Thursday 8 June 2000

2 to 4

Paper 6

INFORMATION ENGINEERING

Answer not more than four questions.

Answer at least one question from each section.

All questions carry the same number of marks.

The approximate number of marks allocated to each part of a question is indicated in the right margin.

Answers to questions in each section should be tied together and handed in separately.

SECTION A

Answer at least one question from this section.

- 1 (a) The function p(t) is a pulse of unit magnitude, commencing at t=0 and of duration τ seconds. By considering p(t) as a combination of two step inputs, find its Laplace transform $\bar{p}(s)$.
- (b) Figure 1 shows a simple mixer vessel in which the contents are perfectly mixed at all times. Solvent flows in at a constant rate Q m³ sec⁻¹. The solution leaves the vessel at the same rate so that the volume V m³ of liquid in the vessel remains constant. A soluble solid is added at a varying rate m(t) kg sec⁻¹ and dissolves rapidly without any significant increase in the solution volume.

If c(t) kg m⁻³ is the concentration of the dissolved solids in the vessel at time t, show that the differential equation relating c(t) to m(t) is

$$\frac{dc}{dt} + \frac{Qc}{V} = \frac{m}{V} \quad . \tag{4}$$

[4]

- (c) If $m(t) = m_0 \ p(t)$ from part (a) with $\tau = 10$ seconds and $m_0 = 0.01 \text{ kg sec}^{-1}$, and if c(0) = 0, $V = 2 \text{ m}^3$ and $Q = 0.02 \text{ m}^3 \text{ sec}^{-1}$, obtain an expression for the concentration c(t).
- (d) Sketch c(t) and calculate the concentration after 5 seconds, and also after 100 seconds. [4]

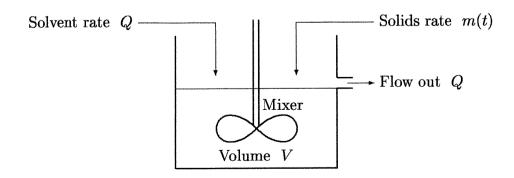


Fig. 1

- Figure 2 represents a mechanical system to control the position c(t) of an object, in response to a reference input r(t). There is a disturbance d(t) in the measurement in the velocity feedback loop. The Laplace transforms of these variables are $\bar{c}(s)$, $\bar{r}(s)$ and $\bar{d}(s)$ respectively.
- (a) Suggest reasons why each of the two feedback loops would have been included in this design. [3]
- (b) Establish the two transfer functions relating $\bar{c}(s)$ to $\bar{r}(s)$, and $\bar{c}(s)$ to $\bar{d}(s)$ in terms of K_c , $G_1(s)$, $G_2(s)$ and K_v . [6]
- (c) The error of this system is defined as $\epsilon(t) = r(t) c(t)$. Using the values given in Fig. 2, find the steady state error for the following three cases:
 - (i) a unit step input r(t) = u(t);
 - (ii) a ramp input r(t) = t u(t);
 - (iii) a step disturbance $d(t) = 0.1 \ u(t)$. [8]
- (d) Suggest how the controller transfer function K_c could be modified to remove the steady state error due to a step disturbance d(t). [3]

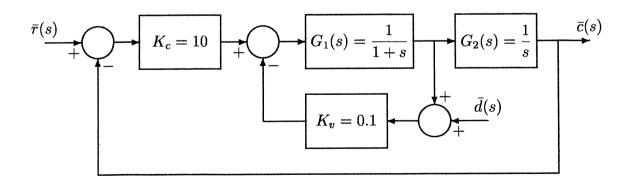


Fig. 2

3 A system has the transfer function

$$G(s) = \frac{2}{s(s+1)(s+2)}$$

and controller K(s), connected as shown in Fig. 3.

- (a) Using the semi-log paper provided, sketch clearly the Bode plots for G(s). (A few spot calculations will probably be required to obtain reasonable accuracy for the next part of this question.)
- (b) From your plots, estimate the gain and phase margins, if proportional control is used with K(s)=1.

[6]

(c) A phase compensator is used to replace the original controller, such that

$$K(s) = \frac{8(s+0.5)}{s+4} .$$

Modify your Bode plots to take account of this controller and determine the new gain and phase margins, showing your constructions clearly. [8]

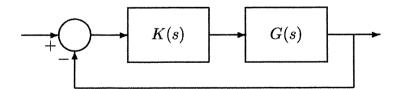


Fig. 3

- In the simple control system shown in Fig. 4, the plant has a transfer function G(s) and the controller transfer function is a pure positive gain K. The Laplace transforms of the reference input and the output are $\bar{r}(s)$ and $\bar{y}(s)$ respectively.
- (a) Show that the closed-loop transfer function relating $\bar{y}(s)$ to $\bar{r}(s)$ is given by

$$H(s) = \frac{G(s)}{\frac{1}{K} + G(s)} .$$

[3]

(b) If the plant transfer function is

$$G(s) = \frac{1}{s(s^2 + 3s + 4)} ,$$

sketch the Nyquist plot for the plant over positive values of angular frequency ω , and show clearly how the magnitude of the closed-loop frequency response, relating the output to the reference input, may be measured graphically from the plot.

[7]

- (c) If the phase margin of the system is 45° , calculate K, and estimate the peak magnitude of the closed-loop frequency response.
- [7]
- (d) Briefly suggest why, for typical control systems, it is usually considered undesirable for the peak magnitude of the closed-loop frequency response to be significantly greater than unity.

[3]

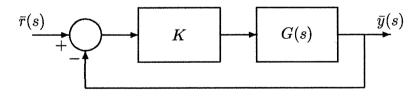


Fig. 4

SECTION B

Answer at least one question from this section.

5 (a) A telephone channel has a transfer function

$$H(s) = G_0 \left(\frac{sT_1}{1 + sT_1} \right) \left(\frac{1}{1 + sT_2} \right)$$

where G_0 is the approximate mid-band gain. If the channel pass band (between its -3dB frequencies) extends from 300 Hz to 3400 Hz, calculate the time constants T_1 and T_2 . What physical elements of the channel typically define the values of T_1 and T_2 ?

- [7]
- (b) Calculate the step response of this channel, and hence sketch its response to a rectangular pulse input of amplitude 1 volt and duration 5 ms.
- [7]
- (c) Why does this result show that 200 bit/s binary data signals should *not* be transmitted directly over this channel? Discuss what further processing would allow satisfactory transmission of such signals. [6]

6 (a) When a signal is digitised, the quantisation process introduces distortion. Explain why this distortion may usually be modelled as additive random noise; and sketch the probability density function of the noise, assuming an ideal uniform quantiser with small step size δV .

[4]

(b) Show that the rms noise voltage introduced by such a quantiser is proportional to δV , and derive the constant of proportionality.

[6]

(c) A periodic symmetrical triangular wave of zero mean and peak amplitude 5 volts is defined by v(t) = 5 - (20|t|/T) for $-T/2 \le t \le T/2$, where T is the period of the wave. This wave is quantised by a 15-bit analogue-to-digital conversion system at a sampling rate of 100 kHz. The fundamental frequency of the triangular wave is approximately 1 kHz. Calculate the maximum signal-to-noise power ratio (in dB) that could be achieved with this system, assuming ideal anti-aliasing lowpass filters at input and output.

[6]

(d) If the bandwidth of the output filter could be varied, comment on how this would affect the output signal wave-shape and the output noise level. Hence comment on the trade-offs which might then be made.

[4]

Note:

For a zero-mean triangular wave, rms amplitude = (peak amplitude) $/\sqrt{3}$.

END OF PAPER