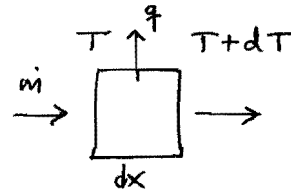
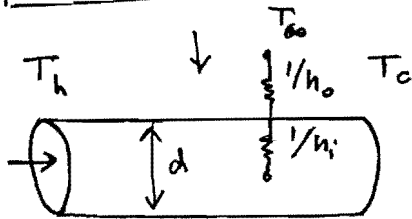


3A6 2013 CRIBS



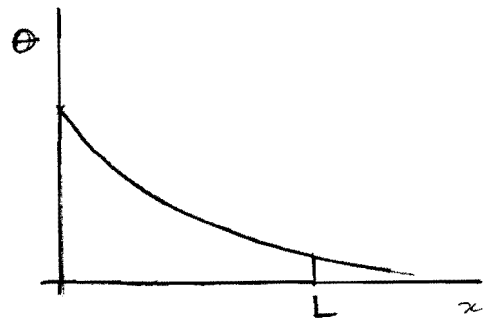
(a) DRY OPERATION

$$\dot{m} c dT = -q \pi d dx = -U \pi d (T - T_{\infty}) dx$$

$$U = \left(\frac{1}{h_o} + \frac{1}{h_i} \right)^{-1}$$

$$\frac{dT}{T - T_{\infty}} = -\frac{U \pi d}{\dot{m} c} dx$$

$$\ln \frac{(T - T_{\infty})}{(T_h - T_{\infty})} = -\frac{U \pi d}{\dot{m} c} x$$



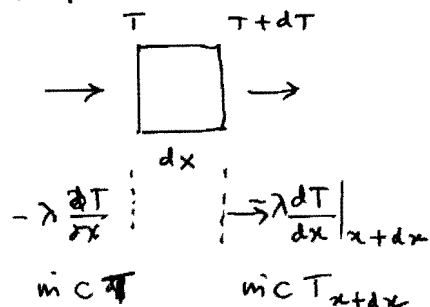
$$\theta = \frac{(T_c - T_{\infty})}{(T_h - T_{\infty})} = \exp \left(-\frac{U \pi d L}{\dot{m} c} \right)$$

$$\dot{Q}_A = \dot{m} c (T_h - T_c) = \dot{m} c \left[(T_h - T_{\infty}) - (T_c - T_{\infty}) \right]$$

$$= \dot{m} c (T_h - T_{\infty}) \left[1 - \exp \left(-\frac{U \pi d L}{\dot{m} c} \right) \right]$$

$$= \dot{m} c (T_h - T_{\infty}) \left[1 - \exp \left(-\frac{\pi d L}{\dot{m} c} \frac{1}{\frac{1}{h_o} + \frac{1}{h_i}} \right) \right] //$$

NOTE : A COMMON MISTAKE WAS TO TAKE AN ENERGY BALANCE WITH CONDUCTION ALONG THE x-DIRECTION :



$$\dot{m} c \frac{dT}{dx} + \lambda \frac{d^2 T}{dx^2} = \frac{dq}{dx}$$

$$\dot{m} c \frac{\Delta T}{L} \quad \lambda \frac{\Delta T}{L^2}$$

CONVECTION DOMINANT ALONG X : $\dot{m} c \gg \frac{\lambda}{L}$ OR $\frac{\alpha}{UL} \ll 1$

(b) WET CONDITIONS

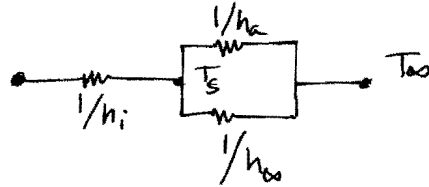
(i) $G_v = h_m (p_{v,s} - p_{v,\infty})$

$$\frac{h_{md}}{\rho} = \frac{h_a d}{\lambda_a} \rightarrow h_m = h_a \frac{\rho}{\lambda_a}$$

$$G_v = \frac{h_a \rho}{\lambda_a} (p_{v,s} - p_{v,\infty}) = \frac{h_a \rho}{\lambda_a} \beta (T_s - T_{\infty})$$

$$q_v = G_v h_{ev} = \frac{h_a \rho}{\lambda_a} h_{ev} \beta (T_s - T_{\infty})$$

(ii) TWO PATHWAYS FOR HEAT TRANSFER: DIRECT AND EVAPORATION



$$h_v = \frac{q_v}{(T_s - T_{\infty})} = \frac{h_a \rho}{\lambda_a} h_{ev} \beta$$

$$R_B = \frac{1/h_a \ 1/h_v}{1/h_a + 1/h_v} + \frac{1}{h_i} = \frac{1}{h_a + h_v} + \frac{1}{h_i}$$

$$U_B = \frac{1}{R_B} = \frac{1}{\frac{1}{h_a + h_v} + \frac{1}{h_i}} = \left[\frac{1}{h_a \left(1 + \frac{\rho h_{ev} \beta}{\lambda_a} \right)} + \frac{1}{h_i} \right]^{-1}$$

USING THE SAME ANALYSIS AS IN (a):

$$\dot{Q}_B = m_i c (T_h - T_c) = m_i c (T_b - T_{\infty}) \left[1 - \exp \left(-U_B \frac{\pi d L}{m_i c} \right) \right]$$

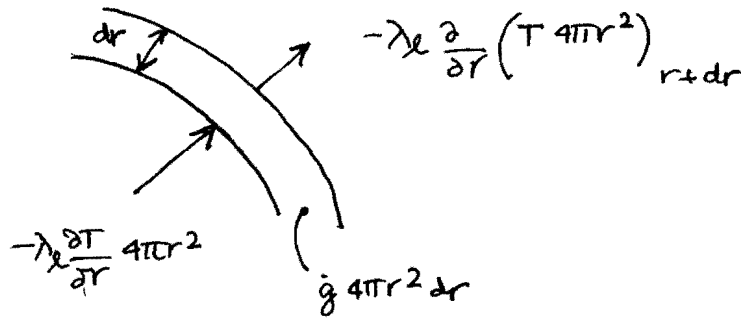
THE EVAPORATION CREATES A NEW PATH FOR HEAT TRANSFER, NOW LIMITED BY THE RATE OF MASS TRANSFER.

THE SIMPLE FINAL ANSWER IS ONLY POSSIBLE BECAUSE OF THE ASSUMPTION REGARDING THE RELATIONSHIP OF PARALLEL DISSIPATIVES AND TEMPERATURE. IN GENERAL, THE TWO WOULD BE COUPLED NON-LINEARLY.

②

(a) SPHERICAL SHELL : dr

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ENERGY CONSERVATION:

$$\rho c (4\pi r^2 dr) \frac{\partial T}{\partial t} = -\lambda_e \frac{\partial T}{\partial r} 4\pi r^2 + \lambda_e \left(\frac{\partial T}{\partial r} 4\pi r^2 + \frac{\partial}{\partial r} \left(\frac{\partial T}{\partial r} 4\pi r^2 \right) dr \right) + \dot{q} 4\pi r^2 dr$$

CANCELLING OUT TERMS AND DIVIDING BY $4\pi r^2$, WE HAVE

$$\rho c \frac{\partial T}{\partial t} dr = -\lambda_e \frac{\partial T}{\partial r} + \lambda_e \frac{\partial T}{\partial r} + \lambda_e \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) dr + \dot{q} dr$$

$$\left[\rho c \frac{\partial T}{\partial t} - \lambda_e \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) = \dot{q} \right]$$

QED

(b) NEGLECTING THE UNSTEADY TERM, WE HAVE

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) = -\frac{\dot{q}}{\lambda_e}$$

$$r^2 \frac{\partial T}{\partial r} = -\frac{\dot{q}}{\lambda_e} r^3 + C_1$$

$$\frac{\partial T}{\partial r} = -\frac{\dot{q}}{\lambda_e} \frac{r}{3} + \frac{C_1}{r^2}$$

$$T = -\frac{\dot{q}}{\lambda_e} \frac{r^2}{6} - \frac{C_2}{6} + C_2$$

FROM SYMMETRY: $\frac{\partial T}{\partial r} \Big|_{r=0} = 0 \rightarrow C_1 = 0$

$$T(R) = T_s = -\frac{\dot{q} R^2}{\lambda_e 6} + C_2 \rightarrow C_2 = T_s + \frac{\dot{q} R^2}{6 \lambda_e}$$

$$\boxed{T(r) = T_s + \frac{\dot{q}}{6\lambda_e} (R^2 - r^2)} \quad \perp \quad \text{QED}$$

(c) FOR AIR, WE HAVE THE SAME EQUATION FOR CONDUCTION, WITH $\dot{q} = 0$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) = 0$$

$$r^2 \frac{\partial T}{\partial r} = D_1$$

$$\frac{\partial T}{\partial r} = \frac{D_1}{r^2}$$

$$T = -\frac{D_1}{r} + D_2$$

$$T(R) = -\frac{D_1}{R} + D_2 = T_s$$

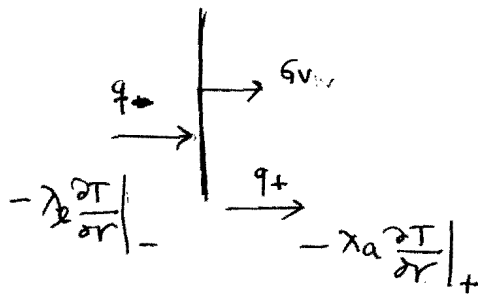
$$T(\infty) = D_2 = T_\infty$$

$$\left. \begin{array}{l} T(R) = -\frac{D_1}{R} + D_2 = T_s \\ T(\infty) = D_2 = T_\infty \end{array} \right\} \rightarrow D_1 = (T_\infty - T_s) R$$

$$\boxed{T(r) = T_\infty + (T_s - T_\infty) \frac{R}{r}}$$

(d)

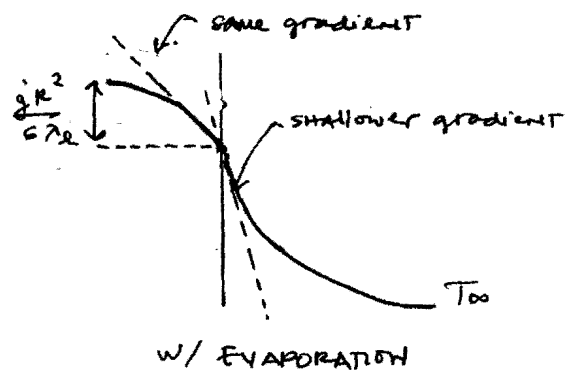
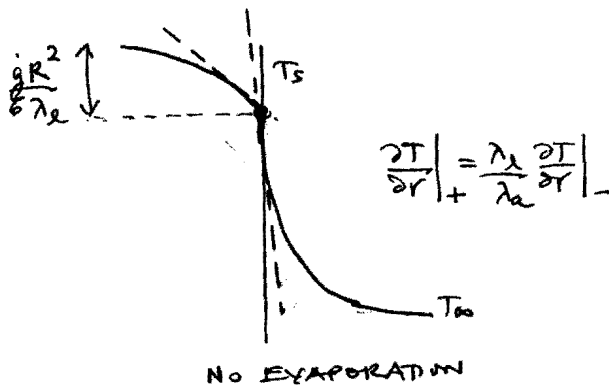
(i)



$$-\lambda_e \left. \frac{\partial T}{\partial r} \right|_- + \lambda_a \left. \frac{\partial T}{\partial r} \right|_+ - \dot{q}_v h_{ev} = 0$$

• NOTE THAT \dot{q} DOES NOT APPEAR EXPLICITLY, AS $dV \rightarrow 0$

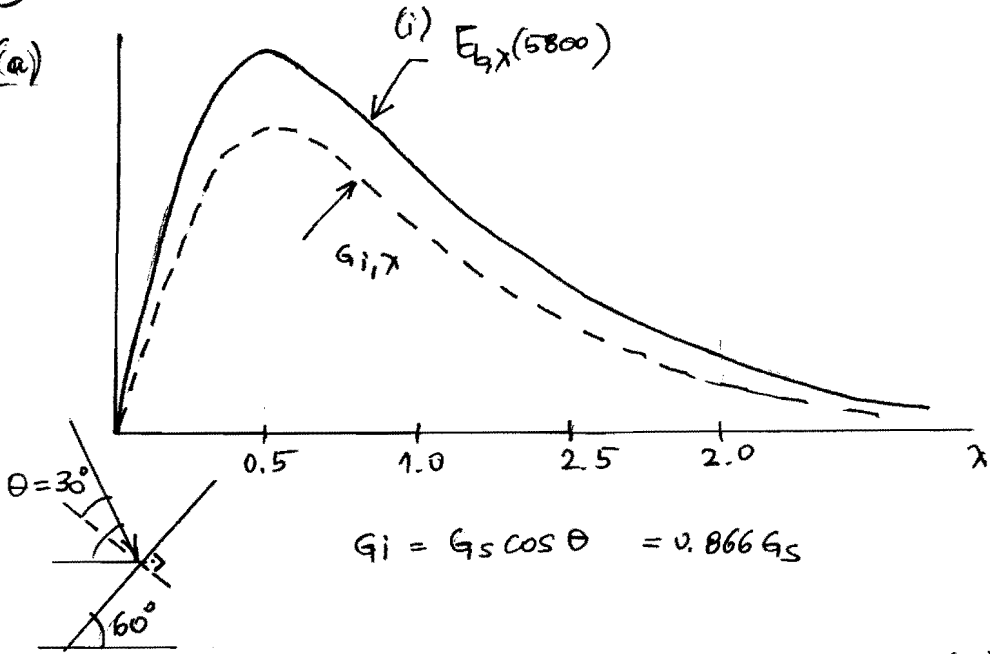
(ii) $\dot{q}_v = 0$: $\lambda_e \left. \frac{\partial T}{\partial r} \right|_- = \lambda_a \left. \frac{\partial T}{\partial r} \right|_+$; $\dot{q}_v > 0$: $\lambda_a \left. \frac{\partial T}{\partial r} \right|_+ - \lambda_e \left. \frac{\partial T}{\partial r} \right|_- = \dot{q}_v h_{ev}$



BONUS: SHOW THAT $T_s = T_\infty + \frac{\dot{q}_v R^2}{3\lambda_e} - \dot{q}_v h_{ev}$

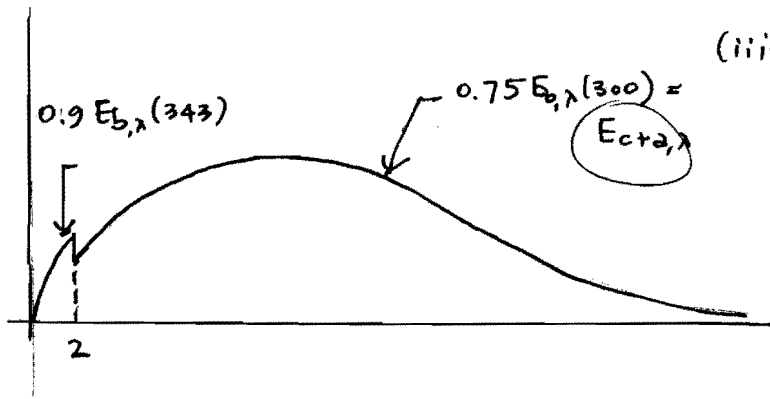
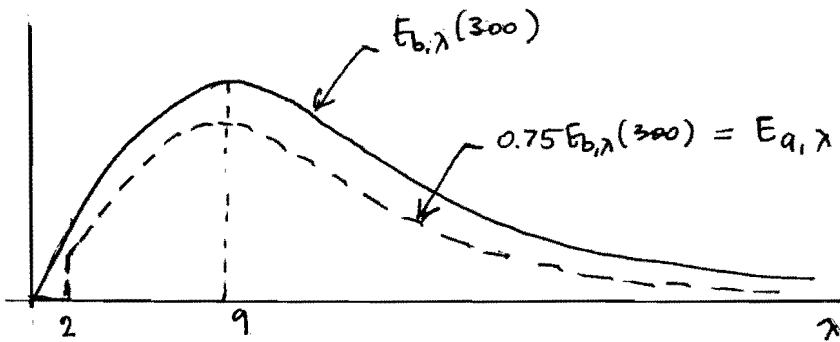
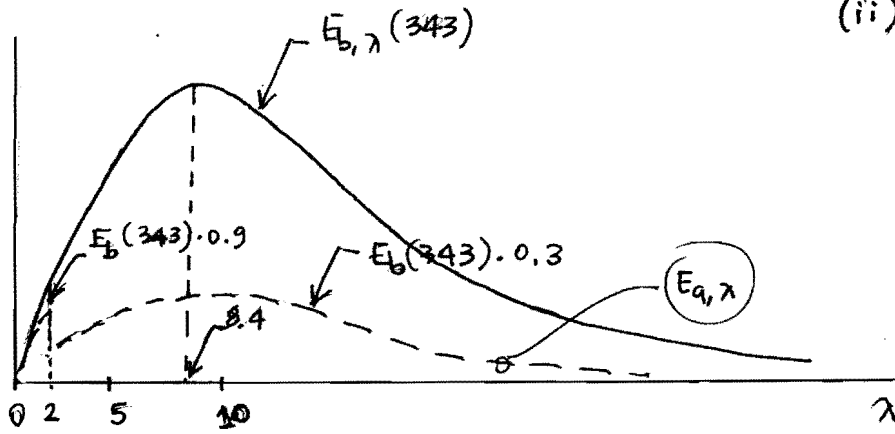
③

(a)



$$G_i = G_s \cos \theta = 0.866 G_s$$

(ii)



(iii) THE ABSORBER COATING IS TRANSPARENT TO THE SHORT WAVELENGTHS OF SUNLIGHT, BUT OPAQUE TO THE LONGER WAVELENGTHS EMITTED BY THE ABSORBER, THUS TRAPPING RADIATIVE POWER.

(b) THE GROSS SOLAR ENERGY ABSORBED IS:

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$$G_a = \int_0^{\infty} \phi_{i,\lambda} \alpha d\lambda = [0.9 F(0-2\mu\text{m})] G_s \cos \theta$$

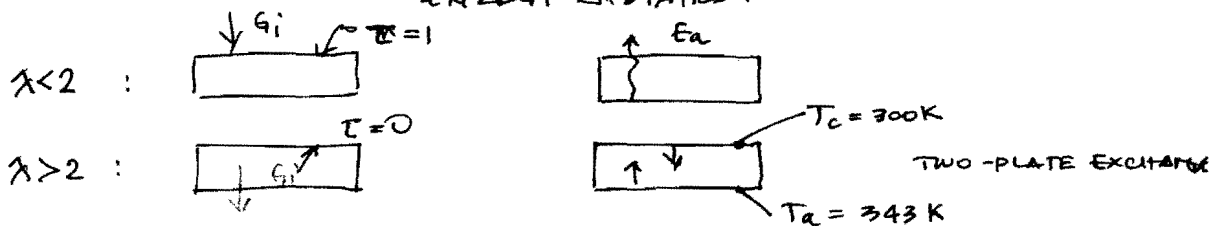
$$\lambda T = (2\mu\text{m})(5800\text{K}) = 11600 \mu\text{mK}$$

$$\text{INTERPOLATION: } F_{0-\lambda} = 0.939959 + (0.945028 - 0.939959) \cdot 100/500 \\ = 0.9409868$$

$$\phi_a = [(0.9)(0.9409868)] (900 \text{ W/m}^2) \cos 30^\circ$$

$$G_a = 660 \text{ W/m}^2$$

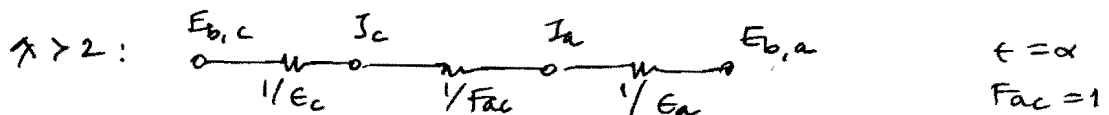
(c) NET FLUX ABSORBED = GROSS ENERGY ABSORBED - ENERGY RADIATED.



$$\lambda < 2: E_a = \int_0^2 \alpha_{a,\lambda} E_{a,\lambda} d\lambda = (0.9) F_{0-2} E_{b,a}$$

$$\lambda T = (2\mu\text{m})(343\text{K}) = 686 \mu\text{mK} \rightarrow F_{0-2} \approx 0$$

$$E_a = 0$$



$$\text{NET RADIATIVE LOSS: } q_L = \frac{E_{b,a} - E_{b,c}}{1/\alpha_c + 1/\alpha_a + 1}$$

$$q_L = \frac{\sigma (T_a^4 - T_c^4)}{1/\alpha_c + 1/\alpha_a + 1} = \frac{5.670 \times 10^{-8} \text{ W/m}^2 \text{K}^4 (343^4 - 300^4) \text{ K}^4}{1/0.5 + 1/0.75 + 1} \\ q_L = 64 \text{ W/m}^2$$

$$\eta = 1 - 64/660 = 0.903 \rightarrow \text{NET EFFICIENCY NET TO COATING.}$$

④ (a) (i) $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$

$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2}$

DEFINE $\theta = \frac{(T - T_s)}{(T_\infty - T_s)}$

$u \frac{\partial \theta}{\partial x} + v \frac{\partial \theta}{\partial y} = \alpha \frac{\partial^2 \theta}{\partial y^2}$

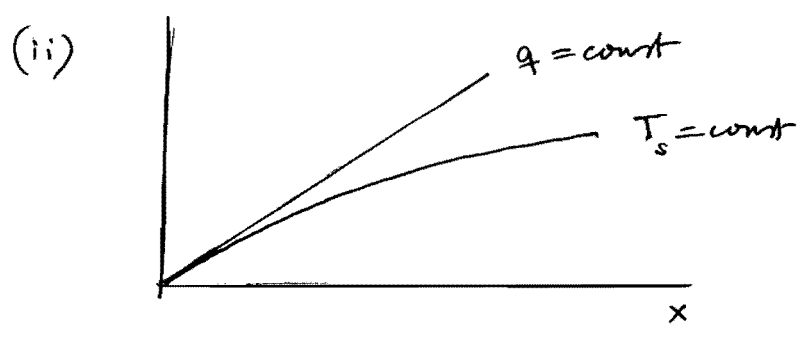
$\frac{\partial}{\partial x} (u\theta) - \theta \frac{\partial u}{\partial x} + \frac{\partial}{\partial y} (v\theta) - \theta \frac{\partial v}{\partial y} = \alpha \frac{\partial^2 \theta}{\partial y^2}$
 ↑ $= 0$ (cont.) ↑

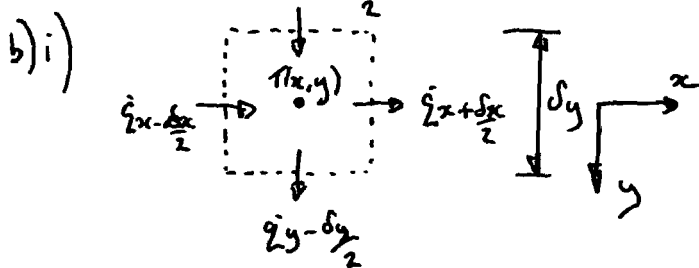
$\frac{\partial}{\partial x} (u\theta) + \frac{\partial}{\partial y} (v\theta) = \alpha \frac{\partial^2 \theta}{\partial y^2}$

$\int_0^\delta \frac{\partial}{\partial x} (u\theta) dy + \left. v\theta \right|_0^\delta = \alpha \left[\left. \frac{\partial \theta}{\partial y} \right|_\delta - \left. \frac{\partial \theta}{\partial y} \right|_0 \right]$

$\frac{\partial}{\partial x} \int_0^\delta u\theta dy = -\frac{\lambda}{\rho c_p} \frac{1}{(T_\infty - T_s)} \left. \frac{\partial T}{\partial y} \right|_0 = \frac{q}{\rho c_p (T_\infty - T_s)}$
 ↙ $\frac{h}{\rho c_p} \frac{u_\infty}{\delta \rightarrow \infty}$

$\frac{d\delta\theta}{dx} = \frac{2}{\lambda} \int_0^\delta \frac{u(T - T_s)}{u_\infty(T_\infty - T_s)} dy = \frac{h}{\rho c_p u_\infty} \quad \text{Q.E.D}$





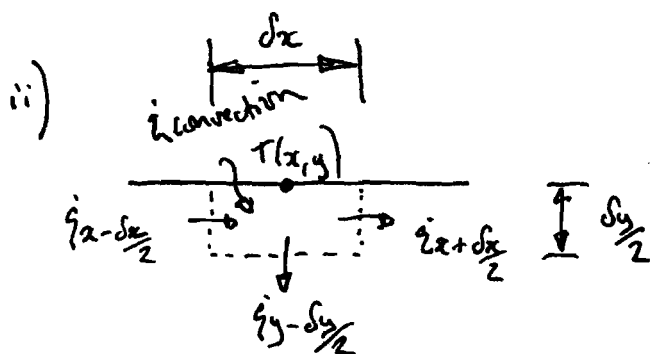
Energy balance: $q_{x-\frac{\delta x}{2}} - q_{x+\frac{\delta x}{2}} + q_{y+\frac{\delta y}{2}} - q_{y-\frac{\delta y}{2}} = 0$

$$-\lambda \frac{\partial T}{\partial x} \Big|_{x-\frac{\delta x}{2}} \delta y - \left(-\lambda \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta x}{2}} \delta y \right) + \lambda \frac{\partial T}{\partial y} \Big|_{y+\frac{\delta y}{2}} \delta x - \left(\lambda \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta y}{2}} \delta x \right) = 0$$

$$-\frac{\partial T}{\partial x} \Big|_{x-\frac{\delta x}{2}} \delta y + \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta x}{2}} \delta y - \frac{\partial T}{\partial y} \Big|_{y+\frac{\delta y}{2}} \delta x + \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta y}{2}} \delta x = 0$$

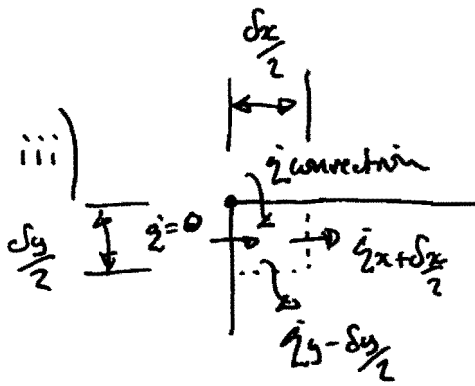
we get

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$



Energy balance: $-\lambda \frac{\partial T}{\partial x} \Big|_{x-\frac{\delta x}{2}} \frac{\delta y}{2} - \left[-\lambda \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta x}{2}} \frac{\delta y}{2} \right] - \left(\lambda \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta y}{2}} \delta x \right) + \frac{h \delta x (T_{\infty} - T_s)}{1} = 0$

$$-\left[\frac{\partial T}{\partial x} \Big|_{x-\frac{\delta x}{2}} - \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta x}{2}} \right] \frac{\delta y}{2} + \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta y}{2}} \delta x + \frac{h \delta x (T_{\infty} - T_s)}{\lambda} = 0$$



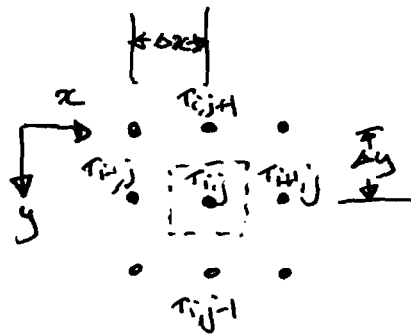
$$0 - \left(-\lambda \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta_x}{2}} \right) - \left(-\lambda \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta_y}{2}} \right) + \frac{h \delta_x}{2l} (T_{\infty} - T) =$$

$$\frac{\delta_y}{2} \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta_x}{2}} + \frac{\delta_x}{2} \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta_y}{2}} + \frac{h \delta_x}{2l} (T_{\infty} - T) = 0$$

$$\delta_y \frac{\partial T}{\partial x} \Big|_{x+\frac{\delta_x}{2}} + \delta_x \frac{\partial T}{\partial y} \Big|_{y-\frac{\delta_y}{2}} + \frac{h \delta_x}{l} (T_{\infty} - T) = 0$$

~~1/2~~

$$c) \quad \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$

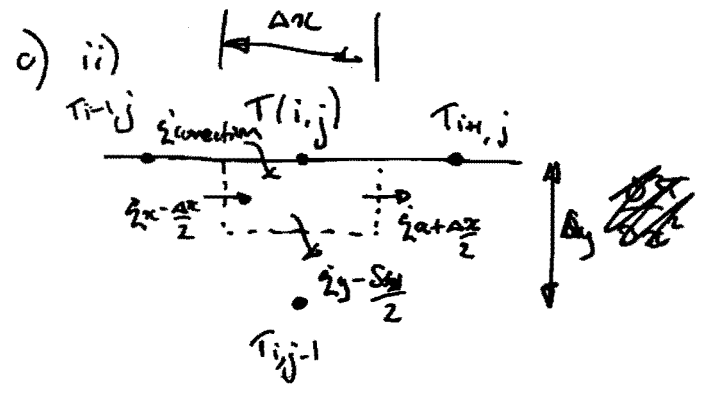


$$\begin{aligned}
 i) \quad \frac{\partial^2 T}{\partial x^2} \Big|_x &\approx \frac{\frac{\partial T}{\partial x} \Big|_{x+\frac{\Delta x}{2}} - \frac{\partial T}{\partial x} \Big|_{x-\frac{\Delta x}{2}}}{\Delta x} \\
 &\approx \frac{\frac{T_{i,j} - T_{i-1,j}}{\Delta x} - (T_{i+1,j} - T_{i,j})}{\Delta x} \\
 &\approx \frac{2T_{i,j} - T_{i-1,j} - T_{i+1,j}}{\Delta x^2}
 \end{aligned}$$

$$\text{similarly } \frac{\partial^2 T}{\partial y^2} \Big|_y \approx \frac{2T_{i,j} - T_{i,j-1} - T_{i,j+1}}{\Delta y^2}$$

$$\Rightarrow 2T_{i,j} - T_{i-1,j} - T_{i+1,j} - T_{i,j-1} - T_{i,j+1} = 0$$

$$\Rightarrow T_{i-1,j} + T_{i+1,j} + T_{i,j-1} + T_{i,j+1} - 4T_{i,j} = 0$$



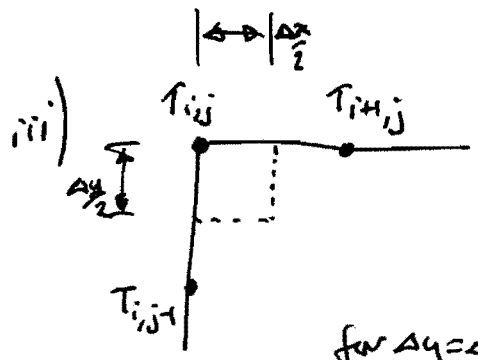
from part b) ii)
$$-\left[\frac{(T_{i,j} - T_{i-1,j})}{\Delta x} - \frac{(T_{i+1,j} - T_{i,j})}{\Delta x} \right] \frac{\Delta y}{2} + \frac{(T_{i,j-1} - T_{i,j}) \Delta x}{\Delta y} + \frac{h \Delta x (T_\infty - T_{i,j})}{1} = 0$$

$$\Rightarrow [-2T_{i,j} + T_{i-1,j} + T_{i+1,j}] \frac{\Delta y}{\Delta x} + 2(T_{i,j-1} - T_{i,j}) \frac{\Delta x}{\Delta y} + \frac{2h \Delta x}{1} (T_\infty - T_{i,j}) = 0$$

for $\Delta x = \Delta y$

$$\Rightarrow -2T_{i,j} + T_{i-1,j} + T_{i+1,j} + 2T_{i,j-1} + \frac{2h \Delta x}{1} T_\infty - \frac{2h \Delta x}{1} T_{i,j} = 0$$

$$T_{i-1,j} + T_{i+1,j} + 2T_{i,j-1} - 2\left(2 + \frac{h \Delta x}{1}\right) T_{i,j} + \frac{2h \Delta x}{1} T_\infty = 0$$



$$\Delta y \frac{(T_{i+1,j} - T_{i,j})}{\Delta x} + \Delta x \frac{(T_{i,j-1} - T_{i,j})}{\Delta y} + \frac{h \Delta x}{1} (T_\infty - T_{i,j}) = 0$$

for $\Delta y = \Delta x$

$$T_{i+1,j} - 2T_{i,j} + T_{i,j-1} + \frac{h \Delta x}{1} T_\infty - \frac{h \Delta x}{1} T_{i,j} = 0$$

$$T_{i+1,j} + T_{i,j-1} - 2\left(1 + \frac{h \Delta x}{2}\right) T_{i,j} + \frac{h \Delta x}{1} T_\infty = 0$$

Set up T_b as a variable in iterative scheme, when RADIATION PRESENT.