

ENGINEERING TRIPOS PART IIA

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Friday 26 April 2013 2 to 3.30

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Module 3C8

MACHINE DESIGN

*Answer not more than **three** questions.*

*All questions carry the same number of marks.*

*The **approximate** percentage of marks allocated to each part of a question is indicated in the right margin.*

*Attachments:*

*Module 3C8 data sheet (9 pages)*

STATIONERY REQUIREMENTS

Single-sided script paper

SPECIAL REQUIREMENTS

Engineering Data Book

CUED approved calculator allowed

**You may not start to read the questions printed on the subsequent pages of this question paper until instructed that you may do so by the Invigilator**

1 The output characteristic of a bicycle rider working at constant effort is shown in Fig. 1(a), where the mean torque  $T_c$  measured at the crank depends linearly on the angular speed of the crank  $\omega_c$ . The intercepts on the axes are  $T_0$  and  $\omega_0$ . The bicycle and rider have combined mass  $m$ , and the wheel radius is  $r$ . The bicycle and rider travel at steady forward speed  $V$  up a slope of small angle  $\alpha$ , as shown in Fig. 1(b). The only resistance to steady motion is the component of weight acting down the slope.

(a) Explain why maximum output power occurs when  $\omega_c = \omega_0 / 2$ . If the fixed ratio of crank speed  $\omega_c$  to wheel speed  $\omega_a$  is  $G = \omega_c / \omega_a$ , show that the ratio  $G$  that maximises the speed  $V$  of the bicycle is given by

$$G = \frac{2mg\alpha r}{T_0}. \quad [30\%]$$

(b) The fixed speed ratio is replaced by an epicyclic gear and an electric motor/generator to provide a variable speed ratio, as shown in Fig. 1(c). The bicycle wheel is connected directly to the annulus, the motor/generator is connected to the sun, and the crank is connected to the planet carrier. The ratio of annulus to sun teeth is  $R$ . The torques acting on the annulus, sun and carrier are denoted  $T_a$ ,  $T_s$  and  $T_c$ , and the corresponding speeds are  $\omega_a$ ,  $\omega_s$  and  $\omega_c$ ; torques and speeds are positive in the same direction.

(i) The carrier (crank) speed  $\omega_c$  is constant and positive. Sketch on one graph the speeds of the annulus  $\omega_a$ , sun  $\omega_s$  and carrier  $\omega_c$  against bicycle speed  $V$ . [20%]

(ii) The carrier (crank) torque  $T_c$  is constant and positive. Derive expressions for  $T_a$  and  $T_s$  in terms of  $T_c$  and  $R$  and sketch on one graph the torques on the annulus  $T_a$ , sun  $T_s$  and carrier  $T_c$  against bicycle speed  $V$ . [25%]

(iii) For the speeds in (i) and torques in (ii) sketch on one graph the power *into* the annulus, sun, and carrier against bicycle speed  $V$ . Find the range of bicycle speeds over which the motor/generator generates electrical power, in terms of  $\omega_c$ ,  $r$  and  $R$ . [25%]

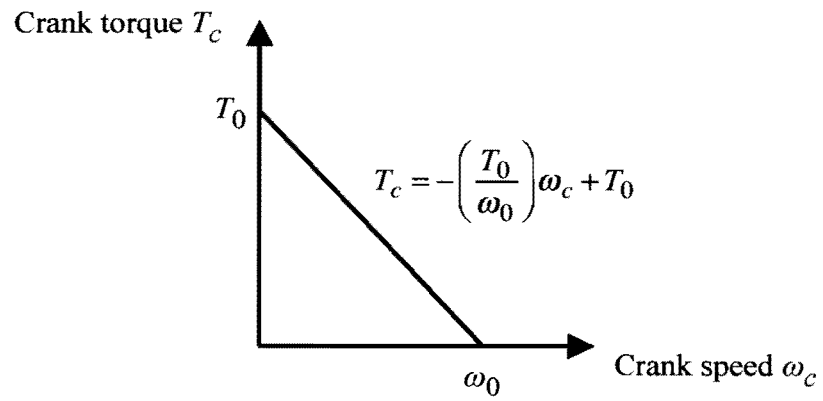


Fig. 1(a)

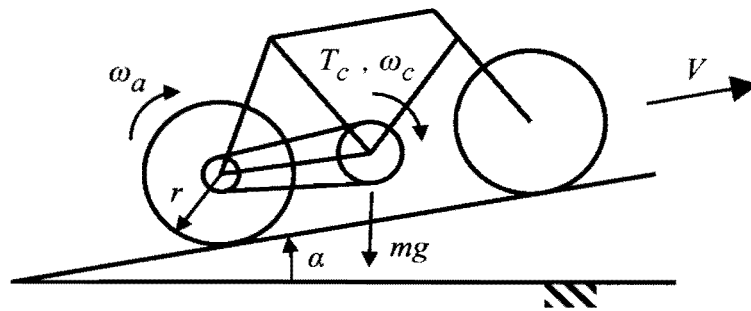


Fig. 1(b)

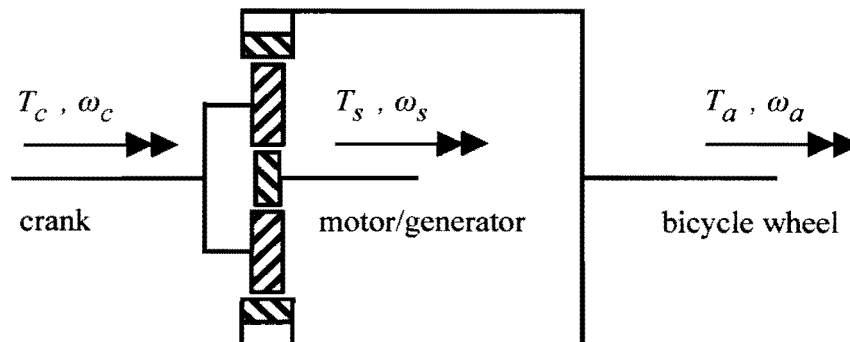


Fig. 1(c)

2 A rigid substrate is covered with a layer of foam material of thickness  $h$ . The foam is indented to a depth  $\delta$  by a rigid sphere of radius  $R$  through the application of the normal force  $P$  as shown in Fig. 2. The deformation is elastic but the foam is compressible so that the deformation is restricted to the volume of material immediately below the contact patch which is of radius  $a$ .

(a) The foam layer can be modelled as a set of independent springs which provide an effective material modulus  $E$ . If  $a \ll R$ , so that the shape of the indenter can be taken to be such that  $\delta = a^2/2R$ , show that the pressure distribution  $p(r)$  between the sphere and the foam can be expressed as

$$p(r) \approx \frac{E}{2Rh} (a^2 - r^2). \quad [30\%]$$

(b) Hence, or otherwise, obtain an expression relating the normal load  $P$  on the sphere to the parameters  $E$ ,  $a$ ,  $h$  and  $R$ . [20%]

(c) The deformation can be expressed non-dimensionally as  $\delta/R$ . Derive an expression which relates  $\delta/R$  to the normalized layer thickness  $h/R$  and the load factor  $P/ER^2$ . [25%]

(d) Discuss the way in which this deformation differs from that normally described as Hertzian. [25%]

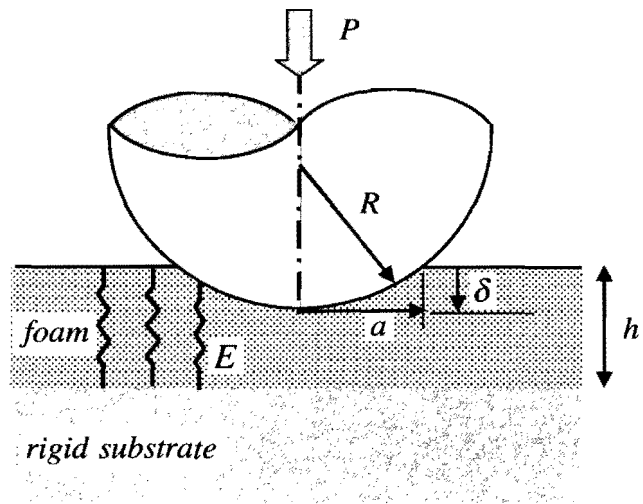


Fig. 2

3 Figure 3 shows a gearbox shaft supported by two identical taper roller bearings (numbered 1 and 2) mounted in a back-to-back arrangement. Axial preload of the bearings is provided by a spring pressing against the outer track of bearing 2. The stiffness of the spring is very much less than the compressive axial stiffness of the bearings. External axial force  $P_a$  and radial force  $P_r$  may be applied at the left hand end of the shaft.

(a) State the advantages and disadvantages of using a preloaded bearing arrangement. [15%]

(b) The axial force  $P_a$  can vary between +10 kN and -5 kN. The radial force  $P_r$  is zero. Use a graphical solution method, or otherwise, to determine the minimum axial preload force required to prevent loss of contact in the bearings. [25%]

(c) The axial force  $P_a$  is removed and a radial force  $P_r = 20$  kN is applied to the shaft.

(i) Calculate the radial forces applied to each bearing and calculate the corresponding minimum axial force on each bearing required to prevent loss of contact. Note that for an individual bearing the minimum axial force  $F_a$  required in the presence of a radial force  $F_r$  is given by  $F_a = 0.5 F_r / Y$  where  $Y = 1.7$ . [25%]

(ii) Using the result from (i), calculate the preload force necessary to prevent loss of contact if the axial force  $P_a$  in the range +10 kN and -5 kN is now applied to the shaft, in addition to the radial force  $P_r = 20$  kN. [25%]

(d) Explain why low stiffness springs are not usually used to provide preload in gearboxes. [10%]

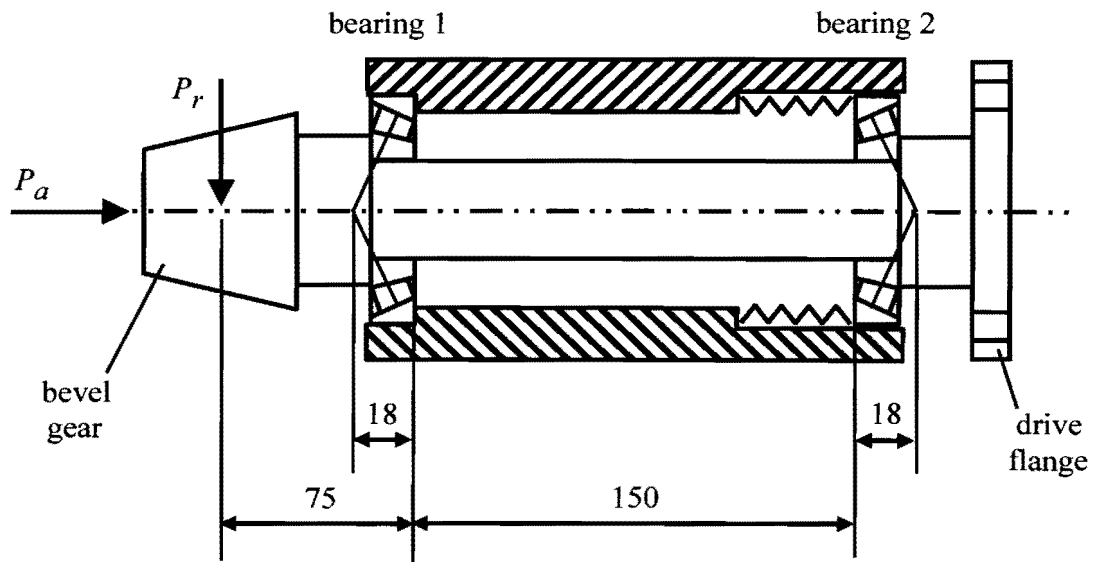


Fig. 3 (dimensions in mm)

FINAL version

(TURN OVER

4 (a) Briefly describe three modes of gear tooth failure. State how the manufacturing precision of the gears might influence the assumptions made in the calculation of stresses. [10%]

(b) A pair of spur gears has the following specification:

module	$m = 3 \text{ mm}$
pressure angle	$\phi = 20^\circ$
face width	$w = 30 \text{ mm}$
addendum	$a = m$
number of teeth on pinion	$N_1 = 19$
number of teeth on wheel	$N_2 = 59$
contact modulus	$E^* = 115 \text{ GN m}^{-2}$

Find the maximum allowable torque on the pinion if the maximum contact stress is not to exceed  $1200 \text{ MN m}^{-2}$ . Assume that the gears are made imprecisely. [50%]

(c) For a given size of gear (pitch circle diameter and face width), tooth bending stress can be reduced by increasing the module.

(i) Show that the minimum number of gear teeth to avoid interference for a pair of *equal* size standard gears ( $a = m$  and  $\phi = 20^\circ$ ) is 13. [30%]

(ii) Explain why increasing the module for a given size of gear might lead to an increase in contact stress. [10%]

**END OF PAPER**



# ENGINEERING TRIPOS Part IIA

## Module 3C8 Data Sheet

### ELASTIC CONTACT STRESS FORMULAE

Suffixes 1, 2 refer to the two bodies in contact.

$$\text{Effective curvature } \frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$$

$$\text{Contact modulus } \frac{1}{E^*} = \frac{1-\nu_1^2}{E_1} + \frac{1-\nu_2^2}{E_2}$$

where  $R_1, R_2$  are the radii of curvature of the two bodies (convex positive).

where  $E_1, E_2$  and  $\nu_1, \nu_2$  are Young's moduli and Poisson's ratios

	<u>Line contact</u> width $2b$ ; load $P'$ per unit length	<u>Circular contact</u> diameter $2a$ ; load $P$
Semi contact width or contact radius	$b = 2 \left\{ \frac{P'R}{\pi E^*} \right\}^{1/2}$	$a = \left\{ \frac{3PR}{4E^*} \right\}^{1/3}$
Maximum contact pressure ('Hertz stress')	$p_0 = \left\{ \frac{P'E^*}{\pi R} \right\}^{1/2}$	$p_0 = \frac{1}{\pi} \left\{ \frac{6PE^{*2}}{R^2} \right\}^{1/3}$
Approach of centres	$\delta = \frac{2P'}{\pi} \left[ \frac{1-\nu_1^2}{E_1} \left\{ \ln \left( \frac{4R_1}{b} \right) - \frac{1}{2} \right\} + \frac{1-\nu_2^2}{E_2} \left\{ \ln \left( \frac{4R_2}{b} \right) - \frac{1}{2} \right\} \right]$	$\delta = \frac{a^2}{R} = \frac{1}{2} \left\{ \frac{9}{2} \frac{P^2}{E^{*2} R} \right\}^{1/3}$
Mean contact pressure	$\bar{p} = \frac{P'}{2b} = \frac{\pi}{4} p_0$	$\bar{p} = \frac{P}{\pi a^2} = \frac{2}{3} p_0$
	$\tau_{\max} = 0.300 p_0$ at $x = 0, z = 0.79b$	$\tau_{\max} = 0.310 p_0$ at $r = 0, z = 0.48a$ for $\nu = 0.3$
Maximum tensile stress	zero	$\frac{1}{3}(1-2\nu)p_0$ at $r = a, z = 0.79b$

#### Mildly elliptical contacts

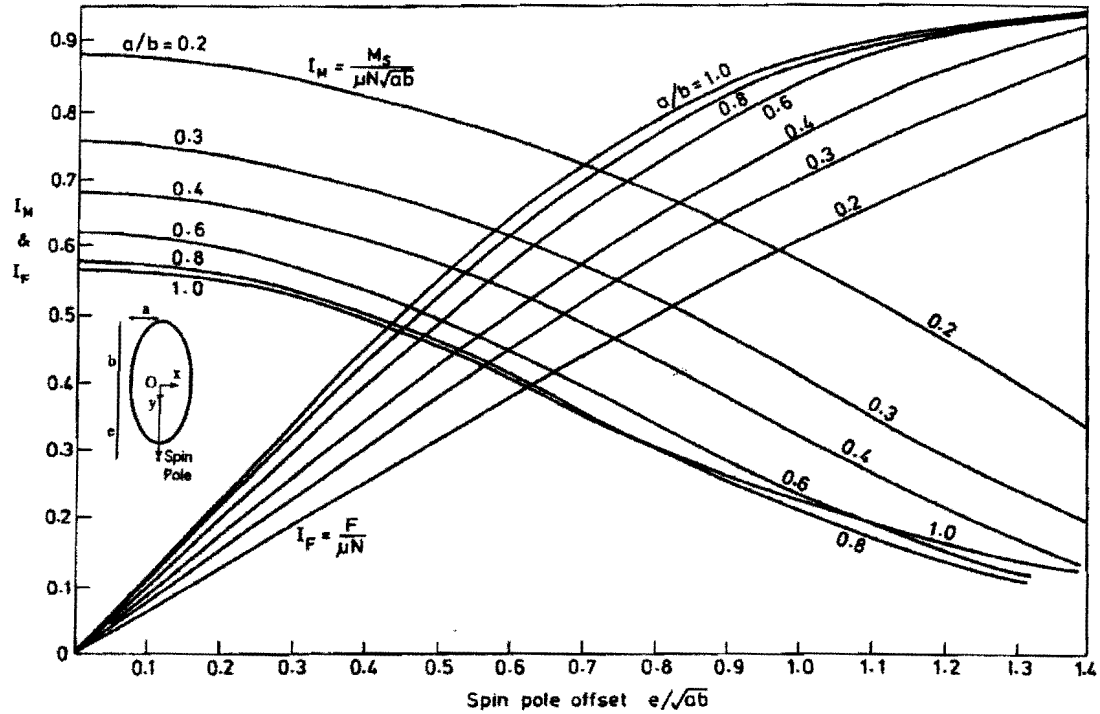
If the gap at zero load is  $h = \frac{1}{2}Ax^2 + \frac{1}{2}By^2$  and  $0.2 < A/B < 5$  then

ratio of semi-axes  $b/a \cong (A/B)^{2/3}$

To calculate the contact **area** or Hertz **stress** use the circular contact equations with  $R = (AB)^{-1/2}$  or better  $R_e = [AB(A+B)/2]^{-1/3}$ .

For **approach** use circular contact equation with  $R = (AB)^{-1/2}$  (**not**  $R_e$ )

## Hertzian contact frictional losses



## INVOLUTE GEARING

### Spur gears

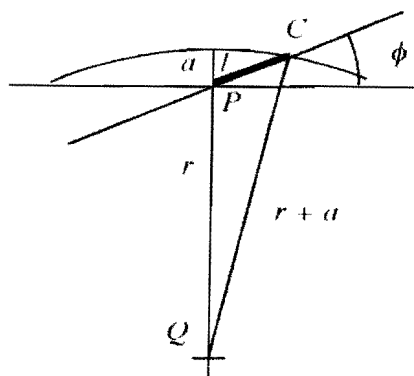
pitch cylinder radii  $r$   
 base cylinder radii  $r_b$   
 addendum cylinder radii  $r_a$   
 number of teeth  $N$

with suffix 1 or 2

addendum  $a = r_a - r$   
 pressure angle  $\phi$

circumferential pitch  $p = 2\pi r / N$   
 base pitch  $p_b = p \cos \phi$   
 module  $m = p / \pi = 2r / N$   
 ratio of contact  $r_c$   
 radius of curvature at pitch point  $\rho = r \sin \phi$

### Path of contact



$$l = \left[ r^2 \sin^2 \phi + a(2r + a) \right]^{1/2} - r \sin \phi$$

For a standard  $20^\circ$  spur wheel with  $N$  teeth of module  $m$  this becomes

$$\frac{l}{m} = \left( 0.02924N^2 + N + 1 \right)^{1/2} - 0.1710N$$

Standard tooth forms

Addendum  $a = m$ , Dedendum  $= \frac{7}{6}m$ , pressure angle  $= 20^\circ$ .

Modules:	0.3 – 1.0 mm in 0.1 mm steps
1.0 – 4.0 mm in 0.25 mm steps	4.0 – 7.0 mm in 0.5 mm steps
7.0 – 16.0 mm in 1.0 mm steps	16.0 – 24.0 mm in 2.0 mm steps
24.0 – 45.0 mm in 3.0 mm steps	45.0 – 75.0 mm in 5.0 mm steps

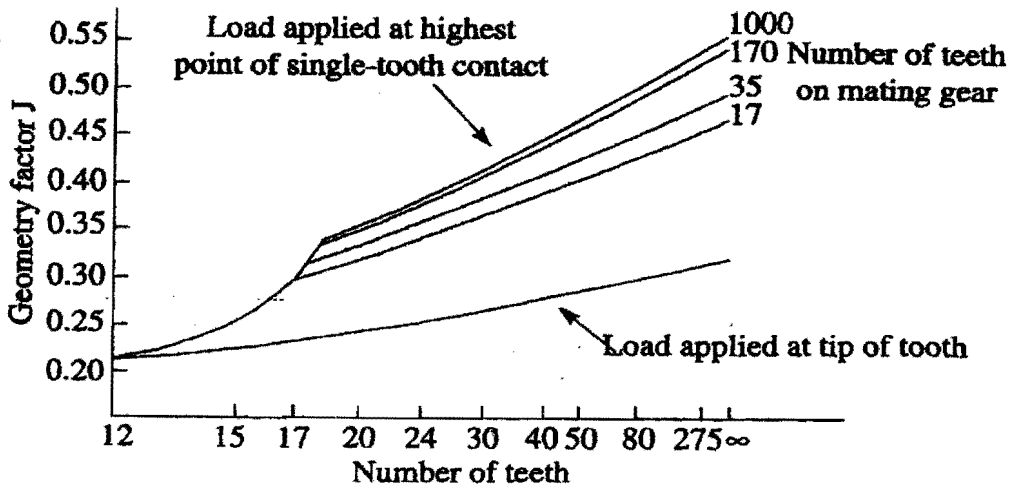
Friction in spur gears

$$\frac{\text{average friction loss}}{\text{power transmitted}} \approx \mu\pi \left\{ \frac{1}{N_1} + \frac{1}{N_2} \right\}$$

Tooth failure

Allowable bending stress  $\sigma_b$  according to AGMA guidelines given by  $\sigma_b = \frac{P_T'}{Jm}$

where  $P_T'$  is force per unit face-width acting tangentially to pitch circle and  $J$  given in the figure below for  $20^\circ$  spur gears. Typical values of  $\sigma_b$  shown in table.



Typical allowable tooth stresses (AGMA)

Material	Condition	Bending fatigue strength $\sigma_b$ (MPa)	Surface fatigue strength $\sigma_s$ (MPa)
Steel	Through hardened and tempered	170-390	590-1200
	Carburised and case hardened	380-480	1250-1550
Cast iron	As cast	69-90	450-590
Nodular iron	Quenched, annealed and tempered	150-300	500-800
Malleable iron	Pearlitic	70-145	500-650

## EPICYCLIC SPEED RULE

$$\omega_s = (1 + R)\omega_c - R\omega_a \quad \text{where } R = \frac{A}{S}$$

## ROLLING ELEMENT BEARINGS

### Fatigue life

$$L = a_1 a_{23} (C/P)^p \quad p = 3 \text{ for ball and } 10/3 \text{ for roller bearings}$$

Fatigue probability %	10	5	4	3	2	1
Life adjust factor $a_1$	1	0.62	0.53	0.44	0.33	0.21

### Bearing choice

The information on the following pages concerning loads, viscosities and standard bearing sizes and ratings is extracted from the SKF General Bearing Catalogue and is copied with permission. It is SKF copyright and is not to be further reproduced.

MPFS, DJC, JAW  
November 07

Required viscosities and the effect of viscosity ratio on  $a_{23}$

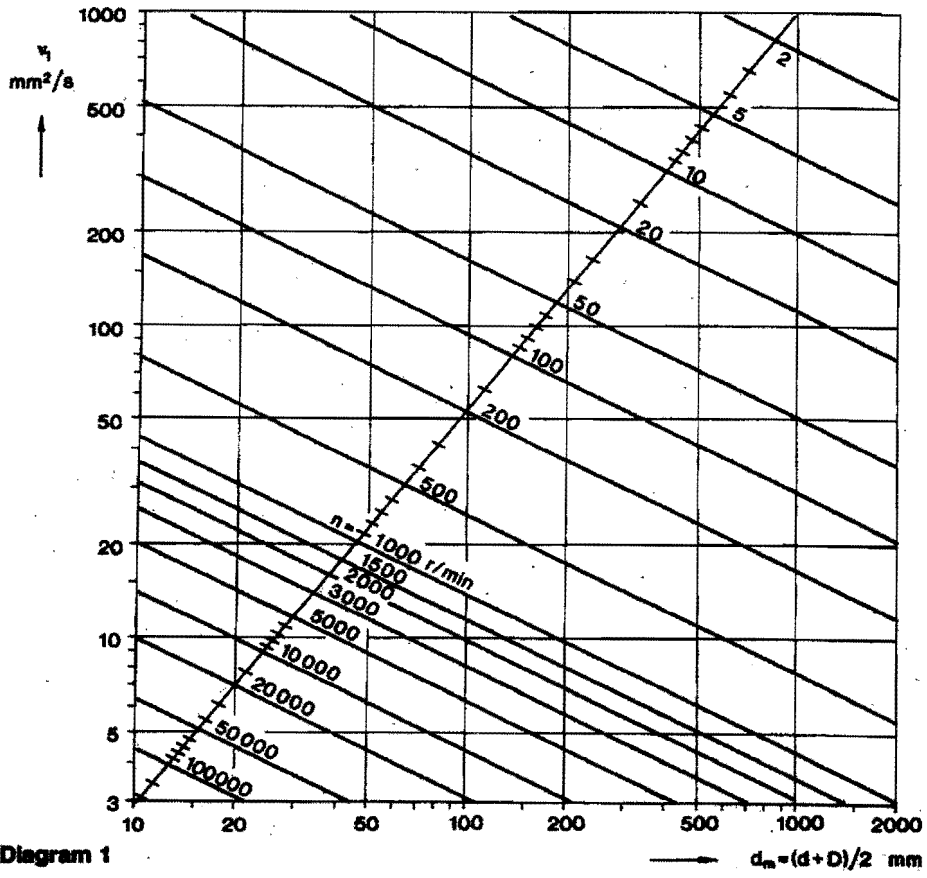


Diagram 1

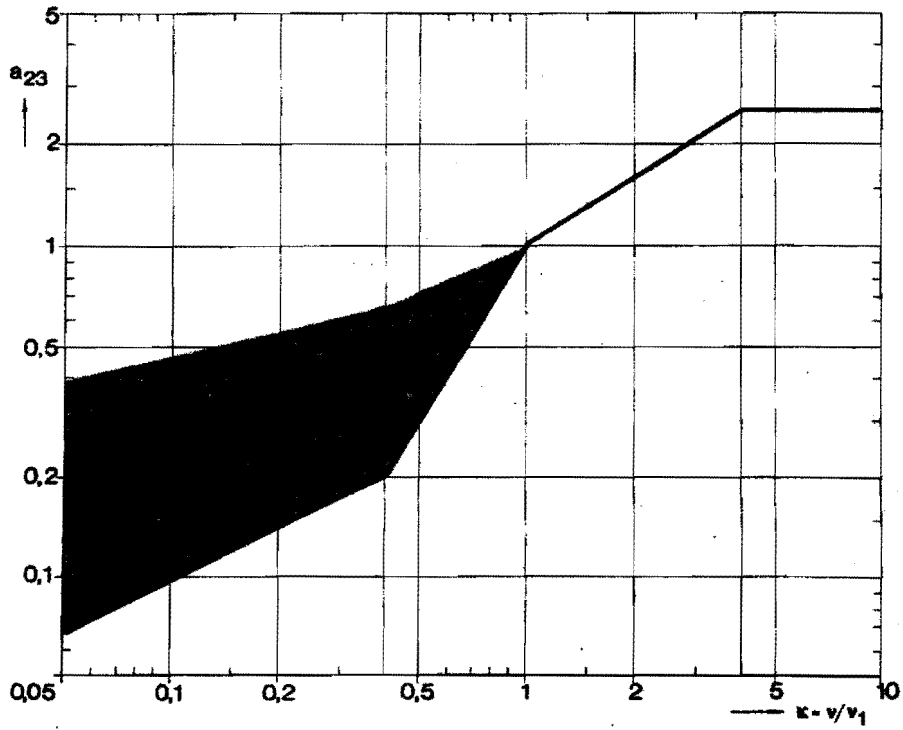
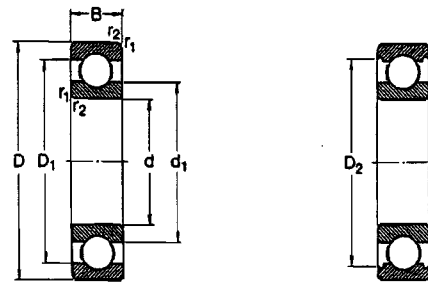


Diagram 3

**Deep groove ball bearings**  
single row  
d 35-55 mm

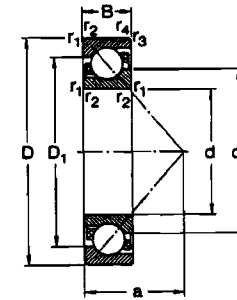


With full outer ring shoulders

With recessed outer ring shoulders

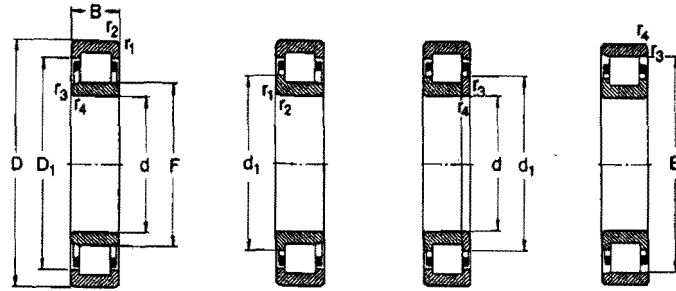
Principal dimensions			Basic load ratings		Fatigue load limit $P_u$	Speed ratings		Mass	Designation
d	D	B	C	$C_0$		grease	oil		
mm			N		N	r/min	kg		-
35	47	7	4 750	3 200	188	13 000	16 000	0,030	61807
	55	10	9 560	6 200	290	11 000	14 000	0,080	61907
	62	9	12 400	8 150	375	10 000	13 000	0,11	16007
	62	14	15 900	10 200	440	10 000	13 000	0,16	6207
	72	17	25 500	15 300	655	9 000	11 000	0,29	6207
60	21	33 200	19 000	815	8 500	10 000	0,46	6307	
	100	25	55 300	31 000	1 290	7 000	8 500	0,95	6407
	40	52	7	4 940	3 450	188	11 000	14 000	0,034
62		12	13 800	9 300	425	10 000	13 000	0,12	61908
68		9	13 300	9 150	440	9 500	12 000	0,13	16008
68		15	16 800	11 600	490	9 500	12 000	0,19	6208
80		18	30 700	19 000	600	8 500	10 000	0,37	6208
90		23	41 000	24 000	1 020	7 500	9 000	0,63	6308
110		27	63 700	36 500	1 530	6 700	8 000	1,25	6408
45		58	7	8 050	4 300	228	9 500	12 000	0,040
	68	12	14 000	9 600	485	9 000	11 000	0,14	61909
	75	10	15 900	10 800	520	9 000	11 000	0,17	16009
	75	16	20 800	14 600	640	9 000	11 000	0,25	6209
	85	19	33 200	21 600	915	7 500	9 000	0,41	6209
	100	25	52 700	31 500	1 340	6 700	8 000	0,83	6309
	120	29	76 100	45 000	1 900	6 000	7 000	1,55	6409
50	65	7	6 240	4 750	250	9 000	11 000	0,052	61810
	72	12	14 600	10 400	500	8 500	10 000	0,14	61910
	80	10	16 300	11 400	580	8 500	10 000	0,18	16010
	80	16	21 600	16 000	710	8 500	10 000	0,28	6210
	90	20	35 100	23 200	960	7 000	8 500	0,48	6210
	110	27	61 800	38 000	1 600	6 300	7 500	1,05	6310
	130	31	87 100	52 000	2 200	5 300	6 300	1,90	6410
55	72	9	8 640	6 800	360	8 500	10 000	0,083	61811
	80	13	15 900	11 400	560	8 000	9 500	0,19	61911
	90	11	19 500	14 000	685	7 500	9 000	0,26	16011
	90	18	28 100	21 200	900	7 500	9 000	0,39	6211
	100	21	43 600	29 000	1 250	6 300	7 500	0,61	6211
	120	29	71 500	45 000	1 900	5 600	6 700	1,35	6311
	140	33	99 500	62 000	2 600	5 000	6 000	2,30	6411

**Angular contact ball bearings**  
single row  
d 10-65 mm



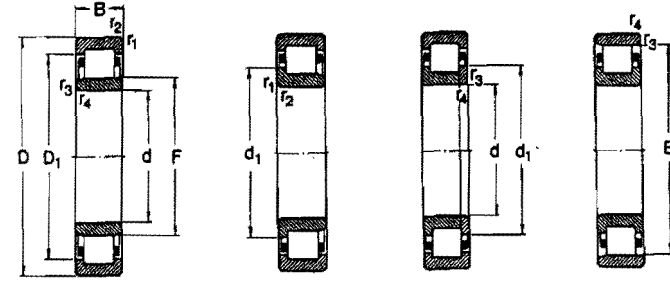
Principal dimensions			Basic load ratings		Fatigue load limit $P_u$	Speed ratings		Mass	Designation
d	D	B	C	$C_0$		grease	oil		
mm			N		N	r/min	kg		-
10	30	9	7 020	3 350	140	19 000	26 000	0,030	7200 BE
12	32	10	7 610	3 800	160	18 000	26 000	0,036	7201 BE
	37	12	10 800	5 000	208	17 000	24 000	0,060	7301 BE
15	35	11	8 840	4 800	204	17 000	24 000	0,045	7202 BE
	42	13	13 000	6 700	280	15 000	20 000	0,080	7302 BE
17	40	12	11 100	6 100	260	15 000	20 000	0,065	7203 BE
	47	14	15 900	8 300	355	13 000	16 000	0,11	7303 BE
20	47	14	14 000	6 300	355	12 000	17 000	0,11	7204 BE
	52	15	19 000	10 400	440	11 000	16 000	0,14	7304 BE
25	52	15	15 800	10 200	430	10 000	15 000	0,13	7205 BE
	62	17	26 000	15 600	655	9 000	13 000	0,23	7305 BE
30	62	16	23 800	15 600	655	8 500	12 000	0,20	7206 BE
	72	19	34 500	21 200	900	6 000	11 000	0,34	7306 BE
35	72	17	30 700	20 800	880	8 000	11 000	0,28	7207 BE
	80	21	39 000	24 500	1 040	7 500	10 000	0,45	7307 BE
40	80	18	36 400	26 000	1 100	7 000	9 500	0,37	7208 BE
	90	23	49 400	33 500	1 400	6 700	9 000	0,63	7308 BE
45	85	19	37 700	28 000	1 200	6 700	9 000	0,42	7209 BE
	100	25	60 500	41 500	1 730	6 000	8 000	0,85	7309 BE
50	90	20	39 000	30 500	1 290	6 000	8 000	0,47	7210 BE
	110	27	74 100	51 000	2 200	5 300	7 000	1,10	7310 BE
55	100	21	46 800	38 000	1 630	5 600	7 500	0,62	7211 BE
	120	29	85 200	60 000	2 550	4 800	6 300	1,40	7311 BE
60	110	22	57 200	45 500	1 930	5 000	6 700	0,80	7212 BE
	130	31	95 800	69 500	3 000	4 500	6 000	1,75	7312 BE
65	120	23	66 300	54 000	2 280	4 500	6 000	1,00	7213 BE
	140	33	108 000	80 000	3 350	4 300	5 600	2,15	7313 BE

**Cylindrical roller bearings  
single row  
d 40-45 mm**



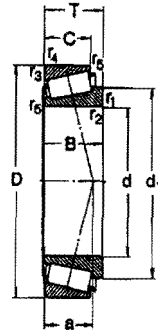
Principal dimensions	Basic load ratings		Fatigue load limit $P_u$	Speed ratings		Mass	Designation	
	dynamic	static		Lubrication grease	oil			
d D B	C	$C_0$	N	r/min	kg	-		
40	90	23	80 900	78 000	10 200	6 700 8 000	0,65	NU 308 EC
(cont.)	90	23	60 900	78 000	10 200	6 700 8 000	0,67	NJ 308 EC
	90	23	80 900	78 000	10 200	6 700 8 000	0,68	NUP 308 EC
	90	23	80 900	78 000	10 200	6 700 8 000	0,64	N 308 EC
	90	33	112 000	120 000	15 300	6 300 7 500	0,94	NU 2308 EC
	90	33	112 000	120 000	15 300	6 300 7 500	0,96	NJ 2308 EC
	90	33	112 000	120 000	15 300	6 300 7 500	0,98	NUP 2308 EC
	110	27	96 800	90 000	11 600	6 000 7 000	1,30	NU 408
	110	27	96 800	90 000	11 600	6 000 7 000	1,30	NJ 408
	110	27	96 800	90 000	11 600	6 000 7 000	1,35	NUP 408
45	75	16	44 600	52 000	6 300	9 000 11 000	0,28	NU 1009 EC
	65	19	60 500	64 000	8 150	6 700 8 000	0,43	NU 209 EC
	65	19	60 500	64 000	8 150	6 700 8 000	0,44	NJ 209 EC
	65	19	60 500	64 000	8 150	6 700 8 000	0,45	NUP 209 EC
	65	19	60 500	64 000	8 150	6 700 8 000	0,43	N 209 EC
	85	23	73 700	81 500	10 600	6 700 8 000	0,52	NU 2209 EC
	85	23	73 700	81 500	10 600	6 700 8 000	0,54	NJ 2209 EC
	85	23	73 700	81 500	10 600	6 700 8 000	0,55	NUP 2209 EC
	85	23	73 700	81 500	10 600	6 700 8 000	0,52	N 2209 EC
	100	25	99 000	100 000	12 900	6 300 7 500	0,90	NU 309 EC
	100	25	99 000	100 000	12 900	6 300 7 500	0,92	NJ 309 EC
	100	25	99 000	100 000	12 900	6 300 7 500	0,95	NUP 309 EC
	100	25	99 000	100 000	12 900	6 300 7 500	0,88	N 309 EC
	100	38	138 000	153 000	20 000	5 600 6 700	1,30	NU 2309 EC
	100	38	138 000	153 000	20 000	5 600 6 700	1,30	NJ 2309 EC
	100	38	138 000	153 000	20 000	5 600 6 700	1,35	NUP 2309 EC
	120	29	106 000	102 000	13 400	5 600 6 700	1,65	NU 409
	120	29	106 000	102 000	13 400	5 600 6 700	1,65	NJ 409
	120	29	106 000	102 000	13 400	5 600 6 700	1,70	NUP 409

**Cylindrical roller bearings  
single row  
d 50-55 mm**



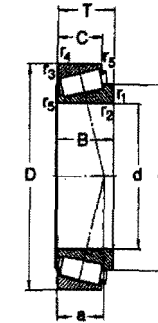
Principal dimensions	Basic load ratings		Fatigue load limit $P_u$	Speed ratings		Mass	Designation	
	dynamic	static		Lubrication grease	oil			
d D B	C	$C_0$	N	r/min	kg	-		
50	80	16	30 800	34 500	4 000	8 500 10 000	0,31	NU 1010
	90	20	64 400	69 500	8 800	6 300 7 500	0,48	NU 210 EC
	90	20	64 400	69 500	8 800	6 300 7 500	0,49	NJ 210 EC
	90	20	64 400	69 500	8 800	6 300 7 500	0,51	NUP 210 EC
	90	20	64 400	69 500	8 800	6 300 7 500	0,48	N 210 EC
	90	23	78 100	88 000	11 400	6 300 7 500	0,56	NU 2210 EC
	90	23	78 100	88 000	11 400	6 300 7 500	0,58	NJ 2210 EC
	90	23	78 100	88 000	11 400	6 300 7 500	0,59	NUP 2210 EC
	110	27	110 000	112 000	15 000	5 000 6 000	1,15	NU 310 EC
	110	27	110 000	112 000	15 000	5 000 6 000	1,15	NJ 310 EC
	110	27	110 000	112 000	15 000	5 000 6 000	1,20	NUP 310 EC
	110	27	110 000	112 000	15 000	5 000 6 000	1,15	N 310 EC
	110	40	161 000	186 000	24 500	5 000 8 000	1,70	NU 2310 EC
	110	40	161 000	186 000	24 500	5 000 8 000	1,75	NJ 2310 EC
	110	40	161 000	186 000	24 500	5 000 6 000	1,80	NUP 2310 EC
	130	31	130 000	127 000	18 600	5 000 8 000	2,00	NU 410
	130	31	130 000	127 000	18 600	5 000 6 000	2,05	NJ 410
55	90	18	57 200	69 500	8 300	7 000 8 500	0,40	NU 1011 EC
	100	21	84 200	95 000	12 200	6 000 7 000	0,66	NU 211 EC
	100	21	84 200	95 000	12 200	6 000 7 000	0,67	NJ 211 EC
	100	21	84 200	95 000	12 200	6 000 7 000	0,69	NUP 211 EC
	100	21	84 200	95 000	12 200	6 000 7 000	0,66	N 211 EC
	100	25	99 000	118 000	15 300	6 000 7 000	0,79	NU 2211 EC
	100	25	99 000	118 000	15 300	6 000 7 000	0,81	NJ 2211 EC
	100	25	99 000	118 000	15 300	6 000 7 000	0,82	NUP 2211 EC
	100	25	99 000	118 000	15 300	6 000 7 000	0,79	N 2211 EC
	120	29	138 000	143 000	18 600	4 800 5 600	1,45	NU 311 EC
	120	29	138 000	143 000	18 600	4 800 5 600	1,50	NJ 311 EC
	120	29	138 000	143 000	18 600	4 800 5 600	1,55	NUP 311 EC
	120	29	138 000	143 000	18 600	4 800 5 600	1,45	N 311 EC

Taper roller bearings  
single row  
d 35-50 mm



Principal dimensions		Basic load ratings		Fatigue load limit	Speed ratings	Mass	Designation	Dimension Series to ISO 355			
d	D	T	C	C <sub>0</sub>	P <sub>u</sub>	r/min	Lubrication grease oil	kg			
mm	N	N	r/min	kg	-	-	-	-			
35 (cont.)	80	22,75	72 100	73 500	8 500	5 000	6 700	0,52	30307	2FB	
	80	22,75	81 800	87 000	7 800	4 500	6 000	0,52	31307	7FB	
	80	32,75	95 200	106 000	12 200	4 800	6 300	0,73	32307	2FE	
	80	32,75	93 500	114 000	13 200	4 500	6 000	0,80	32307 B	5FE	
40	68	19	52 800	71 000	7 800	5 300	7 000	0,27	32006 X	3CD	
	75	26	79 200	104 000	11 800	5 000	6 700	0,51	33106	2CE	
	80	19,75	81 800	88 000	7 850	4 800	6 300	0,42	30206	3DB	
	80	24,75	74 800	86 500	9 800	4 800	6 300	0,53	32206	3DC	
	80	32	105 000	132 000	15 300	4 300	5 600	0,77	33206	2DE	
	65	33	121 000	150 000	17 300	4 500	6 000	0,90	T2EE 040	2FE	
	90	25,25	85 800	95 000	11 000	4 500	6 000	0,72	30306	2FB	
	90	25,25	73 700	81 500	9 850	4 000	5 300	0,72	31306	7FB	
	90	35,25	117 000	140 000	16 300	4 000	5 300	1,00	32306	2FD	
	90	35,25	106 000	140 000	16 300	4 000	5 300	1,10	32306 B	5FD	
	45	75	20	58 300	80 000	8 800	4 800	6 300	0,34	32009 X	3CC
		80	26	84 200	114 000	12 900	4 500	6 000	0,56	33109	3CE
85		20,75	86 000	76 500	8 850	4 500	6 000	0,48	30209	3DB	
85		24,75	80 800	98 000	11 200	4 500	6 000	0,58	32209	3DC	
85		24,75	73 700	93 000	11 000	4 300	5 800	0,60	32209 B	5DC	
85		32	106 000	143 000	16 300	4 000	5 300	0,82	33209	3DE	
95		29	89 700	112 000	12 900	3 600	4 800	0,92	T7FC 045	7FC	
95		36	147 000	186 000	21 200	4 000	5 300	1,20	T2ED 045	2ED	
100		27,25	108 000	120 000	14 600	4 000	5 300	0,97	30309	2FB	
100		27,25	91 300	102 000	12 500	3 400	4 600	0,95	31309	7FB	
100		38,25	140 000	170 000	20 400	3 600	4 800	1,35	32309	2FD	
100		38,25	134 000	176 000	20 000	3 600	4 800	1,45	32309 B	5FD	
50	60	20	60 500	86 000	9 550	4 500	6 000	0,37	32010 X	3CC	
	80	24	69 300	102 000	11 400	4 500	6 000	0,45	33010	2CE	
	82	21,5	72 100	100 000	11 000	4 500	6 000	0,43	K-JLM 104948/K-JLM 104910	-	
	85	26	85 800	122 000	13 700	4 300	5 600	0,59	33110	3CE	
	90	21,75	78 500	91 500	10 400	4 300	5 600	0,54	30210	3DB	
	90	24,75	82 500	100 000	11 600	4 300	5 800	0,61	32210	3DC	
	90	24,75	82 500	104 000	12 500	4 000	5 300	0,65	32210 B	5DC	
	90	26	106 000	140 000	16 300	4 000	5 300	0,75	K-JM 205149/K-JM 205110	-	
	90	26	106 000	140 000	16 300	4 000	5 300	0,75	K-JM 205149/K-JM 205110 A	-	
	90	32	114 000	180 000	18 300	3 600	5 000	0,90	33210	3DE	
	100	36	154 000	200 000	22 600	3 600	5 000	1,30	T2ED 050	2ED	
	105	32	108 000	137 000	16 000	3 200	4 300	1,20	T7FC 050	7FC	

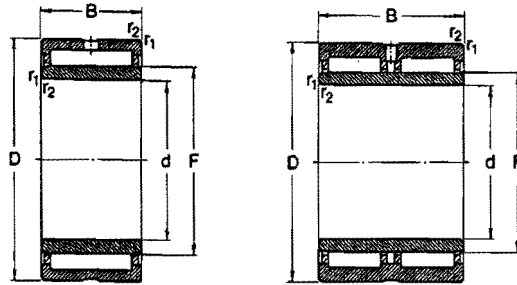
Taper roller bearings  
single row  
d 50-65 mm



Principal dimensions		Basic load ratings		Fatigue load limit	Speed ratings	Mass	Designation	Dimension Series to ISO 355		
d	D	T	C	C <sub>0</sub>	P <sub>u</sub>	r/min	Lubrication grease oil	kg		
mm	N	N	r/min	kg	-	-	-	-		
60 (cont.)	110	29,25	125 000	140 000	17 000	3 600	4 800	1,25	30310	2FB
	110	29,25	106 000	120 000	14 300	3 200	4 300	1,20	31310	7FB
	110	42,25	172 000	212 000	24 500	3 200	4 300	1,80	32310	2FD
	110	42,25	161 000	216 000	25 000	3 200	4 300	1,85	32310 B	5FD
65	90	23	78 100	112 000	12 500	4 000	5 300	0,56	K-JLM 506849/K-JLM 506810	-
	90	23	80 800	118 000	13 200	4 000	5 300	0,55	32011 X	3CC
	90	27	89 700	137 000	15 300	4 000	5 300	0,87	33011	2CE
	95	30	110 000	156 000	18 000	3 800	5 000	0,88	33111	3CE
	100	22,75	89 700	108 000	12 200	3 800	5 000	0,70	30211	3DB
	100	28,75	106 000	129 000	15 000	3 800	5 000	0,83	32211	3DC
	100	28,75	101 000	127 000	15 300	3 800	4 800	0,87	32211 B	-
	100	35	138 000	190 000	22 000	3 400	4 500	1,20	33211	-
	110	39	178 000	232 000	26 500	3 400	4 500	1,70	T2ED 055	3DE
	115	34	125 000	163 000	19 600	3 000	4 000	1,60	T7FC 055	7FB
	120	31,5	142 000	183 000	19 600	3 200	4 300	1,55	30311	2ED
	120	31,5	121 000	137 000	17 000	2 800	3 800	1,55	31311	7FB
120	45,5	198 000	250 000	29 000	3 000	4 000	2,30	32311	2FD	
120	45,5	190 000	260 000	30 000	2 800	3 800	2,50	32311 B	5FD	
60	95	23	82 500	122 000	13 700	3 800	5 000	0,59	32012 X	4CC
	95	24	84 200	132 000	15 000	3 600	4 600	0,62	K-JLM 508748/K-JLM 508710	-
	95	27	91 300	143 000	16 000	3 800	5 000	0,71	33012	2CE
	100	30	117 000	170 000	19 600	3 600	4 800	0,92	33112	3CE
	110	23,75	99 000	114 000	13 400	3 400	4 500	0,88	30212	3EB
	110	29,75	125 000	160 000	19 000	3 400	4 500	1,15	32212	3EC
	110	38	166 000	238 000	27 000	3 000	4 000	1,60	33212	3EE
	115	39	166 000	250 000	27 500	3 000	4 000	1,85	T5ED 060	5ED
	115	40	194 000	260 000	30 000	3 200	4 300	1,85	T2EE 060	2EE
	125	37	154 000	204 000	24 500	2 600	3 600	2,05	T7FC 060	7FC
	130	33,5	168 000	196 000	23 600	3 000	4 000	1,95	30312	2FB
	130	33,5	145 000	168 000	20 400	2 600	3 600	1,90	31312	7FB
130	48,5	229 000	290 000	34 000	2 600	3 600	2,85	32312	2FD	
130	48,5	220 000	305 000	35 500	2 600	3 800	2,80	32312 B	5FD	
65	100	23	84 200	127 000	14 300	3 400	4 500	0,83	32013 X	4CC
	100	27	96 800	156 000	17 600	3 400	4 500	0,78	33013	2CE
	110	28	123 000	163 000	21 200	3 200	4 300	1,05	K-JM 511948/K-JM 511910	-
	110	34	142 000	208 000	24 500	3 200	4 300	1,20	33113	3DE
	120	24,75	114 000	134 000	16 300	3 000	4 000	1,15	30213	3EB
	120	32,75	151 000	189 000	23 200	3 000	4 000	1,50	32213	3EC
	120	39	161 000	240 000	27 500	3 000	4 000	1,95	T5ED 065	5ED



**Needle roller bearings with flanges  
with inner ring**  
d 40-65 mm



Series NKI(S), NA 49

Series NA 69

b

Principal dimensions			Basic load ratings		Fatigue load limit $P_u$	Speed ratings		Mass	Designation
d	D	B	C	$C_0$		Lubrication grease	oil		
mm			N		N	r/min		kg	-
40	55	20	27 500	57 000	7 200	8 300	9 000	0,14	NKI 40/20
	55	30	40 200	93 000	12 000	8 300	9 000	0,22	NKI 40/30
	82	22	42 900	71 000	9 150	5 600	8 000	0,23	NA 4908
	82	40	87 100	125 000	18 000	5 600	8 000	0,43	NA 6908
	65	22	42 900	72 000	9 150	5 600	8 000	0,28	NKIS 40
42	57	20	28 200	61 000	7 650	6 000	8 500	0,15	NKI 42/20
	57	30	41 800	98 000	12 900	6 000	8 500	0,22	NKI 42/30
45	62	25	38 000	78 000	10 000	5 600	8 000	0,23	NKI 45/25
	62	35	49 500	110 000	14 300	5 600	8 000	0,32	NKI 45/35
	68	22	45 700	78 000	10 000	5 300	7 500	0,27	NA 4909
	68	40	70 400	137 000	17 300	5 300	7 500	0,50	NA 6909
	72	22	44 600	78 000	10 000	5 000	7 000	0,34	NKIS 45
50	68	25	40 200	88 000	11 200	5 300	7 500	0,27	NKI 50/25
	68	35	52 300	122 000	16 000	5 300	7 500	0,38	NKI 50/35
	72	22	47 300	85 000	11 000	5 000	7 000	0,27	NA 4910
	72	40	73 700	150 000	19 000	5 000	7 000	0,52	NA 6910
	80	28	62 700	104 000	13 700	4 500	6 300	0,52	NKIS 50
55	72	25	41 800	96 500	12 200	4 800	6 700	0,27	NKI 55/25
	72	35	55 000	134 000	17 600	4 800	6 700	0,38	NKI 55/35
	80	25	57 200	106 000	13 700	4 500	6 300	0,40	NA 4911
	80	45	89 700	190 000	24 000	4 500	6 300	0,78	NA 6911
		85	28	86 000	114 000	15 000	4 300	6 000	0,56
60	82	25	44 000	95 000	12 000	4 300	6 000	0,40	NKI 60/25
	82	35	60 500	146 000	19 000	4 300	6 000	0,55	NKI 60/35
	85	25	60 600	114 000	14 600	4 300	6 000	0,43	NA 4912
	85	45	93 600	204 000	26 000	4 300	6 000	0,81	NA 6912
		90	28	88 200	120 000	15 600	4 000	5 600	0,56
65	90	25	61 800	120 000	15 300	4 000	5 600	0,46	NA 4913
	90	35	82 800	166 000	21 700	4 000	5 600	0,66	NKI 65/35
	90	45	95 200	212 000	27 000	4 000	5 600	0,83	NA 6913
	95	28	70 400	132 000	17 000	3 800	5 300	0,64	NKIS 65