filtered signal using the train of  $\delta$ -functions,  $\delta_p(t)$ . Find the value of  $T$  that guarantees perfect reconstruction of the original signal from the sampled filtered signal. [3]

(b) The Discrete Fourier Transform (DFT) of a sampled signal  $x_n$  with  $N$  samples is

$$X_m = \sum_{n=0}^{N-1} x_n e^{-jnm2\pi/N}, \quad m = 0, \dots, N-1.$$

(i) Let  $N = 4$  and let the sampling interval be  $T = 50$  seconds. Indicate which frequency component of  $\{x_0, x_1, x_2, x_3\}$ , in radians per second, is measured by  $X_m$ . [3]

(ii) Let  $X = \{0, 2j, 0, -2j\}$  be the 4 DFT values obtained. Reconstruct  $\{x_0, x_1, x_2, x_3\}$ . [5]

(c) The periodic signal  $x(t)$  in Fig. 8 is sampled at intervals  $n \times 0.25$  for  $n = \dots, -2, -1, 0, 1, 2, \dots$  and quantised using six equally spaced levels given by  $\{(2m-1)/6\}$  for integers  $m$  between  $-2$  and  $3$ . Calculate the SNR of the quantised signal in dB. [7]

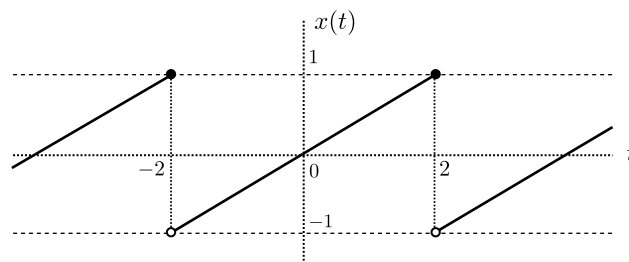


Fig. 8



6 (a) A speech signal  $f(t)$  with values in the range  $\pm 1$  is to be transmitted via modulation on a radio channel centered at 900 kHz. The modulation index is 0.5. The expression for the modulated signal is

$$s(t) = (15 + af(t)) \cos(\omega_c t),$$

with  $\omega_c$  measured in radians per second.

(i) What are the values of the constants  $a$  and  $\omega_c$ ? [4]

(ii) Derive the spectrum  $S(\omega)$  of the modulated signal in terms of the Fourier transform  $F(\omega)$  of the signal  $f(t)$ . [4]

(iii) What bandwidth should be allocated to this channel if  $f(t)$  is a baseband signal with one-sided bandwidth 5 kHz and a gap of 3 kHz must be maintained with the channels on either side of the passband spectrum? [2]

(iv) An alternative modulated signal is given by  $u(t) = af(t) \cos(\omega_c t)$ . Discuss the advantages/disadvantages of  $s(t)$  and  $u(t)$  for transmitting  $f(t)$ . [4]

(b) A sequence of bits is to be transmitted over a channel using Pulse Amplitude Modulation with a binary constellation given by  $\{-A, A\}$ . If the baseband waveform is formed by a pulse  $p(t)$  of duration  $T = 10^{-3}$  seconds, what is the transmission rate in bits per second? [2]

(c) For the sequence in Part (b), let  $X_k$  denote the  $k$ -th constellation symbol being transmitted. The modulated signal is transmitted over an additive Gaussian noise channel and the discrete-time received sequence is  $Y_k = X_k + N_k$ , where  $k = 0, 1, 2, \dots$  and  $N_k$  is Gaussian noise of mean zero and variance  $\sigma^2$ .

(i) The *a priori* symbol probabilities are  $p(X_k = A) = \frac{2}{3}$  and  $p(X_k = -A) = \frac{1}{3}$ . The optimal choice for  $X_k$  given  $Y_k$  is obtained by maximising the posterior probability  $p(X_k|Y_k) = p(Y_k|X_k)p(X_k) \times \text{constant}$ . Find the threshold  $\theta$  such that the receiver chooses  $X_k = A$  if  $Y_k > \theta$  and  $X_k = -A$  otherwise. [5]

(ii) Write down the probability of detection error in terms of the threshold  $\theta$ , the constellation symbol  $A$  and the  $Q(x)$  function, where the latter gives the probability that a standard Gaussian random variable takes values greater than  $x$ . Note that an error will occur when  $X_k = A$  and  $Y_k < \theta$  or when  $X_k = -A$  and  $Y_k > \theta$ . [4]

**END OF PAPER**

**THIS PAGE IS BLANK**