

ENGINEERING TRIPOS PART IIA

Tuesday 3 May 2011 2.30 to 4

Module 3C8

MACHINE DESIGN

Answer not more than three questions.

All questions carry the same number of marks.

The approximate percentage of marks allocated to each part of a question is indicated in the right margin.

Attachment:

Module 3C8 data sheet (9 pages).

STATIONERY REQUIREMENTS

Single-sided script paper

SPECIAL REQUIREMENTS

Engineering Data Book

CUED approved calculator allowed

**You may not start to read the questions
printed on the subsequent pages of this
question paper until instructed that you
may do so by the Invigilator**

1 Figure 1 shows a cross-section of a half-toroidal continuously variable transmission (CVT). The steel input disc is on the left and rotates at angular speed Ω . The steel output disc is on the right. Power is transmitted from the input disc to the output disc through contacts with three intermediate steel discs; only one of the intermediate discs is shown. Point P is one such contact, radial distance r_c from the axis of the input and output discs. The angular alignment of the intermediate discs can be varied in order to vary the speed ratio of the CVT. For this question the rotation axis of the intermediate disc remains perpendicular to the rotation axes of the input and output discs, giving a unity input to output speed ratio. Point B is the centre of profile radius r_d . Point B is at radial distance r_d from the axis of the input and output discs. The contact point P and the centre of the profile radius r_i both lie on a straight line AB. Line AB makes an angle of 60° with the axis of the intermediate disc.

(a) If there is no slip at the contacts show that the angular speed of the input disc equals $\sqrt{3}$ times the angular speed of the intermediate disc and hence determine the spin velocity of the contact in terms of Ω . [25%]

(b) If the contacts are circular show that the fraction of transmitted power lost in all the contacts due to sliding and spinning is given by:

$$\frac{4}{\sqrt{3}} \left(\frac{e}{r_d} + \frac{a I_M}{r_d I_F} \right)$$

where a is the radius of the contact, e is the spin pole offset, I_F is the non-dimensional friction force and I_M is the non-dimensional spin moment, all as defined in the data sheet. [25%]

(c) The designer has specified that $I_F = 0.75$.

(i) For this case show that the fraction of transmitted power lost is approximately $2.7 a / r_d$. [15%]

(ii) Discuss the design conflicts involved in minimising this fraction. [10%]

(d) If the contacts between the discs are circular, find the profile radius r_i of the intermediate disc in terms of r_d . [25%]

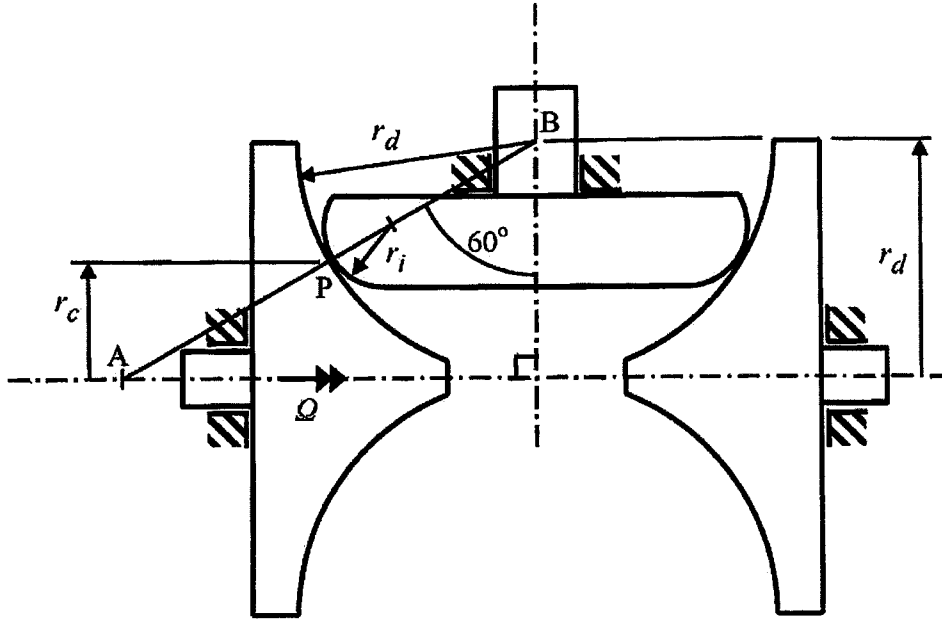


Fig. 1

2 (a) A rotating shaft is to be supported in a stationary housing by rolling-element bearings at each end of the shaft, see Fig. 2. Axial and radial forces are to be applied to the shaft, half way along the shaft.

(i) Explain why the bearing installation must be designed with care to ensure that the predicted life of the bearings is achieved. [10%]

(ii) It has been determined that the shaft can be supported by two cylindrical roller bearings (to support radial forces) and one deep groove ball bearing (to support axial forces). Sketch a suitable conceptual arrangement of the assembly showing the basic shape of the housing and the shaft necessary to accommodate the bearings. Show clearly the interfaces between the bearings, housing and shaft so that it can be seen where forces are transferred and where clearances exist. Do not consider manufacturing or assembly requirements. [20%]

(b) Cylindrical roller bearing NU310EC (see data sheet) has an inner track diameter of 65 mm and 14 rollers of diameter 16 mm and length 19 mm. According to the bearing manufacturer the maximum allowable contact stress under static loading conditions is 4 GPa. The contact modulus E^* is 115 GPa.

(i) Use a Hertz contact stress calculation to estimate the maximum allowable static radial force on the bearing. [40%]

(ii) Compare the force calculated in (i) with the specified static load rating C_0 of bearing NU310EC and suggest reasons for any difference. [10%]

(c) Calculate the allowable radial force on bearing NU310EC for a life of 100,000 revolutions with 10% probability of failure and ideal lubrication conditions. Comment on the value of this force in relation to the static load rating of the bearing. [20%]

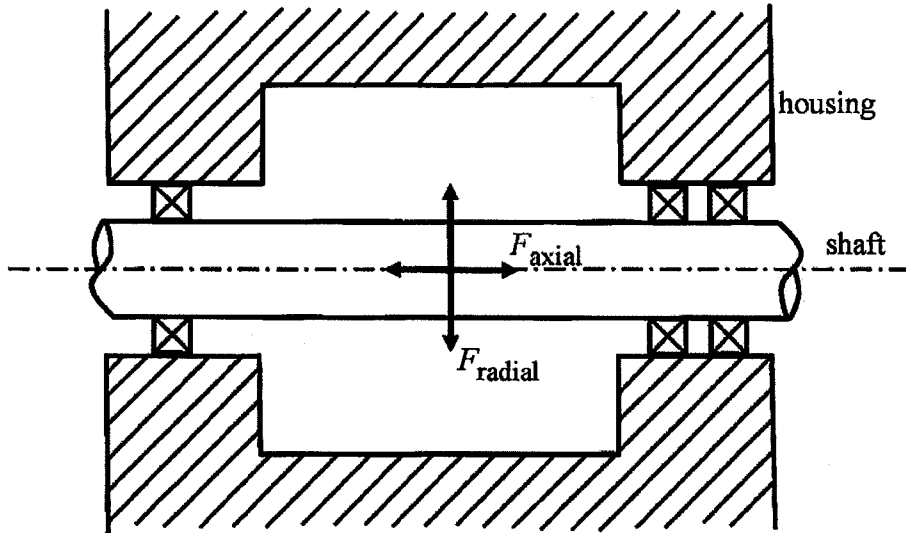


Fig. 2

3 Figure 3 illustrates a gearbox. The sun input shaft rides freely around the carrier input shaft, and both these input shafts and the output shaft run in frictionless bearings in the casing. The input torques on the carrier and sun are T_C and T_S respectively. The torque acting on the output shaft is T_O . Planet gears B and D are rigidly connected to each other and run on a frictionless bearing within the carrier. Tooth numbers for gears A, B, D and E are denoted by their respective letters (A, B, D and E).

(a) Derive the following expression relating the speeds ω_S , ω_C and ω_O of the sun, carrier and output shafts, respectively

$$\omega_O = \alpha\omega_S + (1-\alpha)\omega_C$$

where $\alpha = AD/BE$.

[30%]

(b) Losses in the gearbox can be neglected. For the following two speed conditions find expressions for the output speed, output torque, and power through the sun input as a proportion of the output power, in terms of T_S , ω_S and α :

(i) $\omega_C = 0$;

[25%]

(ii) $\omega_S = 2\omega_C$.

[15%]

(c) The gearbox efficiency is 95%. For the following two speed conditions find expressions for the output torque in terms of T_S and α :

(i) $\omega_C = 0$;

[10%]

(ii) $\omega_S = 2\omega_C$.

[20%]

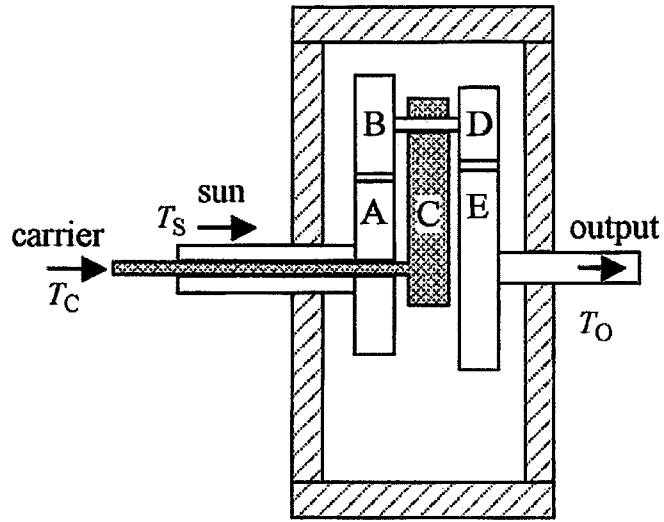


Fig. 3

- 4 A pair of spur gears is to be designed to meet the following specification:
- standard teeth with addendum equal to module and a pressure angle $\phi = 20^\circ$;
 - square pinion with 20 teeth;
 - wheel with 80 teeth;
 - pinion speed 2000 revs per minute;
 - transmitted power of 10 kW;
 - contact modulus $E^* = 115$ GPa;
 - allowable bending and surface stresses $\sigma_b = 400$ MPa and $\sigma_s = 1500$ MPa.

(a) Find the force per unit face-width P' acting along the pressure line in terms of the unknown module m . [25%]

(b) Determine a suitable module m for the gears. State any assumptions that you make. [75%]

END OF PAPER

ENGINEERING TRIPOS Part IIA

Module 3C8 Data Sheet

ELASTIC CONTACT STRESS FORMULAE

Suffixes 1, 2 refer to the two bodies in contact.

Effective curvature $\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$

Contact modulus $\frac{1}{E^*} = \frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2}$

where R_1, R_2 are the radii of curvature of the two bodies (convex positive).

where E_1, E_2 and ν_1, ν_2 are Young's moduli and Poisson's ratios

	<u>Line contact</u> width $2b$; load P' per unit length	<u>Circular contact</u> diameter $2a$; load P
Semi contact width or contact radius	$b = 2 \left\{ \frac{P'R}{\pi E^*} \right\}^{1/2}$	$a = \left\{ \frac{3PR}{4E^*} \right\}^{1/3}$
Maximum contact pressure ('Hertz stress')	$p_0 = \left\{ \frac{P'E^*}{\pi R} \right\}^{1/2}$	$p_0 = \frac{1}{\pi} \left\{ \frac{6PE^{*2}}{R^2} \right\}^{1/3}$
Approach of centres	$\delta = \frac{2P'}{\pi} \left[\frac{1-\nu_1^2}{E_1} \left\{ \ln \left(\frac{4R_1}{b} \right) - \frac{1}{2} \right\} + \frac{1-\nu_2^2}{E_2} \left\{ \ln \left(\frac{4R_2}{b} \right) - \frac{1}{2} \right\} \right]$	$\delta = \frac{a^2}{R} = \frac{1}{2} \left\{ \frac{9 P^2}{2 E^{*2} R} \right\}^{1/3}$
Mean contact pressure	$\bar{p} = \frac{P'}{2b} = \frac{\pi}{4} p_0$	$\bar{p} = \frac{P}{\pi a^2} = \frac{2}{3} p_0$
	$\tau_{\max} = 0.300 p_0$ at $x=0, z=0.79b$	$\tau_{\max} = 0.310 p_0$ at $r=0, z=0.48a$ for $\nu=0.3$
Maximum tensile stress	zero	$\frac{1}{3}(1-2\nu)p_0$ at $r=a, z=0.79b$

Mildly elliptical contacts

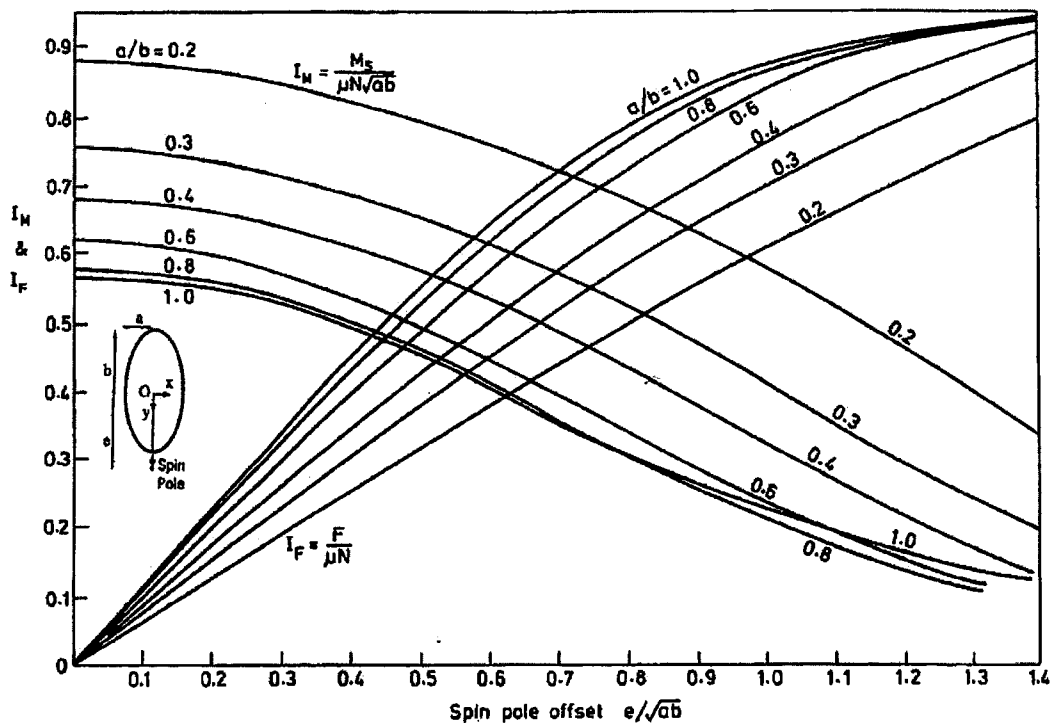
If the gap at zero load is $h = \frac{1}{2}Ax^2 + \frac{1}{2}By^2$ and $0.2 < A/B < 5$ then

ratio of semi-axes $b/a \cong (A/B)^{2/3}$

To calculate the contact area or Hertz stress use the circular contact equations with $R = (AB)^{-1/2}$ or better $R_e = [AB(A+B)/2]^{-1/3}$.

For approach use circular contact equation with $R = (AB)^{-1/2}$ (not R_e)

Hertzian contact frictional losses

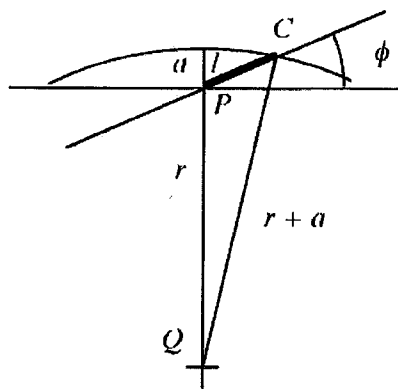


INVOLUTE GEARING

Spur gears

pitch cylinder radii	r	} with suffix 1 or 2	circumferential pitch	$p = 2\pi r/N$
base cylinder radii	r_b		base pitch	$p_b = p \cos \phi$
addendum cylinder radii	r_a		module	$m = p/\pi = 2r/N$
number of teeth	N		ratio of contact	r_c
addendum	$a = r_a - r$		radius of curvature at pitch point	$\rho = r \sin \phi$
pressure angle	ϕ			

Path of contact



$$l = \left\{ r^2 \sin^2 \phi + a(2r + a) \right\}^{1/2} - r \sin \phi$$

For a standard 20° spur wheel with N teeth of module m this becomes

$$\frac{l}{m} = \left(0.02924N^2 + N + 1 \right)^{1/2} - 0.1710N$$

Standard tooth forms

Addendum $a = m$, Dedendum $= \frac{7}{6}m$, pressure angle $= 20^\circ$.

Modules: 0.3 – 1.0 mm in 0.1 mm steps
 1.0 – 4.0 mm in 0.25 mm steps 4.0 – 7.0 mm in 0.5 mm steps
 7.0 – 16.0 mm in 1.0 mm steps 16.0 – 24.0 mm in 2.0 mm steps
 24.0 – 45.0 mm in 3.0 mm steps 45.0 – 75.0 mm in 5.0 mm steps

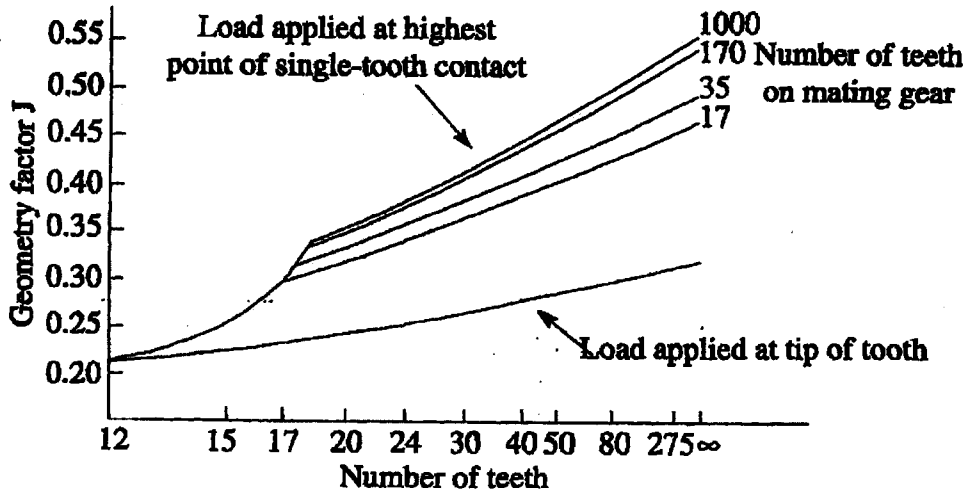
Friction in spur gears

$$\frac{\text{average friction loss}}{\text{power transmitted}} \approx \mu\pi \left\{ \frac{1}{N_1} + \frac{1}{N_2} \right\}$$

Tooth failure

Allowable bending stress σ_b according to AGMA guidelines given by $\sigma_b = \frac{P_T'}{Jm}$

where P_T' is force per unit face-width acting tangentially to pitch circle and J given in the figure below for 20° spur gears. Typical values of σ_b shown in table.



Typical allowable tooth stresses (AGMA)

Material	Condition	Bending fatigue strength σ_b (MPa)	Surface fatigue strength σ_s (MPa)
Steel	Through hardened and tempered	170-390	590-1200
	Carburised and case hardened	380-480	1250-1550
Cast iron	As cast	69-90	450-590
Nodular iron	Quenched, annealed and tempered	150-300	500-800
Malleable iron	Pearlitic	70-145	500-650

EPICYCLIC SPEED RULE

$$\omega_s = (1 + R)\omega_c - R\omega_a \quad \text{where } R = \frac{A}{S}$$

ROLLING ELEMENT BEARINGS

Fatigue life

$$L = a_1 a_2 a_3 (C/P)^p \quad p = 3 \text{ for ball and } 10/3 \text{ for roller bearings}$$

Fatigue probability %	10	5	4	3	2	1
Life adjust factor a_1	1	0.62	0.53	0.44	0.33	0.21

Bearing choice

The information on the following pages concerning loads, viscosities and standard bearing sizes and ratings is extracted from the SKF General Bearing Catalogue and is copied with permission. It is SKF copyright and is not to be further reproduced.

MPFS, DJC, JAW
November 07

Required viscosities and the effect of viscosity ratio on a_{23}

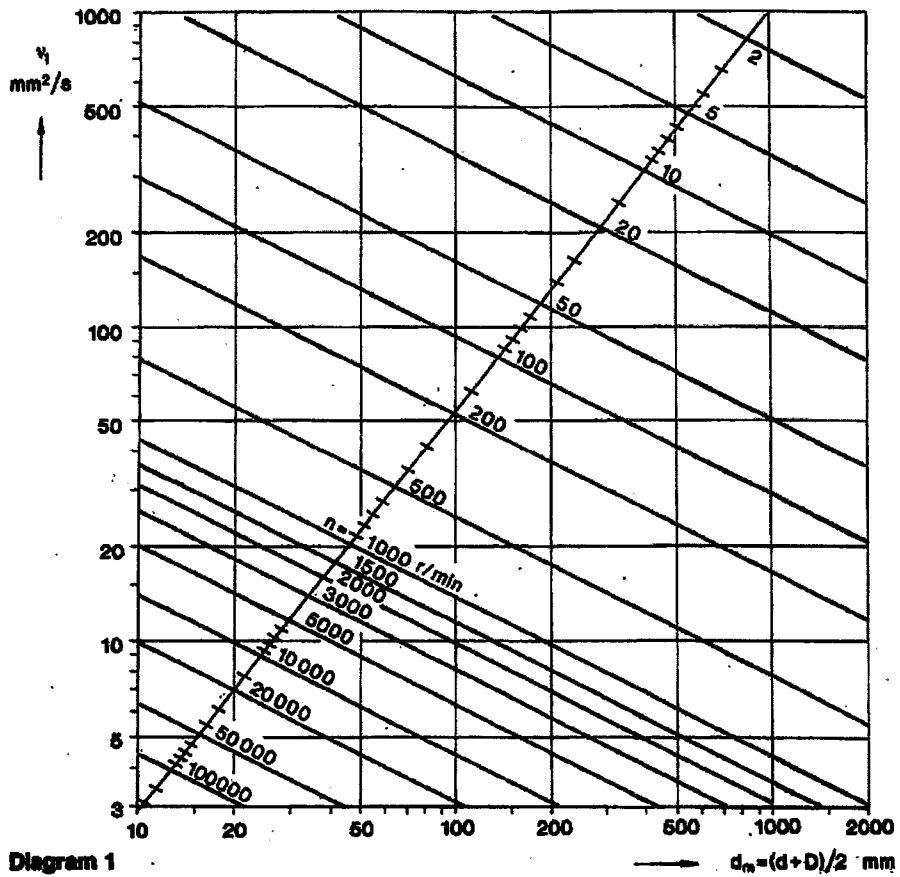


Diagram 1

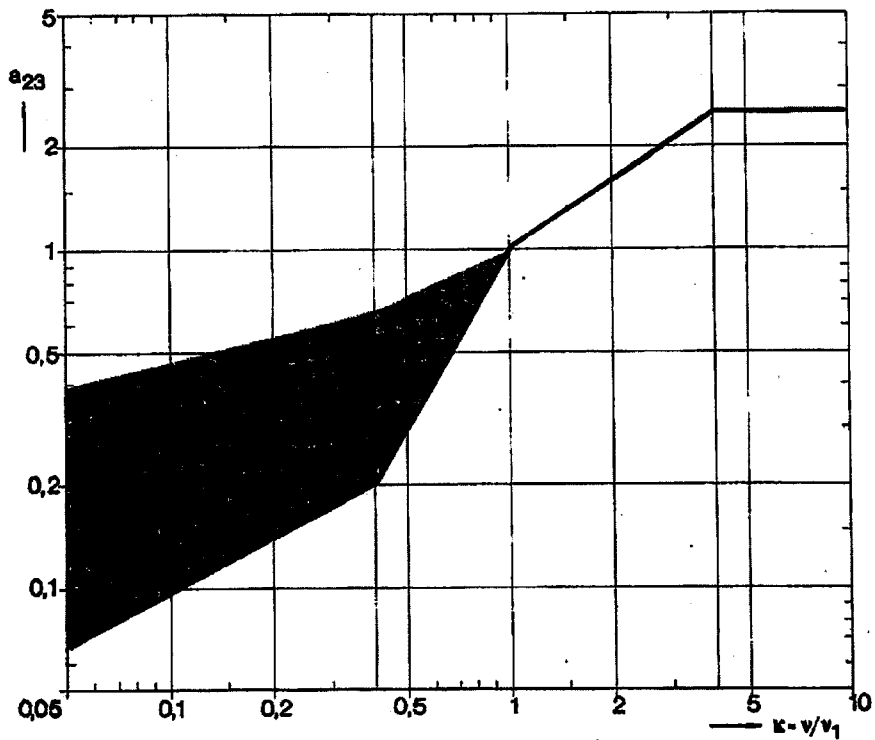
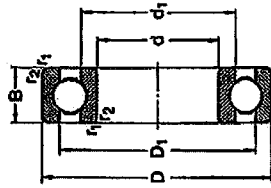
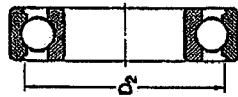


Diagram 3

Deep groove ball bearings
single row
d 35-55 mm



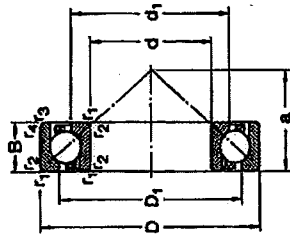
With full outer ring shoulders



With recessed outer ring shoulders

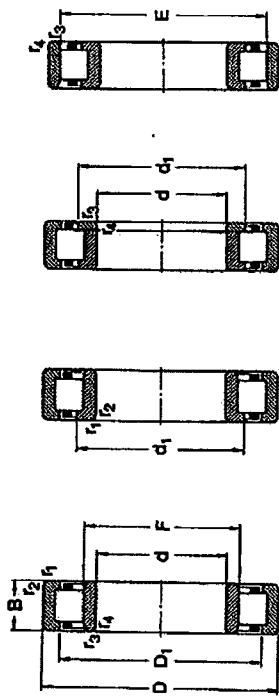
Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation
	d	D	B				
	N			N	r/min	kg	
d	D	B	C	C_0			
35	47	7	4 750	3 200	1 668	0,030	61907
	55	10	9 560	6 200	2 900	0,080	61907
	62	9	12 400	8 150	3 750	0,11	16007
	62	14	15 900	10 200	4 440	0,16	6007
	72	17	25 500	15 300	6 655	0,29	6207
	80	21	39 200	19 000	8 815	0,46	6307
	100	25	55 500	31 000	1 290	0,95	6407
40	52	7	4 940	3 450	1 968	0,034	61908
	62	12	13 800	9 300	4 255	0,12	61908
	68	9	13 900	9 150	4 400	0,13	18008
	68	16	16 800	11 600	4 800	0,19	6008
	80	16	30 700	19 000	8 000	0,32	6308
	80	23	41 000	24 000	1 020	0,53	6308
	110	27	63 700	36 600	1 530	1,25	6408
45	58	7	6 050	4 300	2 288	0,040	61908
	68	12	14 000	9 800	4 655	0,14	61908
	75	16	15 800	10 800	5 200	0,17	18008
	75	18	20 800	14 600	6 400	0,25	6208
	85	18	33 200	21 600	8 155	0,41	6308
	100	25	52 700	31 500	1 340	0,83	6308
	120	29	76 100	45 000	1 900	1,55	6408
50	65	7	6 240	4 750	2 500	0,052	61910
	72	12	14 600	10 400	5 000	0,14	61910
	80	10	16 300	11 400	5 600	0,18	16010
	80	16	21 600	16 000	7 100	0,26	6010
	90	20	35 100	23 200	8 600	0,46	6210
	110	27	61 600	38 000	1 600	1,05	6310
	130	31	87 100	52 000	2 200	1,90	6410
55	72	8	8 840	6 800	3 600	0,083	61911
	80	13	15 900	11 400	5 600	0,19	61911
	90	11	18 500	14 000	6 600	0,26	16011
	90	18	28 100	21 200	9 000	0,39	6011
	100	21	43 600	29 000	1 250	0,91	6211
	120	29	71 500	45 000	1 800	1,35	6311
	140	33	99 500	62 000	2 600	2,30	6411

Angular contact ball bearings
single row
d 10-65 mm



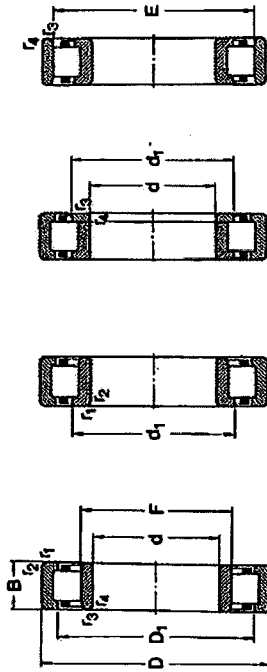
Principal dimensions	Basic load ratings			Fatigue load limit P_u	Speed ratings Lubrication grease oil	Mass	Designation
	d	D	B				
	N			N	r/min	kg	
d	D	B	C	C_0			
10	30	9	7 020	3 350	1 400	0,030	7200 BE
12	32	10	7 610	3 800	1 600	0,036	7201 BE
	32	12	10 600	5 000	2 080	0,060	7301 BE
15	35	11	8 840	4 800	2 040	0,045	7202 BE
	42	13	13 000	6 700	2 680	0,090	7302 BE
17	40	12	11 100	6 100	2 600	0,065	7203 BE
	47	14	15 900	8 300	3 655	0,11	7303 BE
20	47	14	14 000	6 300	3 655	0,11	7304 BE
	52	15	19 000	10 400	4 400	0,14	7304 BE
25	52	15	15 600	10 200	4 300	0,13	7205 BE
	62	17	23 800	15 800	6 655	0,23	7305 BE
30	62	16	23 800	15 800	6 655	0,20	7206 BE
	72	18	34 500	21 200	9 000	0,34	7306 BE
35	72	17	30 700	20 800	8 800	0,28	7207 BE
	80	21	39 000	24 500	1 040	0,45	7307 BE
40	80	18	36 400	26 000	1 100	0,37	7208 BE
	90	23	49 400	33 500	1 400	0,63	7308 BE
45	85	19	37 700	28 000	1 200	0,42	7209 BE
	100	25	60 500	41 500	1 700	0,85	7309 BE
50	90	20	39 000	30 500	1 200	0,47	7210 BE
	110	27	74 100	51 000	2 200	1,10	7310 BE
55	100	21	48 800	38 000	1 630	0,62	7211 BE
	120	29	85 200	60 000	2 550	1,40	7311 BE
60	110	22	57 200	45 500	1 930	0,80	7212 BE
	130	31	95 800	69 500	3 000	1,75	7312 BE
65	120	23	66 900	54 000	2 250	1,00	7213 BE
	140	33	106 000	80 000	3 350	2,15	7313 BE

**Cylindrical roller bearings
single row
d 40-45 mm**



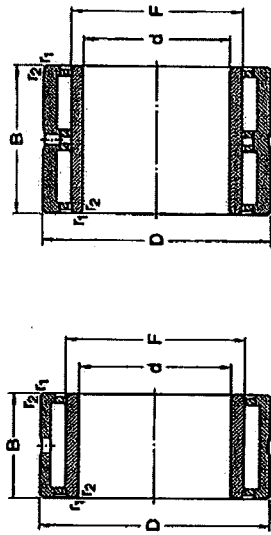
Principal dimensions d D B C	Type NU		Type NUJ		Type NUP		Type N		Designation
	N	C	N	C ₀	N	C	N	Mass	
40	23	80 900	78 000	10 200	6 700	6 000	6 000	0,85	NU 308 EC
50	23	80 900	78 000	10 200	6 700	6 000	6 000	0,67	NJ 308 EC
50	23	80 900	78 000	10 200	6 700	6 000	6 000	0,64	NUP 308 EC
50	33	112 000	120 000	15 300	6 300	7 500	6 300	0,84	NU 2008 EC
50	33	112 000	120 000	15 300	6 300	7 500	6 300	0,96	NJ 2008 EC
50	33	112 000	120 000	15 300	6 300	7 500	6 300	0,98	NUP 2306 EC
110	27	96 800	90 000	11 600	6 000	7 000	6 000	1,30	NU 408
110	27	96 800	90 000	11 600	6 000	7 000	6 000	1,35	NJ 408
110	27	96 800	90 000	11 600	6 000	7 000	6 000	1,35	NUP 408
45	75	44 600	52 000	6 300	9 000	11 000	9 000	0,26	NU-1009 EC
65	19	60 500	64 000	8 150	6 700	8 000	6 700	0,43	NU 208 EC
65	19	60 500	64 000	8 150	6 700	8 000	6 700	0,41	NJ 208 EC
65	19	60 500	64 000	8 150	6 700	8 000	6 700	0,45	NUP 208 EC
65	19	60 500	64 000	8 150	6 700	8 000	6 700	0,45	NUP 209 EC
65	23	73 700	81 500	10 600	6 700	8 000	6 700	0,52	NU 2308 EC
65	23	73 700	81 500	10 600	6 700	8 000	6 700	0,54	NJ 2308 EC
65	23	73 700	81 500	10 600	6 700	8 000	6 700	0,55	NUP 2308 EC
65	23	73 700	81 500	10 600	6 700	8 000	6 700	0,52	N 2309 EC
100	25	89 000	100 000	12 900	6 300	7 500	6 300	0,90	NU 308 EC
100	25	89 000	100 000	12 900	6 300	7 500	6 300	0,92	NJ 308 EC
100	25	89 000	100 000	12 900	6 300	7 500	6 300	0,85	NUP 308 EC
100	25	89 000	100 000	12 900	6 300	7 500	6 300	0,88	N 308 EC
100	36	138 000	153 000	20 000	5 600	6 700	5 600	1,30	NU 2309 EC
100	36	138 000	153 000	20 000	5 600	6 700	5 600	1,30	NJ 2309 EC
100	36	138 000	153 000	20 000	5 600	6 700	5 600	1,35	NUP 2309 EC
120	29	106 000	102 000	13 400	5 600	6 700	5 600	1,65	NJ 409
120	29	106 000	102 000	13 400	5 600	6 700	5 600	1,65	NUP 409
120	29	106 000	102 000	13 400	5 600	6 700	5 600	1,70	N 409

**Cylindrical roller bearings
single row
d 50-55 mm**



Principal dimensions d D B C	Type NU		Type NUJ		Type NUP		Type N		Designation
	N	C	N	C ₀	N	C	N	Mass	
50	16	30 800	34 500	4 000	8 500	10 000	8 500	0,31	NU 1010
50	20	64 400	69 500	8 800	6 300	7 500	6 300	0,48	NU 210 EC
50	20	64 400	69 500	8 800	6 300	7 500	6 300	0,49	NJ 210 EC
50	20	64 400	69 500	8 800	6 300	7 500	6 300	0,51	NUP 210 EC
50	20	64 400	69 500	8 800	6 300	7 500	6 300	0,48	N 210 EC
90	23	78 100	88 000	11 400	6 300	7 500	6 300	0,56	NU 2210 EC
90	23	78 100	88 000	11 400	6 300	7 500	6 300	0,58	NJ 2210 EC
90	23	78 100	88 000	11 400	6 300	7 500	6 300	0,58	NUP 2210 EC
110	27	110 000	112 000	15 000	5 000	6 000	5 000	1,15	NU 310 EC
110	27	110 000	112 000	15 000	5 000	6 000	5 000	1,16	NJ 310 EC
110	27	110 000	112 000	15 000	5 000	6 000	5 000	1,20	NUP 310 EC
110	27	110 000	112 000	15 000	5 000	6 000	5 000	1,15	N 310 EC
110	40	161 000	166 000	24 500	5 000	6 000	5 000	1,70	NU 2310 EC
110	40	161 000	166 000	24 500	5 000	6 000	5 000	1,75	NJ 2310 EC
110	40	161 000	166 000	24 500	5 000	6 000	5 000	1,80	NUP 2310 EC
130	31	130 000	127 000	16 600	5 000	6 000	5 000	2,00	NU 410
130	31	130 000	127 000	16 600	5 000	6 000	5 000	2,05	NJ 410
95	18	57 200	69 500	8 300	7 000	8 500	7 000	0,40	NU 1011 EC
100	21	84 200	95 000	12 200	6 000	7 000	6 000	0,68	NU 211 EC
100	21	84 200	95 000	12 200	6 000	7 000	6 000	0,67	NJ 211 EC
100	21	84 200	95 000	12 200	6 000	7 000	6 000	0,69	NUP 211 EC
100	21	84 200	95 000	12 200	6 000	7 000	6 000	0,66	N 211 EC
100	25	86 000	118 000	15 300	6 000	7 000	6 000	0,79	NU 2211 EC
100	25	86 000	118 000	15 300	6 000	7 000	6 000	0,81	NJ 2211 EC
100	25	86 000	118 000	15 300	6 000	7 000	6 000	0,82	NUP 2211 EC
100	25	86 000	118 000	15 300	6 000	7 000	6 000	0,79	N 2211 EC
120	29	138 000	143 000	18 600	4 800	5 600	4 800	1,45	NU 311 EC
120	29	138 000	143 000	18 600	4 800	5 600	4 800	1,50	NJ 311 EC
120	29	138 000	143 000	18 600	4 800	5 600	4 800	1,55	NUP 311 EC
120	29	138 000	143 000	18 600	4 800	5 600	4 800	1,45	N 311 EC

**Needle roller bearings with flanges
with inner ring
d 40-65 mm**



Series NA 69

Series NK(S), NA 49

Principal dimensions	Basic load ratings				Fatigue load limit P_u	Speed ratings Lubrication greases oil	Mass	Designation
	d	D	B	C				
40	55	20	27 500	57 000	7 200	6 300	9 000	NK1 40/20 NK1 40/30 NA 4909 NA 6908 NK(S) 40
			40 200	83 000	12 000	8 300	9 000	
			42 800	71 000	9 150	5 600	8 000	
			42 800	125 000	16 000	5 600	8 000	
			42 800	72 000	9 150	5 600	8 000	
42	57	20	29 200	61 000	7 850	6 000	8 500	NK1 42/20 NK1 42/30
			41 800	98 000	12 800	6 000	8 500	
45	62	25	38 000	78 000	10 000	5 600	8 000	NK1 45/25 NK1 45/35
			48 500	110 000	14 300	5 600	8 000	
			45 700	78 000	10 000	5 300	7 500	NA 4909
			70 400	137 000	17 300	5 300	7 500	NA 6909
			44 600	78 000	10 000	5 000	7 000	NK(S) 45
50	68	25	40 200	88 000	11 200	5 300	7 500	NK1 50/25 NK1 50/35
			52 300	122 000	16 000	5 300	7 500	
			47 300	85 000	11 000	5 000	7 000	NA 4910
			73 700	150 000	19 000	5 000	7 000	NA 6910
			62 700	104 000	13 700	4 500	6 300	NK(S) 50
55	72	25	41 800	96 500	12 200	4 800	6 700	NK1 55/25 NK1 55/35
			55 000	134 000	17 600	4 800	6 700	
			57 200	106 000	13 700	4 500	6 300	NA 4911
			89 700	180 000	24 000	4 500	6 300	NA 6911
			66 000	114 000	15 000	4 300	6 000	NK(S) 55
60	82	25	44 000	95 000	12 000	4 300	6 000	NK1 60/25 NK1 60/35
			60 500	146 000	19 000	4 300	6 000	
			60 500	114 000	14 600	4 300	6 000	NA 4912
			83 500	204 000	26 000	4 300	6 000	NA 6912
			68 200	120 000	15 600	4 000	5 600	NK(S) 60
65	90	25	61 600	120 000	15 300	4 000	5 600	NA 4913 NK1 65/25 NK1 65/35
			85 700	163 000	21 600	4 000	5 600	
			85 200	212 000	27 000	4 000	5 600	NA 6913
			70 400	132 000	17 000	3 800	5 300	NK(S) 65