

ENGINEERING TRIPOS PART IIA

Tuesday 3 May 2005 2.30 to 4.00

Module 3C3

MACHINE DESIGN – TRIBOLOGY

*Answer not more than **three** questions.*

All questions carry the same number of marks.

*The **approximate** percentage of marks allocated to each part of a question is indicated in the right margin.*

Attachments:

Special datasheet (10 pages).

**You may not start to read the questions
printed on the subsequent pages of this
question paper until instructed that you
may do so by the Invigilator**

(TURN OVER)

1 (a) Explain briefly the idealisations that are made when applying Reynolds' equation in the analysis of hydrodynamically lubricated bearings. [30%]

(b) Figure 1 shows a Rayleigh step bearing in which the two regions of the step are the same length B . The height of the step is d and the velocity of the lower plane surface is U as shown. The width of the bearing is large in comparison to dimension B and the incompressible lubricant has constant viscosity η . Small holes are drilled at the location of the step so that a proportion β of the oil which flows through the entry region can be filtered and returned to the inlet.

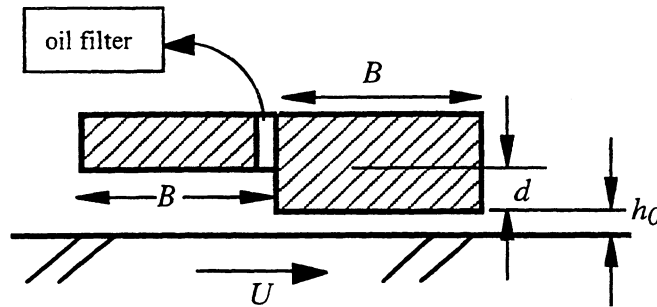


Fig. 1

The maximum hydrodynamic pressure within the bearing p_s is developed at the step. By considering the flow rates in the inlet and outlet regions, show that the value of p_s can be approximately related to the quantities U, B, η, h_0 and β by the expression

$$p_s = \frac{6UB\eta}{h_0^2} \left\{ \frac{(1-\beta)H-1}{(1-\beta)H^3+1} \right\}$$

where H is equal to the ratio $(d+h_0)/h_0$. [40%]

In a particular application the desired value of β is 0.25. Find the numerical relationship between d and h_0 which will maximise the load carrying capacity of a bearing in which this is the case. [30%]

2 A journal bearing of radius R , length L and radial clearance c has a length to diameter ratio of $1/4$. If the Sommerfeld number S is defined as $\left\{ \frac{\eta\omega}{\bar{p}} \right\} \left\{ \frac{R}{c} \right\}^2$ where \bar{p} is the mean nominal pressure on the bearing, ω the speed of rotation and η the viscosity of the lubricant, then the relation between S and the eccentricity ratio ε is as shown in the table below.

ε	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	0.95
S	102	47.6	28.2	17.7	11.2	6.72	3.64	1.65	0.46	.139
Q^*	0.0983	0.196	0.295	0.393	0.491	0.590	0.688	0.787	0.885	0.933
M^*	6.03	5.89	5.83	5.92	6.12	6.50	7.24	8.43	11.8	17.3

(a) Show that if the principal design requirement is to run the loaded bearing with the greatest value of the minimum film thickness h_{\min} , then the appropriate value of ε is approximately 0.7. [30%]

(b) The normalised quantities M^* and Q^* are defined as

$$M^* = \frac{Mc}{\eta\omega LR^3} \quad \text{and} \quad Q^* = \frac{Q}{LR\omega c}$$

where M is the torque required to maintain rotation and Q is the volumetric flow rate of the lubricant. In a particular case, designed for maximum h_{\min} , $W = 5$ kN, $R = 0.05$ m, $c = 75$ μm and $\omega = 300$ s^{-1} . If viscosity is considered constant, estimate the temperature increase ΔT experienced by the lubricant as it flows through the bearing. The density of the lubricant is 880 kg m^{-3} and its specific heat 2.0 $\text{kJ kg}^{-1}\text{K}^{-1}$. [30%]

(c) If the viscosity of the lubricant varies with temperature change ΔT according to the relation

$$\eta = \eta_0 \exp(-\beta \Delta T)$$

where $\beta = 0.04$ K^{-1} and $\eta_0 = 0.05$ Pa s, indicate, by a calculation flow chart, an iterative procedure which could be used to find a better estimate of the steady-state running temperature of this bearing. By making one such iteration, improve your estimate of ΔT made in part (b). [40%]

(TURN OVER)

3 (a) Figure 2 shows the contact geometry between a pair of involute spur gears, with base radii r_{b1} and r_{b2} , rotating at corresponding angular speeds of Ω_1 and Ω_2 .

(i) Explain why the involute tooth geometry dictates that contact between tooth pairs lies along the common tangent AB to the two base circles. [10%]

(ii) Show that the ratio of speeds Ω_1/Ω_2 is equal to the ratio of the base circle radii r_{b2}/r_{b1} . [10%]

(iii) Derive an expression for the sliding velocity between a tooth pair in terms of Ω_1 , Ω_2 and the distance x between the contact position X and the pitch point P. [20%]

(b) Two equal size involute spur gears, each with 29 teeth, mesh together. The gears have standard teeth with module m equal to the addendum and a pressure angle of 20° .

(i) Find the contact ratio. [25%]

(ii) The contact transmits a torque of 5 Nm. Select an appropriate module m for the gears, assuming that the width of the teeth is $5m$ and that the critical condition is for contact between one pair of teeth with an allowable contact stress of 1200 MPa. The effective contact modulus of the gear material $E^* = 115$ GPa. [35%]

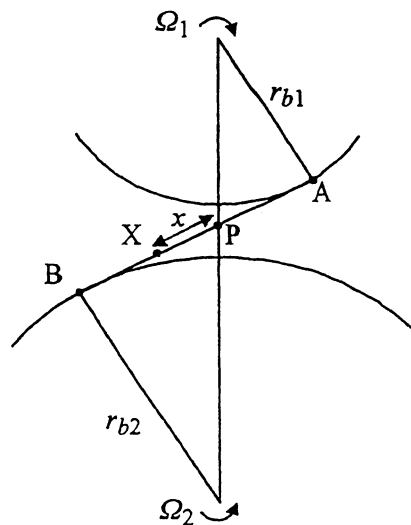


Fig. 2

- 4 (a) Explain briefly the idealisations that are implicit in the Hertzian analysis of tribological contacts. [20%]
- (b) Show that the area of contact between two cylinders of same radius and material pressed into contact with their axes at right angles is approximately circular. [20%]
- (c) A railway vehicle has cylindrical wheels each of radius 350 mm. The mass of the vehicle, which is supported by soft springs, provides a normal load on each wheel of 60 kN. The head of the rail has a radius of curvature of 350 mm so that the contact geometry is effectively that of part (b). The rail is rigidly supported by the track.
- (i) Show that the effective compliance of the wheel-rail contact is approximately $8.43 \times 10^{-10} \text{ m N}^{-1}$. The modulus of the contact can be taken as 115 GPa. [30%]
- (ii) A certain length of the track has small corrugations on the rail surface of a constant wavelength equal to 50 mm. If each wheel has a mass of 300 kg, estimate the speed of the vehicle at which resonant vertical oscillations of the wheel might be expected. [20%]
- (iii) In practice railway wheels are slightly conical to assist stability. Comment briefly on the effect that this might have on the contact conditions between wheel and rail. [10%]

END OF PAPER

ENGINEERING TRIPOS Part IIA

Modules 3C3 and 3C4 Data Sheet

HYDRODYNAMIC LUBRICATION

Viscosity: temperature and pressure effects

Vogel formula $\eta = \eta_0 \exp\left\{\frac{b}{T + T_c}\right\}$

Barus equation $\eta = \eta_0 \exp\{\alpha p\}$

Roelands equation $\eta = \eta_0 \exp\left\{ \left[9.67 + \ln \eta_0 \right] \left[\left(1 + \frac{p}{p_0^*} \right)^\beta - 1 \right] \right\}$

Viscous pressure flow

Rate of flow q_x per unit width of fluid of viscosity η down a channel of height h due to

pressure gradient, $q_x = -\frac{h^3}{12\eta} \frac{dp}{dx}$

Reynolds' Equation for a steady configuration

1-D flow: $\frac{dp}{dx} = 12\eta\bar{U} \left\{ \frac{h-h^*}{h^3} \right\}$

\bar{U} is the entraining velocity so that $|\bar{U}h^*|$ is flow per unit width through the contact.

2-D flow: $\frac{\partial}{\partial x} \left\{ \frac{h^3}{\eta} \frac{\partial p}{\partial x} \right\} + \frac{\partial}{\partial y} \left\{ \frac{h^3}{\eta} \frac{\partial p}{\partial y} \right\} = 12\bar{U} \frac{\partial h}{\partial x}$

Hydrodynamic lubrication of discs

$\frac{h}{R} = C \frac{\eta\bar{U}}{W'}$ where R is the reduced or effective radius and W' the load per unit length

$C_{\min} = 4.00$ for half Sommerfeld boundary conditions

$C_{\min} = 4.89$ for half Reynolds' boundary conditions

ELASTIC CONTACT STRESS FORMULAE

Suffixes 1, 2 refer to the two bodies in contact.

Effective curvature $\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$

where R_1, R_2 are the radii of curvature of the two bodies (convex positive).

Contact modulus $\frac{1}{E^*} = \frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2}$

where E_1, E_2 and ν_1, ν_2 are Young's moduli and Poisson's ratios.

	<u>Line contact</u>	<u>Circular contact</u>
	(width $2b$; load W' per unit length)	(diameter $2a$; load W)
Semi contact width or contact radius	$b = 2 \left\{ \frac{W'R}{\pi E^*} \right\}^{1/2}$	$a = \left\{ \frac{3WR}{4E^*} \right\}^{1/3}$
Maximum contact pressure ("Hertz stress")	$p_0 = \left\{ \frac{W'E^*}{\pi R} \right\}^{1/2}$	$p_0 = \frac{1}{\pi} \left\{ \frac{6WE^{*2}}{R^2} \right\}^{1/3}$
Approach of centres	$\delta = \frac{2W'}{\pi} \left[\frac{1-\nu_1^2}{E_1} \left\{ \ln \left(\frac{4R_1}{b} \right) - \frac{1}{2} \right\} + \frac{1-\nu_2^2}{E_2} \left\{ \ln \left(\frac{4R_2}{b} \right) - \frac{1}{2} \right\} \right]$	$\delta = \frac{a^2}{R} = \frac{1}{2} \left\{ \frac{9}{2} \frac{W^2}{E^{*2} R} \right\}^{1/3}$
Mean contact pressure	$\bar{p} = \frac{W'}{2b} = \frac{\pi}{4} p_0$	$\bar{p} = \frac{W}{\pi a^2} = \frac{2}{3} p_0$
Maximum shear stress	$\tau_{\max} = 0.300 p_0$ at $(x = 0, z = 0.79b)$	$\tau_{\max} = 0.310 p_0$ at $(r = 0, z = 0.48a)$ for $\nu = 0.3$
Maximum tensile stress	zero	$\frac{1}{3}(1-2\nu)p_0$ at $(r = a, z = 0)$

Mildly elliptical contacts

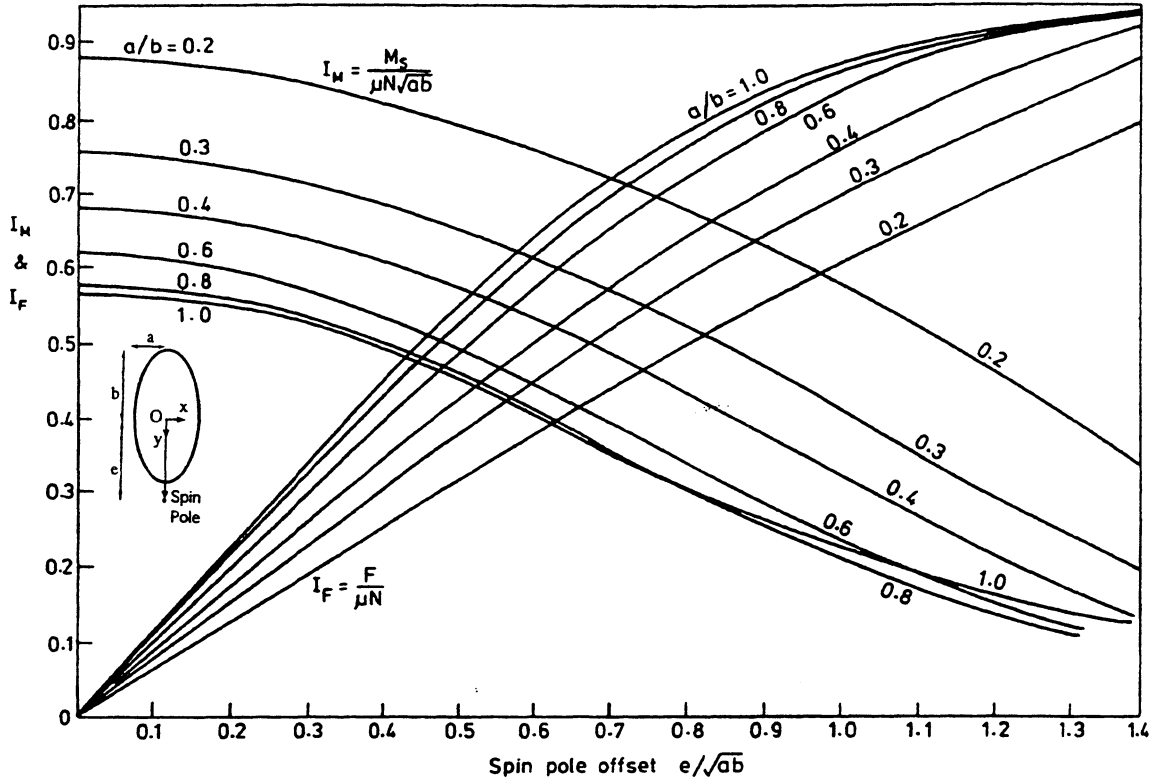
If the gap at zero load is $h = \frac{1}{2}Ax^2 + \frac{1}{2}By^2$, and $0.2 < A/B < 5$

Ratio of semi-axes $b/a \cong (A/B)^{2/3}$

To calculate the contact **area** or Hertz **stress** use the circular contact equations with $R = (AB)^{-1/2}$ or better $R_e = [AB(A+B)/2]^{-1/3}$.

For **approach** use circular contact equation with $R = (AB)^{-1/2}$ (**not** R_e)

Hertzian contact frictional losses



INVOLUTE GEARING

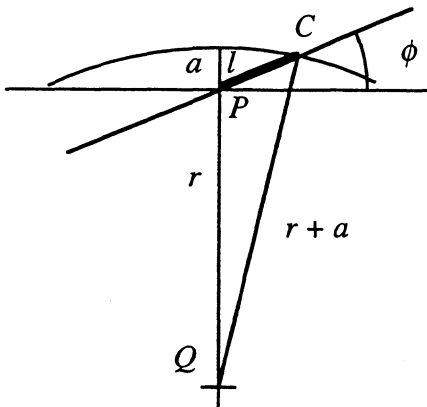
Spur gears

pitch cylinder radii r
 base cylinder radii r_b
 addendum cylinder radii r_a
 number of teeth N
 addendum $a = r_a - r$
 pressure angle ϕ

} with suffix 1 or 2

circumferential pitch $p = 2\pi r/N$
 base pitch $p_b = p \cos \phi$
 module $m = p/\pi = 2r/N$
 ratio of contact r_c
 radius of curvature at pitch point $\rho = r \sin \phi$

Path of contact



$$l = \left\{ r^2 \sin^2 \phi + a(2r + a) \right\}^{1/2} - r \sin \phi$$

For a standard 20° spur wheel with N teeth of module m this becomes

$$\frac{l}{m} = \left(0.02924N^2 + N + 1 \right)^{1/2} - 0.1710N$$

Standard tooth forms

Addendum $a = m$, Dedendum $= \frac{7}{6}m$, pressure angle $= 20^\circ$.

Modules:	0.3 – 1.0 mm in 0.1 mm steps
1.0 – 4.0 mm in 0.25 mm steps	4.0 – 7.0 mm in 0.5 mm steps
7.0 – 16.0 mm in 1.0 mm steps	16.0 – 24.0 mm in 2.0 mm steps
24.0 – 45.0 mm in 3.0 mm steps	45.0 – 75.0 mm in 5.0 mm steps

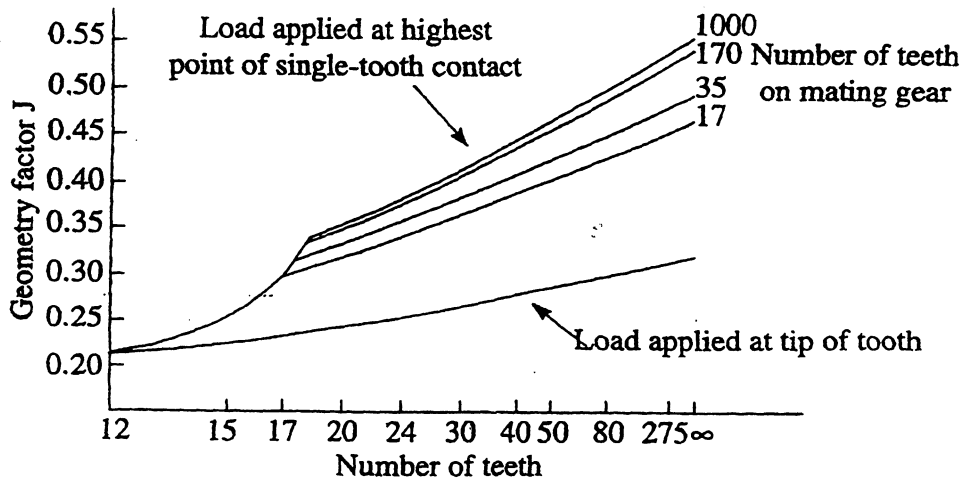
Friction in spur gears

$$\frac{\text{average friction loss}}{\text{power transmitted}} \approx \mu\pi \left\{ \frac{1}{N_1} + \frac{1}{N_2} \right\}$$

Tooth failure

Allowable bending stress σ_b according to AGMA guidelines given by $\sigma_b = \frac{P'_T}{Jm}$

where P'_T is force per unit face-width acting tangentially to pitch circle and J given in the figure below for 20° spur gears. Typical values of σ_b shown in table.



Typical allowable tooth stresses (AGMA)

Material	Condition	Bending fatigue strength σ_b (MPa)	Surface fatigue strength σ_s (MPa)
Steel	Through hardened and tempered	170-390	590-1200
	Carburised and case hardened	380-480	1250-1550
Cast iron	As cast	69-90	450-590
Nodular iron	Quenched, annealed and tempered	150-300	500-800
Malleable iron	Pearlitic	70-145	500-650

EPICYCLIC SPEED RULE

$$\omega_s = (1 + R)\omega_c - R\omega_a \quad \text{where } R = \frac{A}{S}$$

ROLLING ELEMENT BEARINGS

Fatigue life

$$L = a_1 a_2 a_3 (C/P)^p \quad p = 3 \text{ for ball and } 10/3 \text{ for roller bearings}$$

Fatigue probability %	10	5	4	3	2	1
Life adjust factor a_1	1	0.62	0.53	0.44	0.33	0.21

Minimum radial load F_{rm}

$$\text{For a ball bearing } F_{rm} = k_T \left(\frac{\nu n}{1000} \right)^{2/3} \left(\frac{d_m}{100} \right)^2$$

$$\text{For a roller bearing } F_{rm} = k_T \left(6 + \frac{4n}{n_T} \right) \left(\frac{d_m}{100} \right)^2$$

F_{rm} is the minimum radial load in N, d_m is the mean bearing diameter in mm, ν is the kinematic viscosity in mm^2s^{-1} , n the speed in rpm and n_T the limiting speed for oil lubrication. k_T is typically 25 for ball bearings and 150 for roller bearings.

Bearing choice

The information on the following pages concerning minimum loads, viscosities and standard bearing sizes and ratings is extracted from the SKF General Bearing Catalogue and is copied with permission. It is SKF copyright and is not to be further reproduced.

Required viscosities and the effect of viscosity ratio on a_{23}

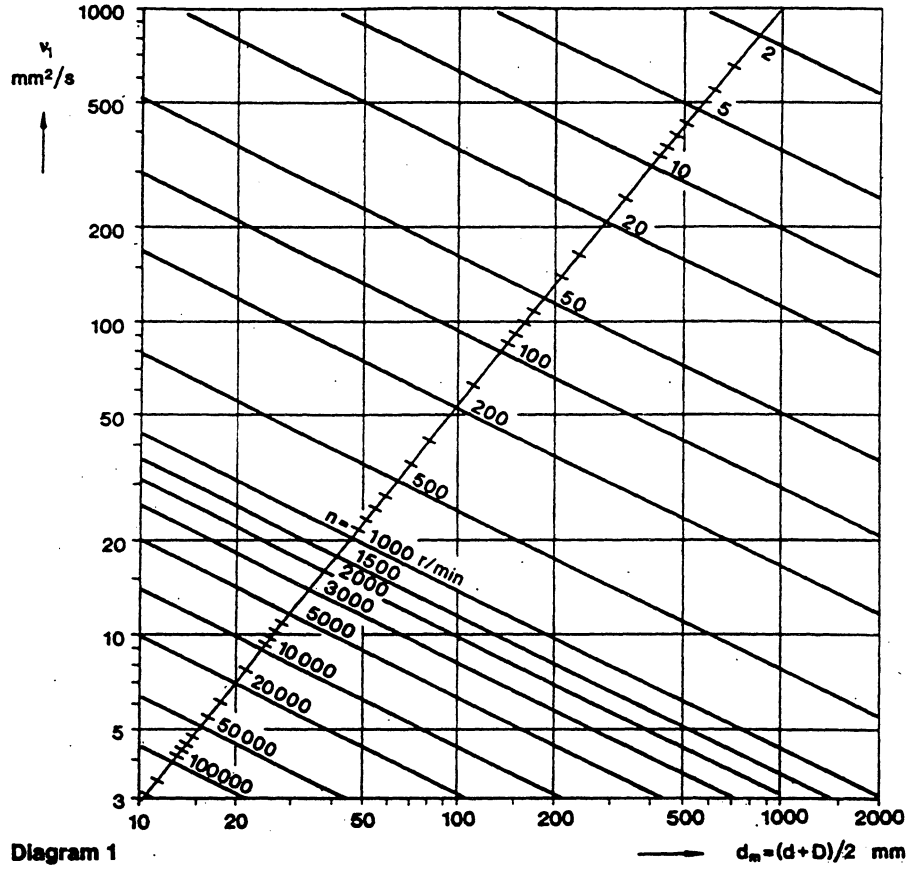


Diagram 1

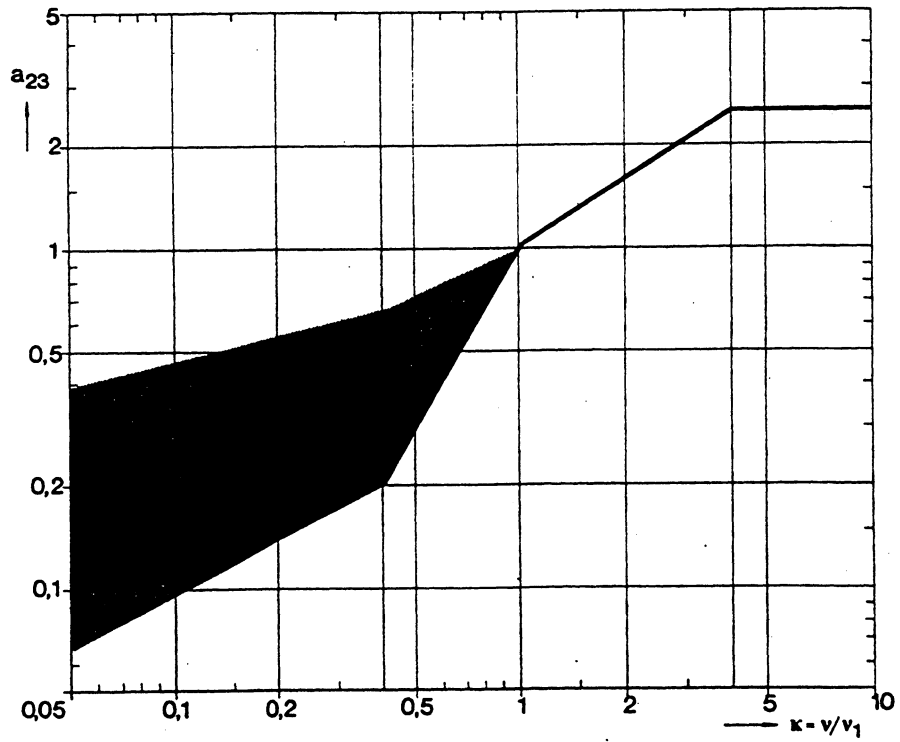
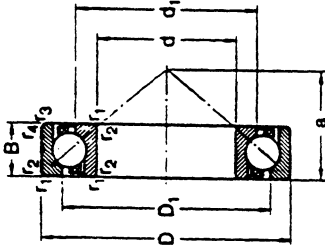
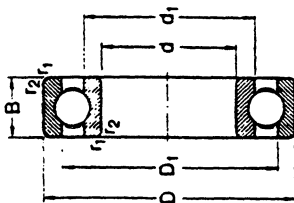


Diagram 3

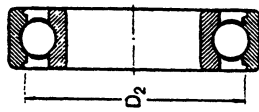
Angular contact ball bearings
single row
d 10-65 mm



Deep groove ball bearings
single row
d 35-55 mm



With full outer ring shoulders

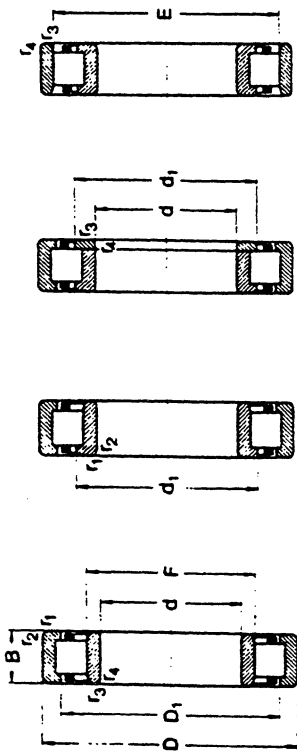


With recessed outer ring shoulders

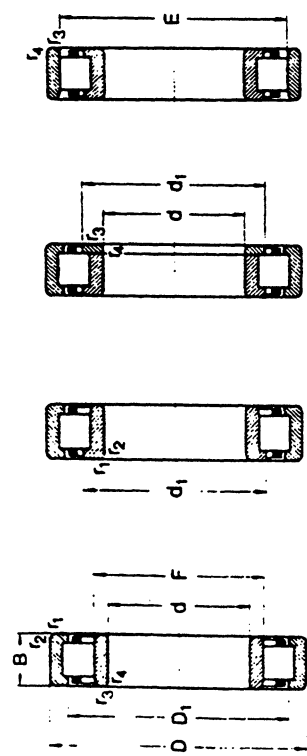
Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation	
	d	D	B					N
35	47	7	4 750	3 200	186	13 000	0.030	61807
	55	10	9 560	6 200	290	11 000	0.080	61907
	62	9	12 400	8 150	375	10 000	0.11	68007
	62	14	15 900	10 200	440	10 000	0.16	6207
	72	17	25 500	15 300	655	9 000	0.29	6307
	80	21	33 200	19 000	815	8 500	0.46	6307
	100	25	55 300	31 000	1 290	7 000	0.95	6407
40	52	7	4 940	3 450	186	11 000	0.034	61808
	62	12	13 800	9 300	425	10 000	0.12	61908
	68	9	13 300	9 150	440	9 500	0.13	68008
	68	15	16 800	11 600	490	8 500	0.19	6008
	80	18	30 700	19 000	800	7 500	0.37	6208
	80	23	41 000	24 000	1 020	6 500	0.63	6308
	110	27	63 700	38 500	1 530	6 700	1.25	6408
45	58	7	6 050	4 300	228	9 500	0.040	61809
	68	12	10 100	6 700	285	9 000	0.14	61909
	75	10	15 600	10 800	520	9 000	0.17	68009
	75	16	20 800	14 600	640	8 000	0.25	6058
	85	19	33 200	21 500	915	7 500	0.41	6209
	100	25	52 700	31 500	1 340	6 700	0.83	6309
	120	29	78 100	45 000	1 900	6 000	1.55	6409
60	65	7	6 240	4 750	250	9 000	0.052	61810
	72	12	14 600	10 400	500	8 500	0.14	61910
	80	10	16 300	11 400	560	8 500	0.18	68010
	80	16	21 600	16 000	710	8 500	0.28	6010
	90	20	35 100	23 200	980	7 000	0.46	6210
	110	27	61 800	38 000	1 600	6 300	1.05	6310
	130	31	87 100	52 000	2 200	5 300	1.90	6410
65	72	9	8 320	6 200	325	8 500	0.083	61811
	80	13	15 900	11 400	560	8 000	0.19	61911
	90	11	19 500	14 000	695	7 500	0.26	68011
	90	16	28 100	21 200	900	7 500	0.39	6011
	100	21	43 600	29 000	1 250	6 300	0.61	6211
	120	29	71 500	45 000	1 900	5 600	1.35	6311
	140	33	99 500	62 000	2 600	5 000	2.30	6411

Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation	
	d	D	B					N
10	30	9	7 020	3 350	140	19 000	0.030	7200 BE
12	32	10	7 610	3 800	160	18 000	0.038	7201 BE
	37	12	10 600	5 000	208	17 000	0.060	7301 BE
15	35	11	8 940	4 600	204	17 000	0.045	7202 BE
	42	13	13 000	6 700	280	15 000	0.080	7302 BE
17	40	12	11 100	6 100	260	15 000	0.065	7203 BE
	47	14	15 900	8 300	355	13 000	0.11	7303 BE
20	47	14	14 000	8 300	355	12 000	0.11	7204 BE
	52	15	19 000	10 400	440	11 000	0.14	7304 BE
25	52	15	15 600	10 200	430	10 000	0.13	7205 BE
	62	17	26 000	15 800	655	9 000	0.23	7305 BE
30	62	16	23 800	15 600	655	8 500	0.20	7206 BE
	72	19	34 500	21 200	900	8 000	0.34	7306 BE
35	72	17	30 700	20 800	880	9 000	0.28	7207 BE
	80	21	39 000	24 500	1 040	7 500	0.45	7307 BE
40	80	18	38 400	26 000	1 100	7 000	0.37	7208 BE
	90	23	49 400	33 500	1 400	6 700	0.63	7308 BE
45	85	19	37 700	28 000	1 200	6 700	0.42	7209 BE
	100	25	60 500	41 500	1 750	6 000	0.85	7309 BE
60	90	20	39 000	30 500	1 280	6 000	0.47	7210 BE
	110	27	74 100	51 000	2 200	6 500	1.10	7310 BE
65	100	21	48 800	38 000	1 620	5 600	0.82	7211 BE
	120	29	85 200	60 000	2 550	4 800	1.40	7311 BE
60	110	22	57 200	45 500	1 930	5 000	0.80	7212 BE
	130	31	95 600	69 500	3 000	4 500	1.75	7312 BE
68	120	23	66 300	54 000	2 280	4 500	1.00	7213 BE
	140	33	108 000	80 000	3 350	4 300	2.15	7313 BE

Cylindrical roller bearings single row d 50-55 mm



Cylindrical roller bearings single row d 40-45 mm



Type N

Type NUP

Type NUJ

Type NU

Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation
	d	D	B				
d	50	80	16	30 800	34 500	4 000	NU 1010
				64 400	69 500	8 800	NU 210 EC
				64 400	69 500	8 800	NJ 210 EC
				64 400	69 500	8 800	NUP 210 EC
				64 400	69 500	8 800	N 210 EC
				78 100	86 000	11 400	NU 2210 EC
				78 100	86 000	11 400	NJ 2210 EC
				78 100	86 000	11 400	NUP 2210 EC
				110 27	112 000	15 000	NU 310 EC
				110 27	110 000	15 000	NJ 310 EC
				110 27	112 000	15 000	NUP 310 EC
				110 27	112 000	15 000	N 310 EC
				161 000	186 000	24 500	NU 2310 EC
				161 000	186 000	24 500	NJ 2310 EC
				161 000	186 000	24 500	NUP 2310 EC
				130 31	130 000	16 600	NU 410
				130 31	130 000	16 600	NJ 410
				57 200	69 500	8 300	NU 1011 EC
				84 200	95 000	12 200	NU 211 EC
				84 200	95 000	12 200	NJ 211 EC
				84 200	95 000	12 200	NUP 211 EC
				84 200	95 000	12 200	N 211 EC
				99 000	118 000	15 300	NU 2211 EC
				99 000	118 000	15 300	NJ 2211 EC
				99 000	118 000	15 300	NUP 2211 EC
				99 000	118 000	15 300	N 2211 EC
				138 000	143 000	18 600	NU 311 EC
				138 000	143 000	18 600	NJ 311 EC
				138 000	143 000	18 600	NUP 311 EC
				138 000	143 000	18 600	N 311 EC

Type N

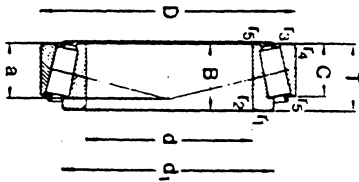
Type NUP

Type NUJ

Type NU

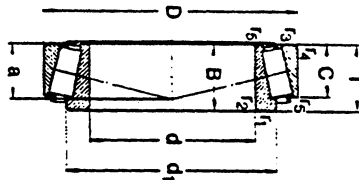
Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation
	d	D	B				
d	40	80	23	80 900	78 000	10 200	NU 308 EC
				80 900	78 000	10 200	NJ 308 EC
				80 900	78 000	10 200	NUP 308 EC
				80 900	78 000	10 200	N 308 EC
				112 000	120 000	15 300	NU 2308 EC
				112 000	120 000	15 300	NJ 2308 EC
				112 000	120 000	15 300	NUP 2308 EC
				96 800	90 000	11 600	NU 408
				96 800	90 000	11 600	NJ 408
				96 800	90 000	11 600	NUP 408
				44 600	52 000	6 300	NU 1009 EC
				60 500	64 000	8 150	NU 209 EC
				60 500	64 000	8 150	NJ 209 EC
				60 500	64 000	8 150	NUP 209 EC
				60 500	64 000	8 150	N 209 EC
				73 700	81 500	10 600	NU 2209 EC
				73 700	81 500	10 600	NJ 2209 EC
				73 700	81 500	10 600	NUP 2209 EC
				73 700	81 500	10 600	N 2209 EC
				99 000	100 000	12 900	NU 309 EC
				99 000	100 000	12 900	NJ 309 EC
				99 000	100 000	12 900	NUP 309 EC
				99 000	100 000	12 900	N 309 EC
				138 000	153 000	20 000	NU 2309 EC
				138 000	153 000	20 000	NJ 2309 EC
				138 000	153 000	20 000	NUP 2309 EC
				138 000	153 000	20 000	N 2309 EC
				106 000	102 000	13 400	NU 409
				106 000	102 000	13 400	NJ 409
				106 000	102 000	13 400	NUP 409
				106 000	102 000	13 400	N 409

Taper roller bearings
single row
d 35-50 mm



Principal dimensions	d	D	T	C	C ₀	B	A	d	d ₁	r ₁	r ₂	r ₃	r ₄	r ₅	r ₆
35 (cont.)	80	22.75	72.100	73.500	8.500	5.000	6.700	0.52	30307	2FB					
	80	22.75	61.600	67.000	7.800	4.500	6.000	0.52	31307	2FE					
40	80	32.75	95.200	106.000	12.200	4.800	6.300	0.73	32307	2FE					
	80	32.75	83.500	114.000	13.200	4.500	6.000	0.80	32307 B	2FE					
45	80	42.75	128.000	140.000	18.300	5.300	7.000	1.00	33308	2FD					
	80	42.75	117.000	140.000	18.300	5.300	7.000	1.10	32308 B	2FD					

Taper roller bearings
single row
d 50-65 mm



Principal dimensions	d	D	T	C	C ₀	B	A	d	d ₁	r ₁	r ₂	r ₃	r ₄	r ₅	r ₆
50 (cont.)	110	28.25	125.000	140.000	17.000	3.600	4.800	1.25	30310	2FB					
	110	28.25	106.000	120.000	14.300	3.200	4.300	1.20	31310	2FB					
55	110	42.25	172.000	212.000	24.500	3.200	4.300	1.80	32310	2FD					
	110	42.25	161.000	216.000	26.000	3.200	4.300	1.85	32310 B	2FD					
60	120	45.5	188.000	230.000	29.000	3.000	4.000	2.30	32311	2FD					
	120	45.5	180.000	250.000	30.000	2.800	3.800	2.50	32311 B	2FD					

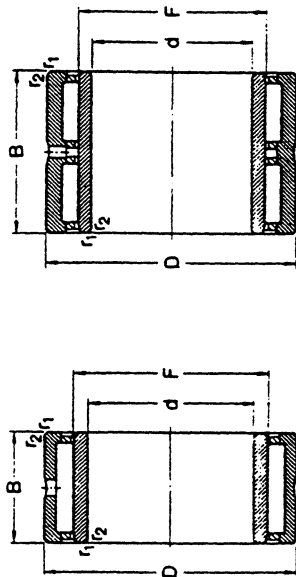


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Principal dimensions	d	D	T	C	C ₀	B	A	d	d ₁	r ₁	r ₂	r ₃	r ₄	r ₅	r ₆
50	60	20	60.500	68.000	9.650	4.500	6.000	0.37	32010 X	3CC					
	60	20	69.500	102.000	11.400	4.500	6.000	0.45	33010	3CC					
65	80	21.5	72.100	100.000	11.000	4.500	6.000	0.43	K-JLM 104948/K-JLM 104910	3CC					
	80	21.5	85.800	132.000	13.700	4.300	5.800	0.58	33110	3CC					
75	80	21.75	76.500	91.500	10.400	4.300	5.800	0.54	30210	3DB					
	80	21.75	82.500	100.000	11.600	4.300	5.800	0.61	32210	3DB					
80	28	108.000	140.000	16.300	4.000	5.300	0.75	K-JM 205149/K-JM 205110	3DC						
	28	108.000	140.000	16.300	4.000	5.300	0.75	K-JM 205149/K-JM 205110 A	3DC						
90	32	114.000	160.000	18.300	3.800	5.000	0.90	32310	3CC						
	32	114.000	200.000	22.800	3.800	5.000	1.30	T2ED 050	3CC						
100	36	154.000	197.000	18.000	3.800	4.500	1.20	T2ED 050	3CC						
	36	154.000	197.000	18.000	3.800	4.500	1.20	T2ED 050	3CC						

Principal dimensions	d	D	T	C	C ₀	B	A	d	d ₁	r ₁	r ₂	r ₃	r ₄	r ₅	r ₆
65	100	23	84.200	127.000	14.300	3.400	4.500	0.83	32013 X	4CC					
	100	23	96.800	156.000	17.000	3.400	4.500	0.78	33013	2CE					
70	110	27	123.000	183.000	21.200	3.200	4.300	1.05	K-JM 511844/K-JM 511810	3DE					
	110	27	142.000	208.000	24.500	3.000	4.000	1.30	32113	3DE					
75	120	24.75	114.000	134.000	16.300	3.000	4.000	1.15	30213	3CC					
	120	24.75	151.000	193.000	23.200	3.000	4.000	1.50	32213	3CC					
80	38	181.000	240.000	27.600	2.800	3.600	1.85	T2ED 045	3ED						
	38	181.000	240.000	27.600	2.800	3.600	1.85	T2ED 045	3ED						

**Needle roller bearings with flanges
with inner ring**
d 40-65 mm



Series NK(S), NA 49

Series NA 69

Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation
	dynamic	static	C_0				
d	D	B	C	N	N	kg	
mm	mm	mm	mm	N	r/min	kg	
40	55	20	27 500	57 000	7 200	6 300	0.14 NKI 40/20
	55	30	40 200	83 000	12 000	9 000	0.22 NKI 40/30
	62	22	42 800	71 000	9 150	5 600	0.23 NA 4908
	62	40	67 100	125 000	16 000	8 000	0.43 NA 6908
	65	22	42 800	72 000	9 150	5 600	0.28 NKIS 40
42	57	20	29 200	61 000	7 650	6 000	0.15 NKI 42/20
	57	30	41 800	98 000	12 800	8 500	0.22 NKI 42/30
46	62	25	38 000	78 000	10 000	5 600	0.23 NKI 45/25
	62	35	49 500	110 000	14 300	8 000	0.32 NKI 45/35
	68	22	45 700	78 000	10 000	5 300	0.27 NA 4909
	68	40	70 400	137 000	17 300	7 500	0.50 NA 6909
	72	22	44 600	78 000	10 000	5 000	0.34 NKIS 45
50	68	25	40 200	88 000	11 200	5 300	0.27 NKI 50/25
	68	35	52 300	122 000	16 000	7 500	0.38 NKI 50/35
	72	22	47 300	85 000	11 000	5 000	0.27 NA 4910
	72	40	73 700	150 000	19 000	7 000	0.52 NA 6910
	80	28	62 700	104 000	13 700	4 500	0.52 NKIS 50
55	72	25	41 800	98 500	12 200	4 800	0.27 NKI 55/25
	72	35	55 000	134 000	17 600	6 700	0.38 NKI 55/35
	80	25	57 200	106 000	13 700	4 500	0.40 NA 4911
	80	45	89 700	190 000	24 000	6 300	0.78 NA 6911
	85	28	66 000	114 000	15 000	4 300	0.58 NKIS 55
60	82	25	44 000	98 000	12 000	4 300	0.40 NKI 60/25
	82	35	60 500	146 000	19 000	6 000	0.55 NKI 60/35
	85	25	60 500	114 000	14 800	4 300	0.43 NA 4912
	85	45	93 500	204 000	28 000	6 000	0.81 NA 6912
	90	28	68 200	120 000	15 600	4 000	0.58 NKIS 60
65	90	25	61 600	120 000	15 300	4 000	0.46 NA 4913
	90	25	52 800	106 000	13 700	4 000	0.47 NKI 65/25
	90	35	73 700	163 000	21 600	5 600	0.86 NKI 65/35
	90	45	95 200	212 000	27 000	4 000	0.83 NA 6913
	95	28	70 400	132 000	17 000	3 800	0.84 NKIS 65