

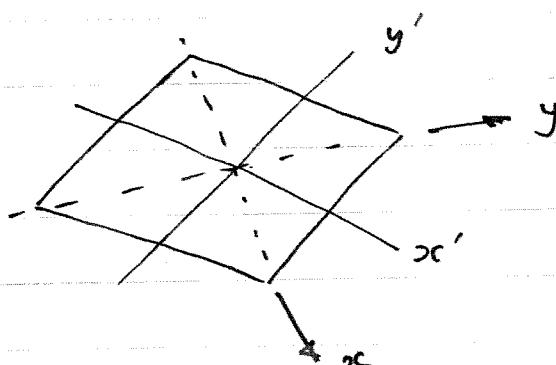
PAPER 3C5 DYNAMICS 2003 SOLUTIONS

(a) For the plate

$$I_{x'x'} = I_{y'y'} = \frac{1}{3}ma^2$$

from Data book

$$I_{zz} = \frac{2}{3}ma^2 \text{ using } \underline{\text{t axes theorem.}}$$



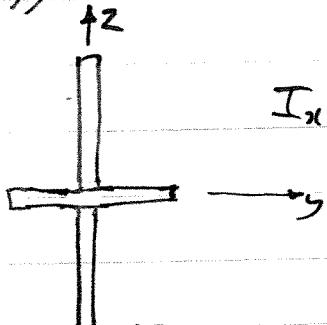
The plate is like a disc since

it has two equal moments of inertia. All inplane axes are the same.

$$\text{So } I_{x'x'} = I_{y'y'} = \frac{1}{3}ma^2$$

[25%]

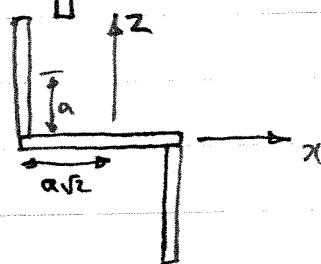
(b) View along x



$$I_{xx} = \frac{1}{3}ma^2 + \frac{1}{3}m(2a)^2$$

$$I_{yz} = 0$$

View along y



$$I_{yy} = \frac{1}{3}ma^2 + 2\left[\frac{1}{3}\frac{ma^2}{2} + \frac{ma^2}{2}(2+1)\right]$$

$$= \frac{1}{3}ma^2 + \frac{10}{3}ma^2$$

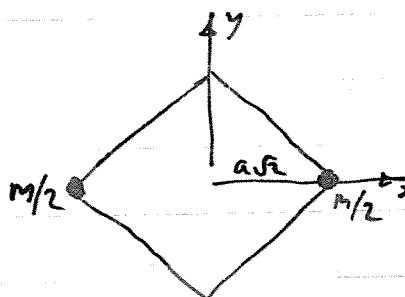
$$= \frac{11}{3}ma^2$$

$$I_{xz} = \int xz dm = -2a\sqrt{2} \int z dz \frac{ma}{2a}$$

$$= -\frac{m\sqrt{2}}{2} \left(\frac{1}{2}z^2\right)_0^a$$

$$= -m\sqrt{2}a^2$$

View along z



$$I_{zz} = \frac{2}{3}ma^2 + m(a\sqrt{2})^2$$

$$= \frac{8}{3}ma^2$$

$$I_{xy} = 0$$

$$\therefore I_G = \frac{ma^2}{3} \begin{bmatrix} 5 & 0 & +3\sqrt{2} \\ 0 & 11 & 0 \\ +3\sqrt{2} & 0 & 8 \end{bmatrix}$$

[60%]

1(c) For principal moments of inertia:

$$\begin{vmatrix} 5-\lambda & 0 & +3\sqrt{2} \\ 0 & 11-\lambda & 0 \\ +3\sqrt{2} & 0 & 8-\lambda \end{vmatrix} = 0$$

$$\therefore (11-\lambda)(5-\lambda)(8-\lambda) - (3\sqrt{2})^2 = 0$$

$$\therefore (11-\lambda)(\lambda^2 - 13\lambda + 40 - 18) = 0$$

$$\therefore (11-\lambda)(\lambda^2 - 13\lambda + 22) = 0$$

$$\therefore (1-\lambda)(11-\lambda)(2-\lambda) = 0$$

∴ Principal moments of inertia are :

$$\frac{11ma^2}{3}, \frac{11ma^2}{3}, \frac{2ma^2}{3}$$

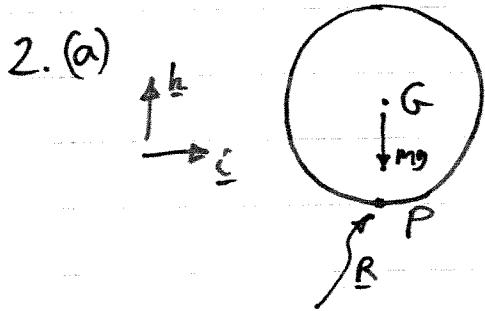
Diagonal AC is the Y axis and it was principal before transformation so it must still be principal. $I_{yy} = \frac{11ma^2}{3}$

[30%]

(d) The assembly is an "AAC" body just like a cylinder.

Any forces applied to the assembly and to a cylinder of the same mass and with the same AAC values will cause identical responses.

[5%]



Consider the point P directly below G at all times. $\underline{U}_P = \underline{U}_G$

The weight force mg and any contact reaction at P have no moment about P so consider using the formulae

$$\underline{Q}_P = \underline{h}_P + \dot{\underline{r}}_P \times \underline{k}$$

with $\underline{Q}_P = 0$ and since $\underline{k} = m \underline{U}_G$
we have $\dot{\underline{r}}_P \times \underline{k} = 0$

So $\boxed{\underline{h}_P = 0}$

$$\underline{h}_P = Aw_1\mathbf{i} + Aw_2\mathbf{j} + Cw_3\mathbf{k} \quad \text{with} \quad A = \frac{2}{5}ma^2 \\ C = \frac{3}{5}ma^2$$

$$\underline{h}_P = \text{const} \quad \text{so} \quad w_1 = \text{const}$$

$$w_2 = \text{const}$$

$$w_3 = \text{const}$$

$$\text{No slip at P} \quad \underline{U}_G + \underline{\omega} \times (-a\mathbf{k}) = 0$$

$$\therefore \underline{U}_G + aw_1\mathbf{i} - aw_2\mathbf{j} = 0$$

$$\text{Let } \underline{U}_G = U_1\mathbf{i} + U_2\mathbf{j} + U_3\mathbf{k}$$

$$\text{so } U_1 = aw_2 = \text{constant}$$

$$U_2 = -aw_1 = \text{zero (also constant)}$$

$$U_3 = 0$$

Note there is no constraint on w_3 so Ant spin is allowable.

[20%]

2(b) Just as for (a) but now $\mathbf{Q}_p = -\mathbf{F}a_i$

So $-\mathbf{F}a_i = A\omega_1 \mathbf{i} + A\omega_2 \mathbf{j} + A\omega_3 \mathbf{k}$

So $A\omega_1 = -Fa$ ①

$\omega_2 = \text{const}$ $\therefore \dot{\mathbf{U}}_r = a\omega_2 = \text{constant}$

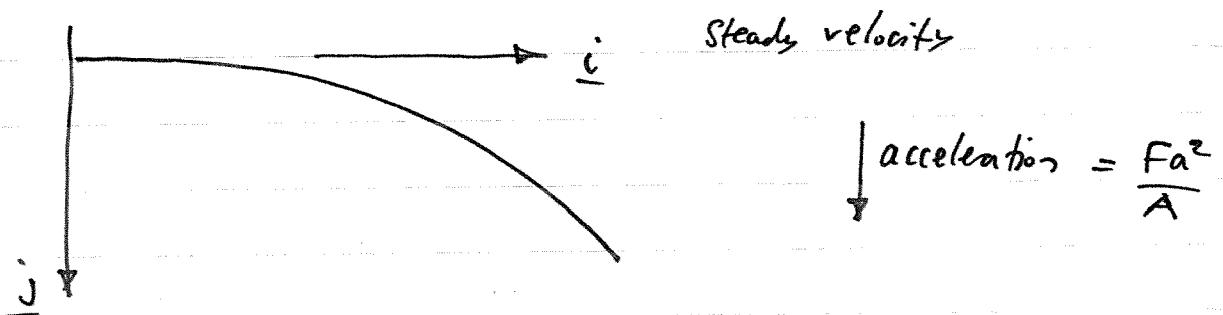
$\omega_3 = \text{const}$

① $\Rightarrow \dot{\omega}_1 = -\frac{Fa}{A}$ but $\dot{\mathbf{U}}_r = -a\omega_1$,

$$\therefore \dot{\mathbf{U}}_r = -a\dot{\omega}_1 = \frac{Fa^2}{A}$$

$\dot{\mathbf{U}}_r$ is the acceleration in the \mathbf{j} direction
constant

and since $\dot{\mathbf{U}}_r$ is constant this is just like projectile motion

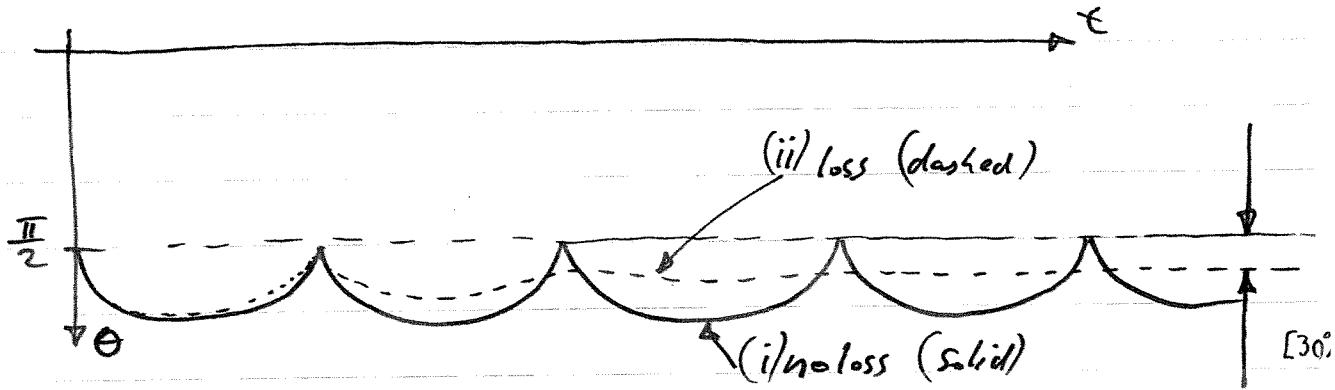


[60%]

(c) Again note that ω_3 is unconstrained, so spin does not affect the motion

[20%]

3(a)



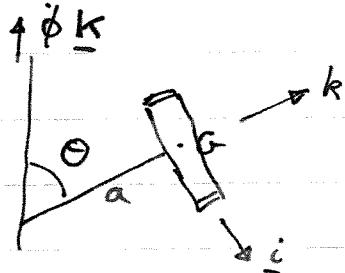
this is the permanent steady state value of the θ offset.

$$(b) \text{ To begin with, } KE = \frac{1}{2} C \omega^2 .$$

$$\text{and } h \cdot k = 0$$

if there is no moment of momentum about a vertical axis.

Subsequent motion: PE + KE & $h \cdot k$ are conserved.



$$\text{Velocity of G: } \dot{G} = a\dot{\theta}i + a\sin\theta\dot{\phi}i$$

$$\text{Angular velocity of rotor: } \omega = \omega_i i + \omega_2 j + \omega_3 k$$

$$\omega_1 = -\dot{\phi}\sin\theta$$

$$\omega_2 = \dot{\theta}$$

$$\omega_3 = \dot{\phi}\cos\theta + \omega = \omega \text{ for fast spin}$$

$$\therefore KE = \frac{1}{2} ma^2 (\dot{\theta}^2 + \sin^2\theta \dot{\phi}^2) + \frac{1}{2} A(\dot{\phi}^2 \sin^2\theta) + \frac{1}{2} A\dot{\theta}^2 + \frac{1}{2} C \omega^2$$

At extreme position $\dot{\theta} = 0$

$$\therefore KE = \frac{1}{2}(ma^2 + A) \sin^2\theta \dot{\phi}^2 + \frac{1}{2} C \omega^2$$

$$\text{Put } \theta = \frac{\pi}{2} + \alpha \quad \therefore \begin{cases} \sin\theta = \cos\alpha \approx 1 \\ \cos\theta = -\sin\alpha = -\alpha \end{cases} \quad \left. \begin{array}{l} \text{small} \\ \alpha \end{array} \right\}$$

$$\text{Energy Conservation: } KE + PE = \frac{1}{2}(ma^2 + A) \dot{\phi}^2 + \frac{1}{2} C \omega^2 - m g a \alpha = \frac{1}{2} C \omega^2$$

$$\therefore \boxed{(ma^2 + A) \dot{\phi}^2 = 2mga\alpha} \quad (1)$$

$$\text{Moment of Momentum: } h = (A + ma^2)\omega_i i + (A + ma^2)\omega_2 j + C\omega_k k$$

$$h \cdot k = (A + ma^2)(-\dot{\phi}\sin\theta)(-\sin\theta) + C\omega\cos\theta = 0$$

$$\therefore (A + ma^2)\dot{\phi}\cos^2\alpha - C\omega\sin\alpha = 0$$

3(b) cont

$$\therefore \boxed{(A+ma^2)\dot{\phi} = C\omega \alpha} \quad (2)$$

eliminate $\dot{\phi}$ from (1) & (2)

$$\frac{(2)^2}{(1)} \therefore (A+ma^2) = \frac{C^2 \omega^2 \alpha}{2mga}$$

$$\therefore \boxed{\alpha = \frac{2mga(A+ma^2)}{C^2 \omega^2}} \quad [40\%]$$

(c) For steady motion (precession) small α

$$Q_2 = C\omega \dot{\phi}$$

$$\therefore mga = C\omega \dot{\phi} \quad (3)$$

But (2) (conservation of moment of momentum about K)
must always be satisfied

$$\therefore \frac{(2)}{(3)} \text{ gives } \frac{A+ma^2}{C\omega} = \frac{C\omega \alpha_s}{mga}$$

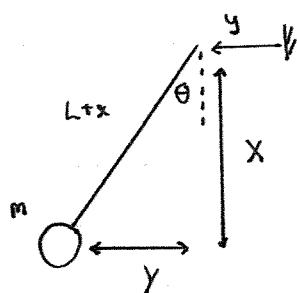
$$\therefore \alpha_s = \frac{mga(A+ma^2)}{C^2 \omega^2}$$

Note that $\alpha_s = 2\alpha$

i.e. steady α is half the peak α reached.

[30]

4. a)



$$\text{Mass position } X = (L+x) \cos\theta$$

$$Y = y + (L+x) \sin\theta$$

$$\text{kinetic energy } T = \frac{1}{2}m(\dot{x}^2 + \dot{y}^2)$$

$$T = \frac{1}{2}m \left\{ [\ddot{x} \cos\theta - (L+x)\dot{\theta} \sin\theta]^2 + [\ddot{y} + \ddot{x} \sin\theta + (L+x)\dot{\theta} \cos\theta]^2 \right\}$$

$$T = \frac{1}{2}m \left\{ \ddot{x}^2 + \dot{y}^2 + (L+x)^2 \dot{\theta}^2 + 2\ddot{x}\dot{y}(L+x) \cos\theta + 2\ddot{y}\dot{x} \sin\theta \right\}$$

$$V_g = -MgX = -Mg(L+x) \cos\theta \quad \text{gravity}$$

$$V_s = \frac{1}{2}kx^2 \quad \text{spring}$$

$$V = -Mg(L+x) \cos\theta + \frac{1}{2}kx^2$$

[10]

b) For x : $\frac{d}{dt} \left[\frac{\partial T}{\partial \dot{x}} \right] - \frac{\partial T}{\partial x} + \frac{\partial V}{\partial x} = 0$

$$\frac{d}{dt} [m\ddot{x}] - m(L+x)\dot{\theta}^2 - M\ddot{y}\dot{\theta} \cos\theta + \frac{d}{dt} [M\ddot{y}\sin\theta] - Mg\cos\theta + kx = 0$$

$$M\ddot{x} - m(L+x)\dot{\theta}^2 + M\ddot{y}\sin\theta - Mg\cos\theta + kx = 0 \quad (1)$$

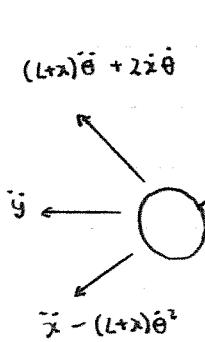
For θ : $\frac{d}{dt} \left[\frac{\partial T}{\partial \dot{\theta}} \right] - \frac{\partial T}{\partial \theta} + \frac{\partial V}{\partial \theta} = 0$

$$\frac{d}{dt} [M(L+x)^2 \dot{\theta}] + M\ddot{y}\dot{\theta} (L+x) \sin\theta - M\ddot{x}\dot{y} \cos\theta + Mg(L+x) \sin\theta = 0$$

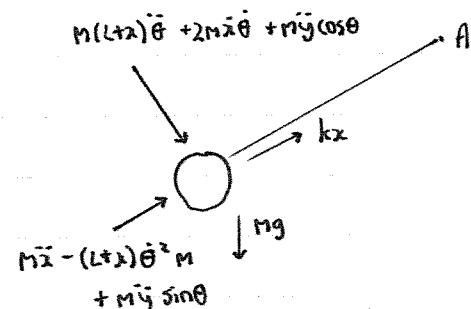
$$M(L+x)^2 \ddot{\theta} + 2M\ddot{x}\dot{\theta}(L+x) + M\ddot{y}(L+x) \cos\theta + Mg(L+x) \sin\theta = 0 \quad (2)$$

[65]

c)



Accelerations



Forces

Resolve along string \Rightarrow eqn (1) ✓

Moments about A \Rightarrow eqn (2) ✓

[25]

d) for $\omega \neq 0$ and θ small, equation (2) becomes:-

$$ML^2\ddot{\theta} + MgL\theta = -ML\ddot{y} \Rightarrow \ddot{\theta} + \omega_n^2\theta = -\left(\frac{1}{L}\right)\ddot{y} = \left(\frac{A}{L}\right)\sin\omega t ; \omega_n^2 = g/L$$

The solution is $\theta = \frac{A \sin\omega t}{L(\omega_n^2 - \omega^2)} + \alpha \cos\omega nt + \beta \sin\omega nt$

P.I. C.F.

Validity : θ must remain small \Rightarrow small, non-resonant motion $y(t)$

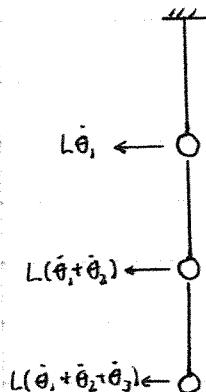
[20]

5 : a) If the generalised coordinates are $q_1, q_2 \dots q_N$, then:-

$$M_{ij} = \frac{\partial^2 T}{\partial q_i \partial q_j}; \quad k_{ij} = \frac{\partial^2 U}{\partial q_i \partial q_j}$$

[5]

b) Assuming that the angles are small, the velocities are:-



$$\text{Thus } T = \frac{1}{2} M L^2 \left\{ \dot{\theta}_1^2 + (\dot{\theta}_1 + \dot{\theta}_2)^2 + (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \right\}$$

$$M_{ij} = \frac{\partial^2 T}{\partial \theta_i \partial \theta_j} \Rightarrow M = \frac{1}{2} M L^2 \begin{pmatrix} 2+2+2 & 2+2 & 2 \\ \text{Symm} & 2+2 & 2 \\ & & 2 \end{pmatrix}$$

$$U = -mgL \cos \theta_1 - mgL (\cos \theta_1 + \cos \theta_2) - mgL (\cos \theta_1 + \cos \theta_2 + \cos \theta_3)$$

$$k_{ij} = \frac{\partial^2 U}{\partial \theta_i \partial \theta_j} = mgL \begin{pmatrix} 3 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Thus the equations of motion can be written in the form (with $\omega_0^2 = g/L$):-

$$\begin{pmatrix} 3 & 2 & 1 \\ 2 & 2 & 1 \\ 1 & 1 & 1 \end{pmatrix} \begin{pmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \\ \ddot{\theta}_3 \end{pmatrix} + \begin{pmatrix} 3 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 1 \end{pmatrix} \omega_0^2 \begin{pmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \frac{FL}{ML^2}$$

[5]

note generalised Force vector

$$\delta W = L(\delta \theta_1 + \delta \theta_2 + \delta \theta_3) F$$

c) For $\ddot{\theta}_1 = 0$:

$$\begin{pmatrix} 2 & 1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} \ddot{\theta}_2 \\ \ddot{\theta}_3 \end{pmatrix} + \omega_0^2 \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \theta_1 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 1 \\ 1 \end{pmatrix} \frac{FL}{ML^2}$$

Consider Free harmonic vibration : must have $(-\omega^2 m + k) \theta = 0$, so that:-

$$\begin{pmatrix} 2(\omega_0^2 - \omega^2) & -\omega^2 \\ -\omega^2 & \omega_0^2 - \omega^2 \end{pmatrix} \begin{pmatrix} \theta_2 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$$\begin{aligned} \text{Determinant} = 0 &\Rightarrow 2(\omega_0^2 - \omega^2)^2 - \omega^4 = 0 \\ &\Rightarrow 2\omega_0^2 - 4\omega_0^2\omega^2 + \omega^4 = 0 \Rightarrow \omega^2 = \frac{4\omega_0^2 \pm \sqrt{16\omega_0^4 - 8\omega_0^4}}{2} \\ &\Rightarrow \underline{\omega^2 = \omega_0^2(2 \pm \sqrt{2})} \end{aligned}$$

$$\text{For } \omega^2 = \omega_0^2(2 - \sqrt{2}) \quad \begin{pmatrix} 2(-1 + \sqrt{2})\omega_0^2 & -\omega_0^2(2 - \sqrt{2}) \\ \omega_0^2 & \omega_0^2(2 - \sqrt{2}) \end{pmatrix} \begin{pmatrix} \theta_2 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \quad \theta_3 = \frac{2(\sqrt{2} - 1)}{2 - \sqrt{2}} \theta_2 \quad \theta_2 = \underline{\sqrt{2}\theta_2}$$

$$\text{For } \omega^2 = \omega_0^2(2 + \sqrt{2}) \quad \begin{pmatrix} 2(-1 - \sqrt{2})\omega_0^2 & -\omega_0^2(2 + \sqrt{2}) \\ \omega_0^2 & \omega_0^2(2 + \sqrt{2}) \end{pmatrix} \begin{pmatrix} \theta_2 \\ \theta_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \quad \theta_3 = \frac{-2(1 + \sqrt{2})}{2 + \sqrt{2}} \theta_2 \quad \theta_2 = \underline{-\sqrt{2}\theta_2}$$

[So]