

- (a) Think of cubes as AAA bodies
 (b) that, like spheres, have all axes through their centre principal.

The body described is an 8-cube cube with a cube missing.

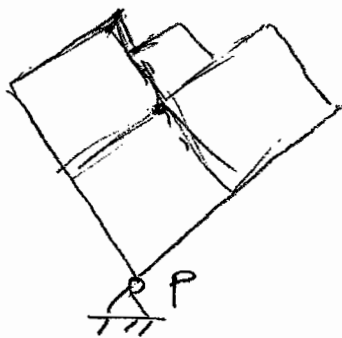
For the small cube $A_1 = \frac{1}{6} m a^2$

For the Eight-cube cube $A_8 = \frac{1}{6} 8M (2a)^2 = \frac{32}{6} M a^2$

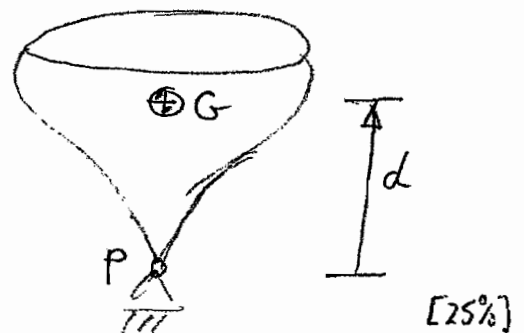
The moment of inertia along PO is , since PO is principal for both cubes,

$$C = A_8 - A_1 = \frac{31}{6} M a^2 \quad [25\%]$$

The resulting 7-cube body is an AAC body, just like a spinning top. So we can draw it like a top



≡



[25%]

- (b) G is distance r from O such that the "missing" cube of mass m when added to the 7m body has its G at O

hence $7m r = M \frac{a}{2} \sqrt{3}$

$\therefore r = \frac{a}{14} \sqrt{3}$

Hence distance PG = d = $a\sqrt{3} \left(1 - \frac{1}{14}\right) = \frac{13\sqrt{3} a}{14}$ [25%]

(d) Steady precession of a fast-spinning top

Gyro equation 2

$$-C\omega_3\omega_1 = Q_2$$

with $Q_2 = 7mgd \sin\theta$

and $\omega_1 = -\dot{\phi} \sin\theta$

$$\therefore \dot{\phi} = \frac{7mgd}{C\omega}$$

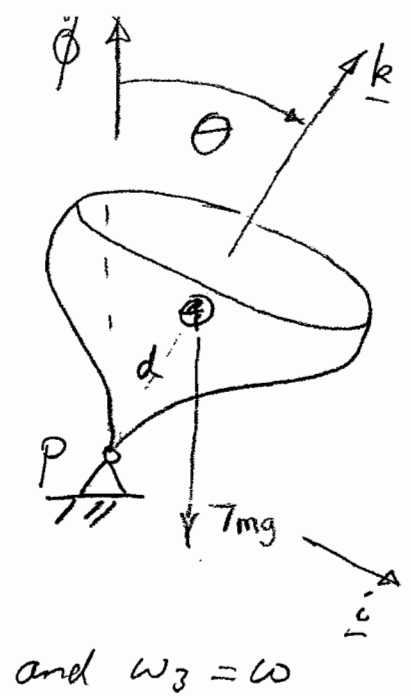
and $C = \frac{31}{6} ma^2$

$$d = \frac{13\sqrt{3}}{14} a$$

$$\therefore \dot{\phi} = \frac{13\sqrt{3}}{14} \frac{6}{31} \frac{7g}{a\omega}$$

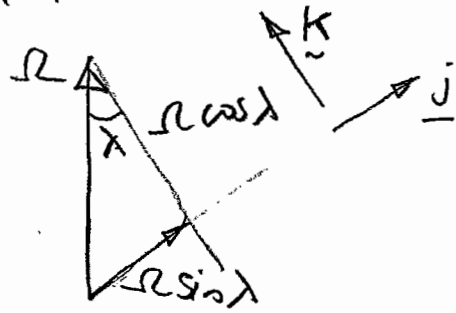
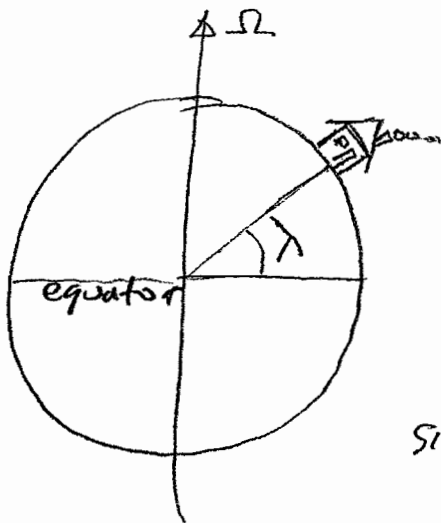
$$= \frac{78\sqrt{3}}{62} \frac{g}{a\omega}$$

$$= 2.18 \frac{g}{a\omega}$$

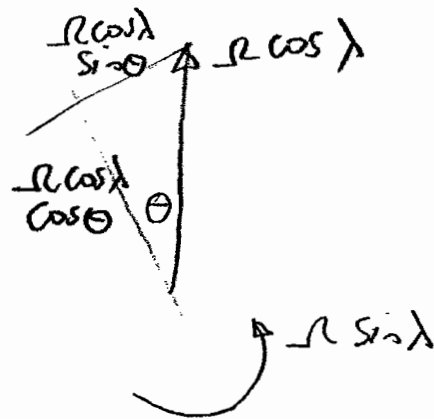
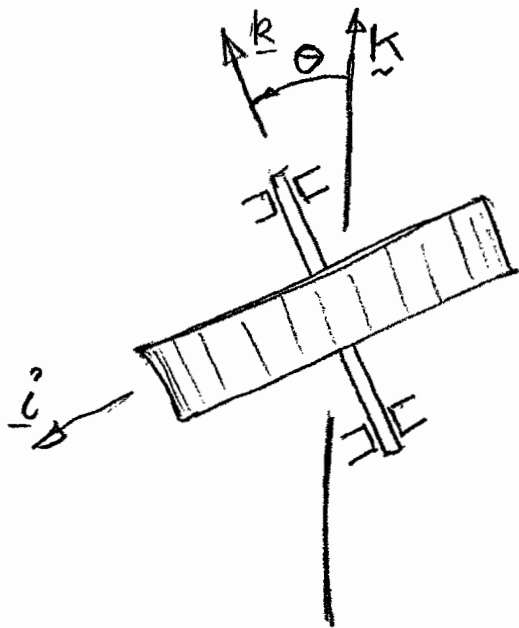


[25%]

2 (a) First resolve the Earth's Ω into the local reference frame



Next resolve the $\Omega \cos \lambda$ component into its \underline{i} & \underline{k} components

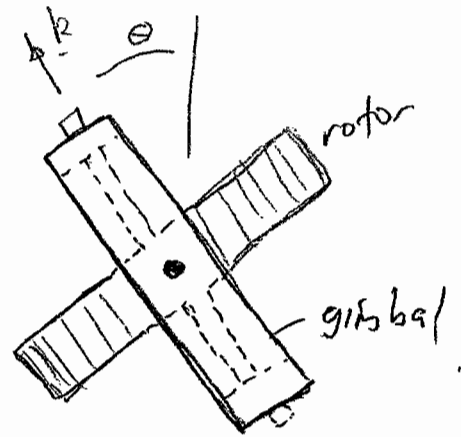


So the angular velocity of the reference frame (the gimbal) is

$$\begin{aligned} \Omega_1 &= -\Omega \cos \lambda \sin \theta \\ \Omega_2 &= \Omega \sin \lambda + \dot{\theta} \\ \Omega_3 &= \Omega \cos \lambda \cos \theta \end{aligned}$$

and with fast spin $\omega_3 \gg \Omega_3$

- (b) The gimbal is free to
- (c) rotate about the \underline{j} axis and the rotor is free about the \underline{k} axis but the \underline{i} axis is constrained



So $Q_1 \neq 0$ $Q_2 = 0$, $Q_3 = 0$

Use the second gyro equation

$$A \dot{\Omega}_2 + (A - C \cos \lambda - C \omega_3) \Omega_1 = 0$$

(post spin)

$$\therefore A \ddot{\theta} + C \omega_3 \cos \lambda \sin \theta = 0$$

$$\therefore \ddot{\theta} + \lambda^2 \sin \theta = 0 \quad \lambda^2 = \frac{C \omega_3 \cos \lambda}{A}$$

This has two steady-state solutions for $\sin \theta = 0$

$$\theta = 0 \quad , \quad \theta = \pi$$

Test these for stability :

$$\theta = \text{small} \quad \therefore \ddot{\theta} + \lambda^2 \theta = 0$$

- Stable SHM at frequency λ [40%]

$$\theta = \pi + \alpha \quad , \quad \sin \theta = -\sin \alpha \quad , \quad \ddot{\theta} = \ddot{\alpha}$$

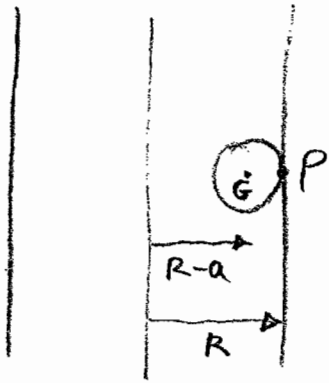
$$\alpha = \text{small} \quad \therefore \ddot{\alpha} - \lambda^2 \alpha = 0$$

unstable $e^{\lambda t}$ solutions

Hence the gyrocompass oscillates about $\theta = 0$ (ie North)

Damping causes this oscillation to die away and the gyrocompass comes to rest pointing north [30%]

3



(a) P in the ball is at rest (no slip) and G is moving on a horizontal circle

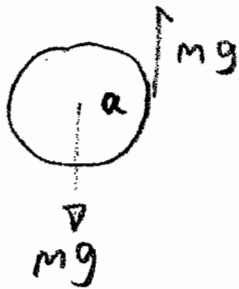
$$\underline{v}_G = (R-a) \underline{j}$$

$$\begin{aligned} \underline{v}_P &= \underline{v}_G + \underline{\omega} \times a \underline{i} \\ &= (R-a) \underline{j} + \omega_3 a \underline{j} - \omega_2 a \underline{k} \\ &= 0 \end{aligned}$$

$$\therefore \omega_3 = -\frac{(R-a)}{a} \Omega \quad \text{and} \quad \omega_2 = 0 \quad [25\%]$$

No constraint on ω_1 , yet

(b)



(i) $\underline{Q} = -mga \underline{j}$

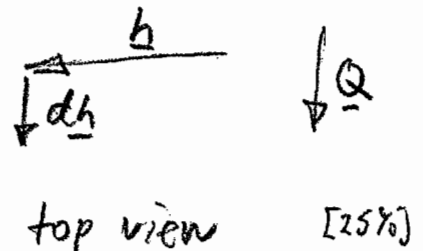
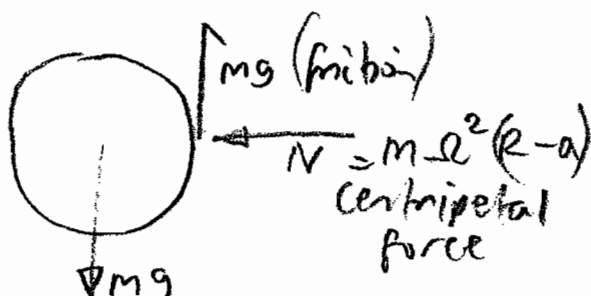
(ii) $\underline{h} = A(\omega_1 \underline{i} + \omega_2 \underline{j} + \omega_3 \underline{k})$
 $= \frac{2}{5} ma^2 (\omega_1 \underline{i} - \frac{R-a}{a} \Omega \underline{k})$ [25%]

(c) $\underline{Q} = \dot{\underline{h}}$ and in steady state $\omega_1 = \text{const}$
 $\Omega = \text{const}$

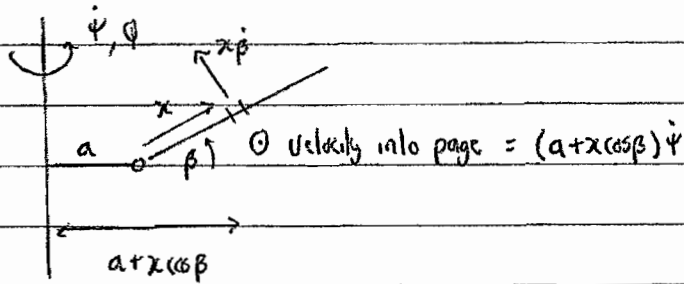
$$\begin{aligned} \therefore \underline{h} &= \underline{h}|_{\text{rot}} + \underline{\Omega} \times \underline{h} \\ &= 0 + \Omega \underline{k} \times \underline{h} \\ &= \frac{2}{5} ma^2 \omega_1 \Omega \underline{j} \end{aligned}$$

$$\therefore -mga \underline{j} = \frac{2}{5} ma^2 \omega_1 \Omega \underline{j} \quad \therefore \underline{\omega}_1 = \underline{\underline{-\frac{5}{2} \frac{g}{a\Omega}}} \quad [25\%]$$

(d)



4) a)



$$T = \frac{1}{2} m \int_0^L [(x\dot{\beta})^2 + (a+x\cos\beta)^2 \dot{\psi}^2] dx$$

$$T = \frac{1}{2} mL^3 \dot{\beta}^2 + \frac{1}{2} ma^2L \dot{\psi}^2 + \frac{1}{2} maL^2 \cos\beta \dot{\psi}^2 + \frac{1}{6} mL^3 \cos^2\beta \dot{\psi}^2 \quad [25\%]$$

b) For β , generalized momentum $\equiv \frac{\partial T}{\partial \dot{\beta}} = \frac{1}{3} mL^3 \dot{\beta}$ = moment of momentum about Flap hinge

For ψ , generalized momentum $\equiv \frac{\partial T}{\partial \dot{\psi}} = (ma^2L + maL^2 \cos\beta + \frac{1}{3} mL^3 \cos^2\beta) \dot{\psi}$
= moment of momentum about rotor axis [25%]

c) For β , $\frac{d}{dt} \left[\frac{\partial T}{\partial \dot{\beta}} \right] - \frac{\partial T}{\partial \beta} + \frac{\partial V}{\partial \beta} = 0$ with $V = (ML)g \times \frac{1}{2} L \sin\beta$ ← gravitational P.E.

$$\Rightarrow \frac{1}{3} mL^3 \ddot{\beta} - \left[-\frac{1}{2} maL^2 \sin\beta \dot{\psi}^2 - \frac{1}{3} mL^3 \cos\beta \sin\beta \dot{\psi}^2 \right] + \frac{1}{2} MgL^2 \cos\beta = 0$$

$$\Rightarrow \frac{1}{3} mL^3 \ddot{\beta} + \left[\frac{1}{2} maL^2 \sin\beta + \frac{1}{3} mL^3 \cos\beta \sin\beta \right] \dot{\psi}^2 = -\frac{1}{2} MgL^2 \cos\beta \quad (*)$$

For ψ , $\frac{d}{dt} \left[\frac{\partial T}{\partial \dot{\psi}} \right] - \frac{\partial T}{\partial \psi} + \frac{\partial V}{\partial \psi} = 0$

$$\Rightarrow \frac{d}{dt} \left[(ma^2L + maL^2 \cos\beta + \frac{1}{3} mL^3 \cos^2\beta) \dot{\psi} \right] = 0 \quad [25\%]$$

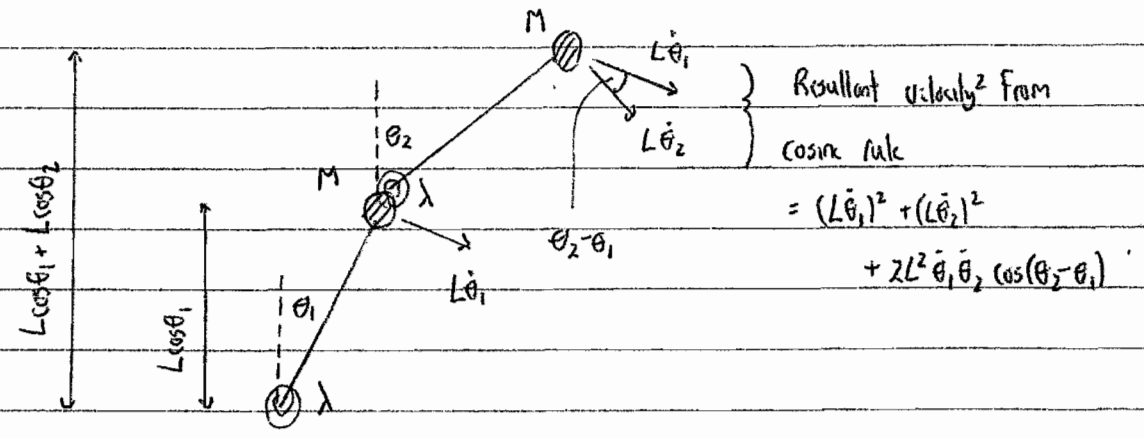
↑ could be expanded

d) For $\dot{\psi}$ constant, and β small, equation (*) becomes:

$$\frac{1}{3} mL^3 \ddot{\beta} + \left(\frac{1}{2} maL^2 + \frac{1}{3} mL^3 \right) \dot{\psi}^2 \beta = -\frac{1}{2} MgL^2$$

For SHM, $\omega_n^2 = \left(\frac{1}{2} maL^2 + \frac{1}{3} mL^3 \right) \dot{\psi}^2 / \left(\frac{1}{3} mL^3 \right) = \dot{\psi}^2 \left(1 + \frac{3a}{2L} \right) \quad [25\%]$

5 a)



$$T = \frac{1}{2} m [(L\dot{\theta}_1)^2 + (L\dot{\theta}_1)^2 + (L\dot{\theta}_2)^2 + 2L^2 \dot{\theta}_1 \dot{\theta}_2 \cos(\theta_2 - \theta_1)]$$

$$V = Mg [L\cos\theta_1 + L\cos\theta_1 + L\cos\theta_2] + \frac{1}{2} \lambda \theta_1^2 + \frac{1}{2} \lambda (\theta_2 - \theta_1)^2 \quad [25\%]$$

b) For mass matrix $M_{ij} = \frac{\partial^2 T}{\partial \dot{\theta}_i \partial \dot{\theta}_j} \Big|_{\theta_i = \theta_j = 0}$

$$\frac{\partial^2 T}{\partial \dot{\theta}_1^2} \Big|_0 = 2ML^2 \quad \frac{\partial^2 T}{\partial \dot{\theta}_1 \partial \dot{\theta}_2} \Big|_0 = ML^2 \quad \frac{\partial^2 T}{\partial \dot{\theta}_2^2} = ML^2$$

For stiffness matrix $k_{ij} = \frac{\partial^2 V}{\partial \theta_i \partial \theta_j} \Big|_{\theta_i = \theta_j = 0}$

$$\frac{\partial^2 V}{\partial \theta_1^2} \Big|_0 = -2MgL + 2\lambda \quad \frac{\partial^2 V}{\partial \theta_1 \partial \theta_2} \Big|_0 = -\lambda \quad \frac{\partial^2 V}{\partial \theta_2^2} \Big|_0 = -MgL + \lambda$$

$$\Rightarrow ML^2 \begin{pmatrix} 2 & 1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{pmatrix} + \begin{pmatrix} -2MgL + 2\lambda & -\lambda \\ -\lambda & -MgL + \lambda \end{pmatrix} \begin{pmatrix} \theta_1 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix} \quad [30\%]$$

c) For natural frequencies $|\omega^2 M + k| = 0$

$$\Rightarrow \begin{vmatrix} -2ML^2\omega^2 - 2MgL + 2\lambda & -ML^2\omega^2 - \lambda \\ -ML^2\omega^2 - \lambda & -ML^2\omega^2 - MgL + \lambda \end{vmatrix} = 0$$

$$\Rightarrow 2 (ML^2\omega^2 + MgL - \lambda)^2 = (ML^2\omega^2 + \lambda)^2 \Rightarrow (ML^2\omega^2 + MgL - \lambda) = \pm \frac{1}{\sqrt{2}} (ML^2\omega^2 + \lambda) \quad [*]$$

For lowest frequency take "-" root $\Rightarrow (1 - \frac{1}{\sqrt{2}}) ML^2\omega^2 = (1 - \frac{1}{\sqrt{2}}) \lambda - MgL$

This yields $\omega=0$ For $MgL/\lambda = 1 - \frac{1}{\sqrt{2}}$

For $MgL/\lambda > 1 - \frac{1}{\sqrt{2}}$ the structure is unstable and will buckle

[20%]

d) Neglecting "g" terms, $(1 + \frac{1}{\sqrt{2}})ML^2\omega^2 = (1 - \frac{1}{\sqrt{2}})\lambda \Rightarrow \omega_1^2 = \left(\frac{\sqrt{2}-1}{\sqrt{2}+1}\right) \frac{\lambda}{ML^2}$
or $(1 - \frac{1}{\sqrt{2}})ML^2\omega^2 = (1 + \frac{1}{\sqrt{2}})\lambda \Rightarrow \omega_2^2 = \left(\frac{\sqrt{2}+1}{\sqrt{2}-1}\right) \frac{\lambda}{ML^2}$

For mode shapes:
$$\begin{pmatrix} -2ML^2\omega^2 + 2\lambda & -ML^2\omega^2 - \lambda \\ \checkmark & \checkmark \end{pmatrix} \begin{pmatrix} \theta_1 \\ \theta_2 \end{pmatrix} = \begin{pmatrix} 0 \\ \checkmark \end{pmatrix}$$

And $2ML^2\omega^2 - \lambda = \begin{matrix} \checkmark \text{ mode 2} \\ \pm \sqrt{2} (ML^2\omega^2 + \lambda) \\ \checkmark \text{ mode 1} \end{matrix}$ From equation [4]

\Rightarrow Mode 1 has $(-\sqrt{2}\theta_1 + \theta_2) = 0 \Rightarrow \theta_2 = \sqrt{2}\theta_1$

Mode 2 has $(+\sqrt{2}\theta_1 + \theta_2) = 0 \Rightarrow \theta_2 = -\sqrt{2}\theta_1$

[25%]