

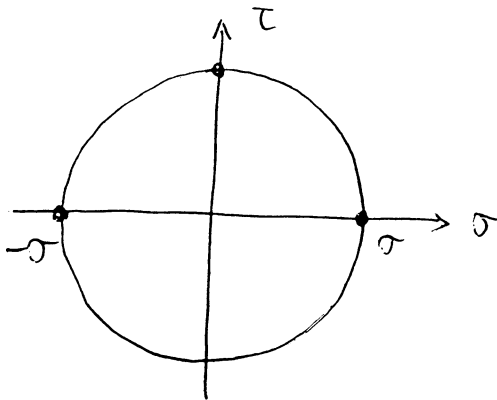
1. (a) $\sigma_{xx} = \sigma$, $\sigma_{yy} = -\sigma$, $\sigma_{zz} = 0$
 $\epsilon_{xx} = \frac{\Delta a}{a}$, $\epsilon_{yy} = -\frac{\Delta a}{a}$, $\epsilon_{zz} = 0$

Assume plane stress, then

$$\epsilon_{xx} = \frac{\sigma_{xx}}{E} - \nu \frac{\sigma_{yy}}{E} = \frac{(1+\nu)\sigma}{E}$$

$$\Rightarrow \frac{\Delta a}{a} = \frac{1+\nu}{E} \sigma \quad (20\%)$$

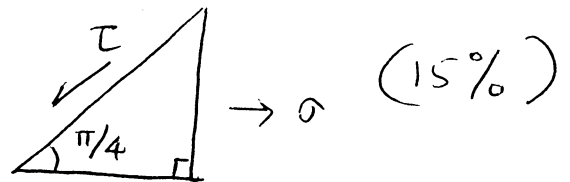
(b) Draw the Mohr's circle



The diagonal plane is $\frac{\pi}{4}$ angle from the x -axis. From the Mohr's circle, it then follows

$$\tau = \sigma$$

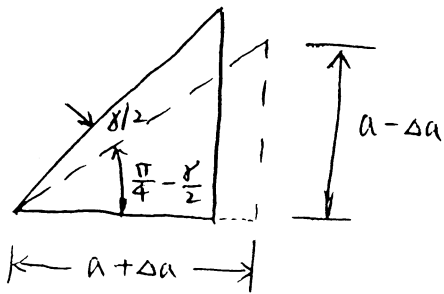
This can also be proved by considering equilibrium.



(c) Engineering shear strain is defined as the change in angle between two lines that were originally perpendicular to each other. For the current problem, the shear strain along the diagonal plane is γ , and

$$\tau = G\gamma \quad (15\%)$$

1. (d)



$$\tan\left(\frac{\pi}{4} - \frac{\gamma}{2}\right) = \frac{a - \Delta a}{a + \Delta a} = \frac{1 - \frac{\Delta a}{a}}{1 + \frac{\Delta a}{a}}$$

But

$$\begin{aligned} \tan\left(\frac{\pi}{4} - \frac{\gamma}{2}\right) &= \frac{\sin\left(\frac{\pi}{4} - \frac{\gamma}{2}\right)}{\cos\left(\frac{\pi}{4} - \frac{\gamma}{2}\right)} \\ &= \frac{\sin\frac{\pi}{4}\cos\frac{\gamma}{2} - \cos\frac{\pi}{4}\sin\frac{\gamma}{2}}{\cos\frac{\pi}{4}\cos\frac{\gamma}{2} + \sin\frac{\pi}{4}\sin\frac{\gamma}{2}} \quad (30\%) \\ &= \frac{1 - \frac{\gamma}{2}}{1 + \frac{\gamma}{2}} = \frac{1 - \frac{\Delta a}{a}}{1 + \frac{\Delta a}{a}} \end{aligned}$$

$$\left(\begin{array}{l} \sin\frac{\pi}{4} = \cos\frac{\pi}{4} = \frac{\sqrt{2}}{2} \\ \cos\frac{\gamma}{2} \approx 1; \sin\frac{\gamma}{2} \approx \frac{\gamma}{2} \end{array} \right)$$

$$\Rightarrow \frac{\gamma}{2} = \frac{\Delta a}{a} \Rightarrow \boxed{\gamma = 2 \frac{\Delta a}{a}}$$

(e)

$$G = \frac{\tau}{\gamma} = \frac{\sigma}{2 \Delta a/a} = \frac{\sigma}{2 \frac{(1+\nu)}{E} \sigma} \quad (10\%)$$

$$\Rightarrow \boxed{G = \frac{E}{2(1+\nu)}}$$

(f)

Bulk modulus

There are 2 independent material parameters.

(10%)

2. (a) Lamé solutions

$$\sigma_{rr} = A - \frac{B}{r^2}, \quad \sigma_{\theta\theta} = A + \frac{B}{r^2}$$

$$\epsilon_{\theta\theta} = \frac{u}{r} = \frac{\sigma_{\theta\theta}}{E} - \frac{\nu\sigma_{rr}}{E}$$

(assume plane stress first)
change to plane strain later

$$= \frac{1}{E} \left\{ A + \frac{B}{r^2} - \nu A + \frac{\nu B}{r^2} \right\}$$

$$\Rightarrow u = \frac{r}{E} \left\{ A(1-\nu) + \frac{B}{r^2}(1+\nu) \right\}$$

For plane strain, replace E by $\frac{E}{1-\nu^2}$ and ν by $\frac{\nu}{1-\nu}$ to get

$$u = \frac{r(1-\nu^2)}{E} \left\{ A \left(1 - \frac{\nu}{1-\nu}\right) + \frac{B}{r^2} \left(1 + \frac{\nu}{1-\nu}\right) \right\}$$

$$= \frac{r(1+\nu)}{E} \left\{ A(1-2\nu) + \frac{B}{r^2} \right\}$$

(40%)

(b) (i) At $r=a$, $\sigma_{rr} = -p_0 = A - \frac{B}{a^2} \Rightarrow A = \frac{B}{a^2} - p_0$

At $r=b$

$$\sigma_{rr} = -p_e = \frac{E}{b} (u)_{r=b}$$

$$= \frac{E}{b} \cdot \frac{b(1+\nu)}{E} \left\{ A(1-2\nu) + \frac{B}{b^2} \right\}$$

$$= A(1+\nu)(1-2\nu) + \frac{B}{b^2}(1+\nu)$$

$$\Rightarrow -\frac{p_e}{1+\nu} = \left(\frac{B}{a^2} - p_0 \right) (1-2\nu) + \frac{B}{b^2}$$

Rearrange gives

$$B = \frac{p_0(1-2\nu) - p_e/(1+\nu)}{\frac{1-2\nu}{a^2} + \frac{1}{b^2}}$$

$$A = \frac{p_0 \frac{a^2}{b^2} - \frac{p_e}{1+\nu}}{(1-2\nu) + \frac{a^2}{b^2}}$$

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2. (b) continued

Finally,

$$\begin{aligned} p_e &= -(\sigma_{rr})_{r=b} = \frac{B}{b^2} - A \\ &= \frac{p_o(1-2\nu) - \frac{p_e}{1+\nu}}{1 + (1-2\nu)\frac{b^2}{a^2}} - \frac{p_o\frac{a^2}{b^2} - \frac{p_e}{1+\nu}}{(1-2\nu) + \frac{a^2}{b^2}} \\ &= \frac{\frac{p_e}{1+\nu} \left(\frac{b^2}{a^2} - 1 \right) - 2\nu p_o}{1 + (1-2\nu)\frac{b^2}{a^2}} \end{aligned}$$

$$\Rightarrow 2\nu p_o = p_e \left\{ \frac{\frac{b^2}{a^2} - 1}{1+\nu} - 1 - (1-2\nu)\frac{b^2}{a^2} \right\}$$

$$\Rightarrow p_e = \frac{2\nu p_o (1+\nu)}{\frac{b^2}{a^2} [1 + (1-2\nu)(1+\nu)] + \nu} \quad (40\%)$$

(ii) The change in the thickness is

$$\begin{aligned} \Delta &= (u)_{r=b} - (u)_{r=a} \\ &= \frac{b}{E} \left[A(1-\nu) + \frac{B}{b^2} (1+\nu) \right] - \frac{a}{E} \left[A(1-\nu) + \frac{B}{a^2} (1+\nu) \right] \\ &= \frac{A(1-\nu)}{E} (b-a) + \frac{B(1+\nu)}{E} \left(\frac{1}{b} - \frac{1}{a} \right) \end{aligned}$$

Where A and B have been found earlier. To be precise, the thickness change should be $|\Delta|$.

(20%)

3

$$a) \quad \phi = \frac{Cr^2}{\tan \alpha - \alpha} \left[\alpha - \theta + \frac{\sin 2\theta}{2} - \tan \alpha \cos^2 \theta \right]$$

$$\frac{\partial \phi}{\partial r} = \frac{2Cr}{\tan \alpha - \alpha} \left[\alpha - \theta + \frac{\sin 2\theta}{2} - \tan \alpha \cos^2 \theta \right]$$

$$\frac{\partial^2 \phi}{\partial r^2} = \frac{2C}{\tan \alpha - \alpha} \left[\alpha - \theta + \frac{\sin 2\theta}{2} - \tan \alpha \cos^2 \theta \right]$$

$$\frac{\partial \phi}{\partial \theta} = \frac{Cr^2}{\tan \alpha - \alpha} \left[-1 + \cos 2\theta + 2 \tan \alpha \sin \theta \cos \theta \right]$$

$$\frac{\partial^2 \phi}{\partial \theta^2} = \frac{Cr^2}{\tan \alpha - \alpha} \left[-2 \sin 2\theta + 2 \tan \alpha (\cos^2 \theta - \sin^2 \theta) \right]$$

$$\frac{\partial}{\partial r} \left[\frac{1}{r} \frac{\partial \phi}{\partial \theta} \right] = \frac{C}{\tan \alpha - \alpha} \left[-1 + \cos 2\theta + 2 \tan \alpha \sin \theta \cos \theta \right]$$

$$\sigma_{rr} = \frac{1}{r} \frac{\partial \phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2}$$

$$= \frac{C}{\tan \alpha - \alpha} \left[2\alpha - 2\theta - \sin 2\theta - 2 \tan \alpha \sin^2 \theta \right]$$

$$\sigma_{\theta\theta} = \frac{\partial^2 \phi}{\partial r^2} = \frac{C}{\tan \alpha - \alpha} \left[2\alpha - 2\theta + \sin 2\theta - 2 \tan \alpha \cos^2 \theta \right] \quad (30\%)$$

$$\sigma_{r\theta} = -\frac{\partial}{\partial r} \left[\frac{1}{r} \frac{\partial \phi}{\partial \theta} \right] = \frac{C}{\tan \alpha - \alpha} \left[1 - \cos 2\theta - 2 \tan \alpha \sin \theta \cos \theta \right]$$

b) Along OB: $\sigma_{r\theta} = \sigma_{\theta\theta} = 0$

Along OA: $\sigma_{r\theta} = 0, \sigma_{\theta\theta} = -p$.

$$\sigma_{\theta\theta} \Big|_{\theta=\alpha} = \frac{C}{\tan \alpha - \alpha} \left[2\alpha - 2\alpha - \sin 2\alpha - 2 \sin \alpha \cos \alpha \right] = 0$$

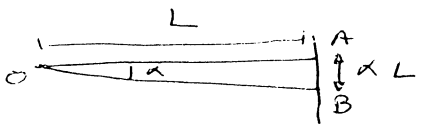
$$\sigma_{r\theta} \Big|_{\theta=\alpha} = \frac{C}{\tan \alpha - \alpha} \left[1 - \cos 2\alpha - 2 \sin^2 \alpha \right] = 0$$

\Rightarrow r.c. along OB satisfied.

$$\sigma_{xx}|_{\theta=0} = \frac{C}{\tan \alpha - \alpha} [2\alpha - 2 \tan \alpha] = -2C = -p$$

$$C = \frac{p}{2}$$

$$\sigma_{xx}|_{\theta=0} = \frac{C}{\tan \alpha - \alpha} [1 - 1 - 0] = 0 \quad (30\%)$$

(c) (i)  consider cantilever of unit depth

$$M = pL \frac{L}{2} = \frac{pL^2}{2}$$

$$I \text{ at } AB = \frac{bd^3}{12} = \frac{1(\alpha L)^3}{12}$$

$$\sigma \text{ at } A = \frac{M_y}{I} = \frac{pL^2}{2} \frac{\alpha L}{2} \cdot \frac{12}{\alpha^3 L^3}$$

$$= \frac{3p}{\alpha^2} \quad (20\%)$$

(ii)

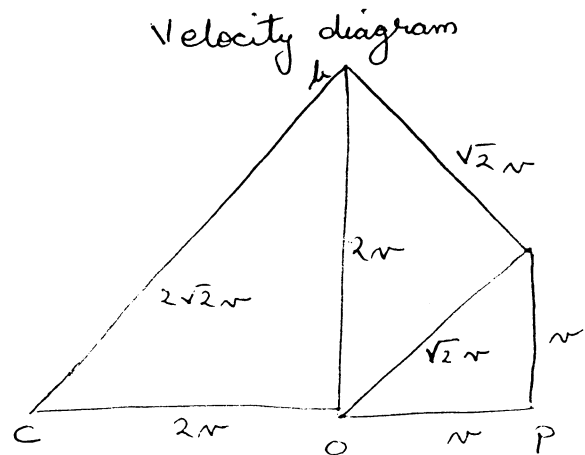
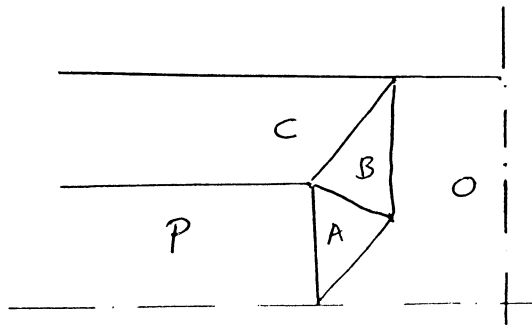
$$\sigma_{xx}|_{\theta=0} = \frac{P}{2(\tan \alpha - \alpha)} [2\alpha]$$

$$\tan \alpha \sim \alpha + \frac{\alpha^3}{3}$$

$$= \frac{P}{2 \frac{\alpha^3}{3}} 2\alpha = \frac{3P}{\alpha^2} \quad (20\%)$$

4)

a)



Unit depth:

~~P~~ Input power = $2lvnp$

power dissipated along OA : $(\sqrt{2}lk)\sqrt{2}v = 2blv$

AB : $2blv$

OB : $(2lk)2v = 4blv$

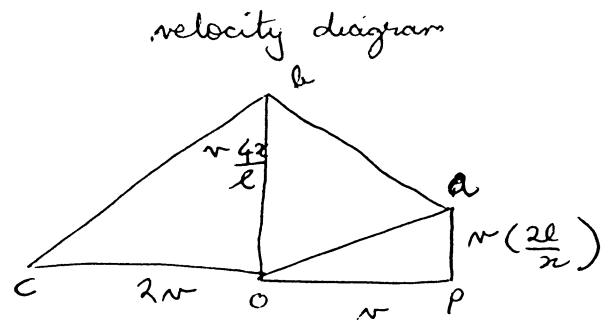
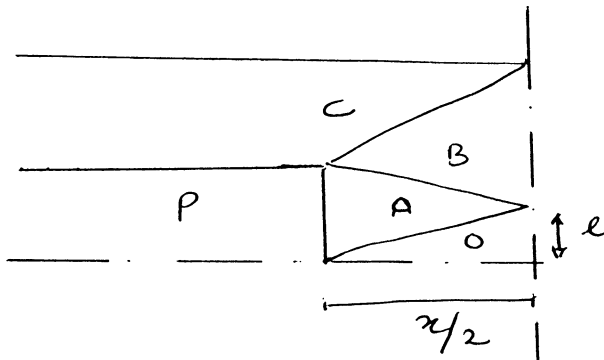
BC : $(\sqrt{2}kl)2\sqrt{2}v = 4blv$

$\Rightarrow 2plv = 12blv$

$p = 6k$

(40%)

b)



I/P power = $2plv$

power dissipated along OA : $k \sqrt{l^2 + \frac{x^2}{4}}$ ~~$2r \sqrt{(\frac{2l}{x})^2 + 1}$~~

$$= \frac{2r k}{x} \left(l^2 + \left(\frac{x}{2}\right)^2 \right)$$

AB : $\frac{2r k}{x} \left(l + \left(\frac{x}{2}\right)^2 \right)$

BC : $k \left[l^2 + \left(\frac{x}{2}\right)^2 \right]^{\frac{1}{2}} \cdot 4r x \left[l^2 + \left(\frac{x}{2}\right)^2 \right]$

$$= \frac{4r k}{x} \left[l^2 + \left(\frac{x}{2}\right)^2 \right]$$

$$2 p_{bc} = \frac{8r k}{x} \left[l^2 + \left(\frac{x}{2}\right)^2 \right]$$

$$p = \frac{4k}{x l} \left[l^2 + \frac{x^2}{4} \right] \quad (40\%)$$

(c) Equate (a) & (b)

$$6k = \frac{4k}{x l} \left[l^2 + \frac{x^2}{4} \right]$$

$$\frac{3x l}{2} = l^2 + \frac{x^2}{4}$$

$$\frac{x}{l} = 3 \pm \sqrt{5}$$

$\frac{x}{2} > l$ for mech. (b) to be operative

$$\Rightarrow x = 5.24 l \quad (20\%)$$