

Q1 (a) From lecture notes: velocity potential ϕ for the flow satisfies $\nabla^2 \phi = 0$

Boundary conditions:

(1) Top surface $\frac{\partial^2 \phi}{\partial t^2} = -g \frac{\partial \phi}{\partial z}$ on $z=0$

(2) Bottom: deep water, so $u = \nabla \phi \rightarrow 0$ as $z \rightarrow -\infty$

(3) Side walls: no flow through walls so $\frac{\partial \phi}{\partial y} = 0$ on $y=0, L$

The model neglects viscosity and surface tension. It also assumes that wave amplitudes are small.

(b) Try separable solution $\phi = f(z)g(y)e^{i(\omega t - kx)}$

Then $\nabla^2 \phi = 0$ gives $-k^2 fg + f''g + g''f = 0$

$\therefore \frac{f''}{f} + \frac{g''}{g} - k^2 = 0$

This is in separated form, so deduce that

$\frac{g''}{g} = -\mu^2$ say, and $\frac{f''}{f} = k^2 + \mu^2$ (μ constant)

So $g = \frac{\sin}{\cos} \mu y$. But $g'(0) = 0$, so must be \cos .

Then $g'(y) = 0$ at $y = L$, so $\sin \mu L = 0$

$\therefore \mu = \frac{n\pi}{L}$, $n = 0, 1, 2, 3, \dots$

Then $f'' = (k^2 + \mu^2)f$ so $f = e^{\pm \sqrt{k^2 + \mu^2} z}$

But $f' \rightarrow 0$ as $z \rightarrow -\infty$ (deep water) so only the + sign is relevant.

So possible solutions are $\phi = \phi_0 e^{\sqrt{k^2 + \mu^2} z} \cos \mu y e^{i(\omega t - kx)}$

with $\mu = \frac{n\pi}{L}$, $n = 0, 1, 2, \dots$

Now the top surface condition gives

$$-w^2 = -g \sqrt{k^2 + \mu^2}$$

$$\therefore k^2 = \frac{w^4}{g^2} - \left(\frac{n\pi}{L}\right)^2, \quad n=0, 1, 2, \dots$$

(c) Cut-on frequency where k^2 goes from negative to positive, so where $\frac{w^2}{g} = \frac{n\pi}{L}$.

Phase velocity $c_p = \frac{w}{k} = \frac{w}{\sqrt{\frac{w^4}{g^2} - \left(\frac{n\pi}{L}\right)^2}}$

Group velocity $c_g = \frac{dw}{dk} = \frac{d}{dk} \left[g^2 (k^2 + \mu^2) \right]^{1/4}$

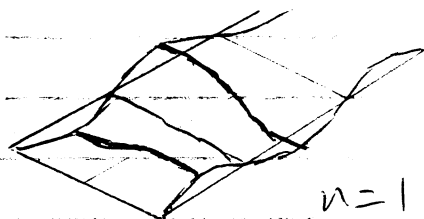
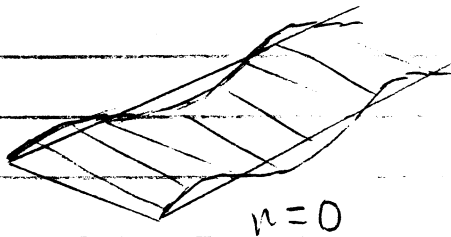
$$= \frac{1}{4} \left[g^2 (k^2 + \mu^2) \right]^{-3/4} \cdot 2g^2 k$$

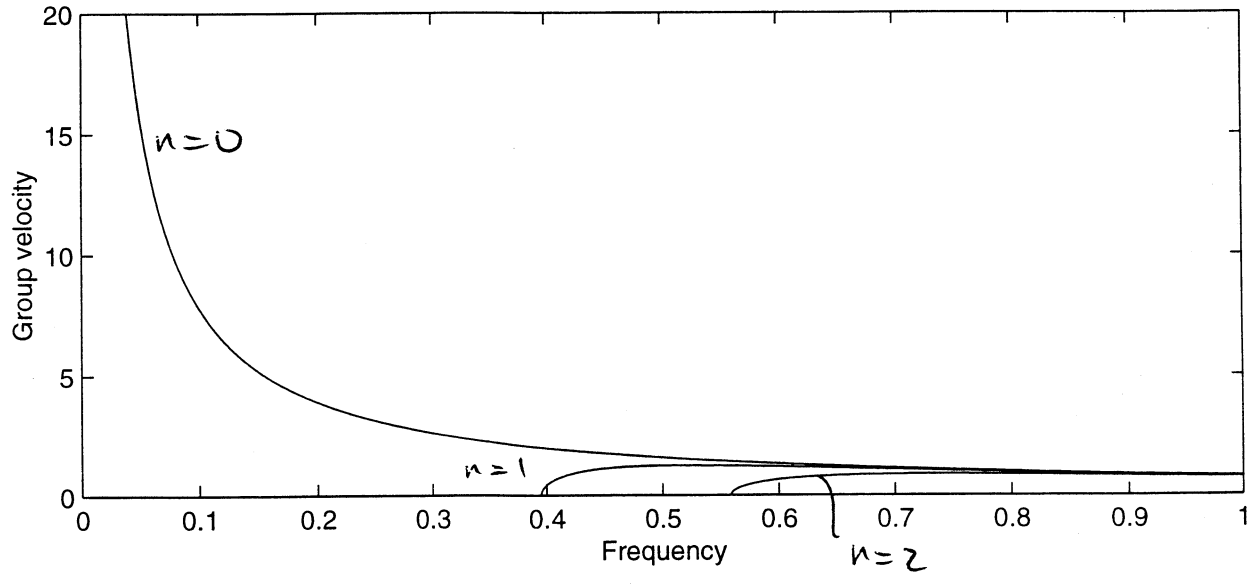
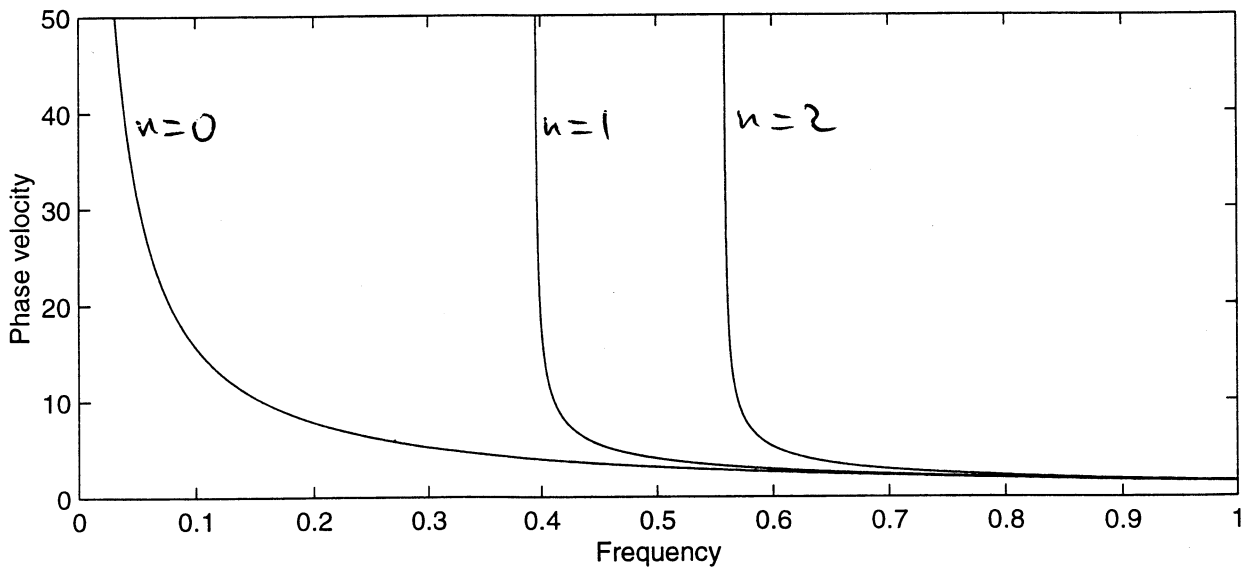
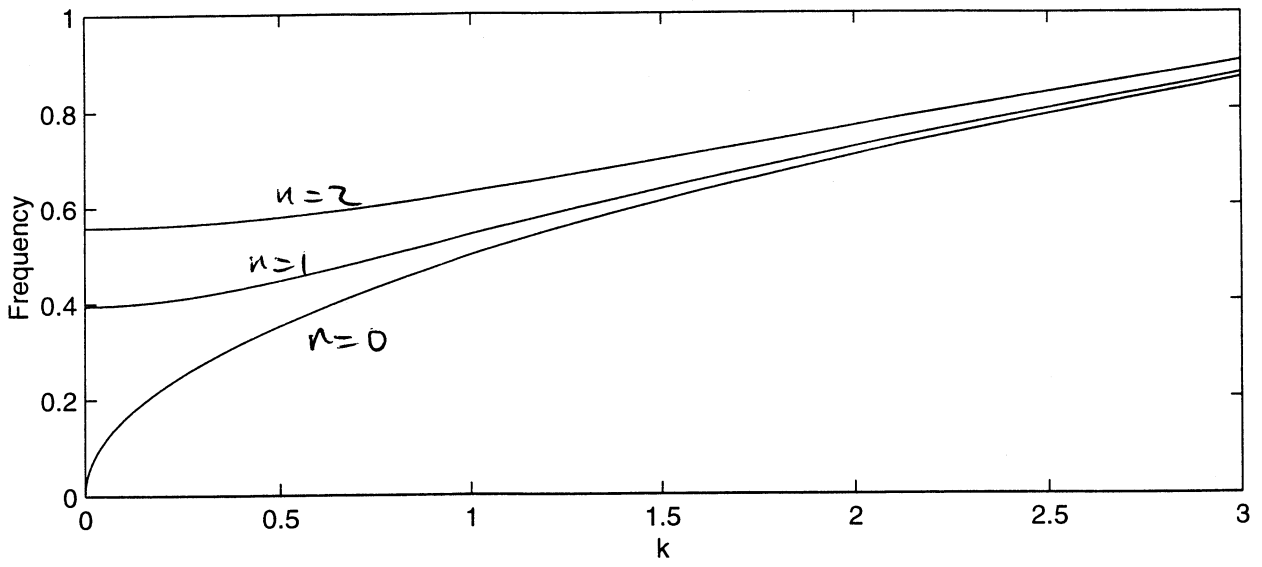
$$= \frac{g^2}{2} \frac{k}{w^3} = \frac{g^2}{2w^3} \sqrt{\frac{w^4}{g^2} - \left(\frac{n\pi}{L}\right)^2}$$

Note that at a cut-on frequency, $c_p \rightarrow \infty$, $c_g \rightarrow 0$.

(d) $L = 5\text{ m}$, so cut-on frequencies are

$n=0$, 0 Hz
$n=1$, 0.395 Hz
$n=2$, 0.559 Hz

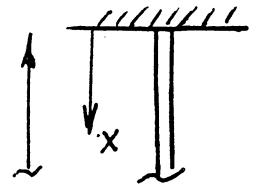




Q2 (a) conservation of translational momentum

$$M \tilde{V}_0 = 2M V_0 \rightarrow V_0 = \tilde{V}_0 / 2$$

$$\sigma_0 = \frac{Mg}{A}$$



(b) eq of motion for mass, $t > 0$

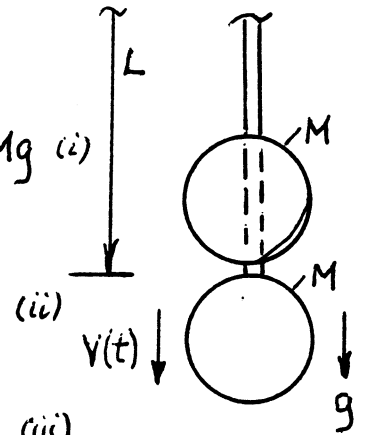
$$2M \frac{dV}{dt} = -A[\sigma_i(L,t) + \sigma_r(L,t)] - A\sigma_0 + 2Mg \quad (i)$$

continuity of velocity

$$V(t) = \dot{u}_i(L,t) + \dot{u}_r(L,t)$$

cons. momentum across wavefront, $t > 0$

$$\sigma_i = -\rho c_0 \dot{u}_i, \quad \sigma_r = \rho c_0 \dot{u}_r \quad (iii)$$



$$\therefore \frac{dV}{dt} = \frac{\rho c_0 A}{2M} \left\{ \dot{u}_i(L,t) - [V(t) - \dot{u}_i(L,t)] \right\} + \frac{g}{2}$$

or $\frac{dV}{dt} + \frac{c_0}{mL} V = 2\dot{u}_i(L,t) + \frac{g}{2}$ where $m \equiv \frac{2M}{\rho AL}$

sol'n

$$V = \frac{gmL}{2c_0} + B e^{-c_0 t / mL}$$

I.C. $V_0 = V(0) = \frac{gmL}{2c_0} + B \Rightarrow B = V_0 - \frac{gmL}{2c_0}$

$$\therefore V(t) = \alpha + (V_0 - \alpha) e^{-\beta t}$$

$$\alpha = \frac{gmL}{2c_0}, \quad \beta = \frac{c_0}{mL}$$

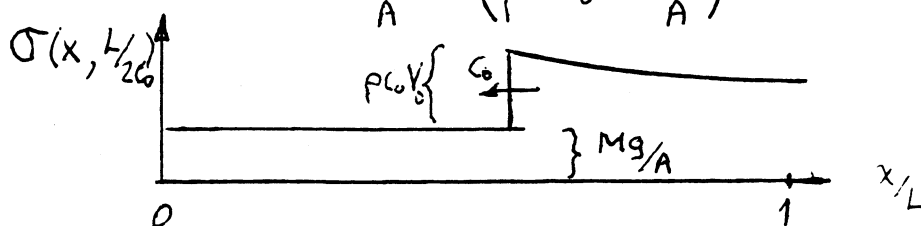
$t < 2L/c_0$

(c)

$$\sigma_r(L,t) = \rho c_0 V(t)$$

$$\sigma_r(x,t) = \rho c_0 \left\{ \alpha + (V_0 - \alpha) e^{-\frac{(c_0 t + x - L)}{mL}} \right\} \quad x > L - c_0 t$$

$$= \frac{Mg}{A} + \left(\rho c_0 V_0 - \frac{Mg}{A} \right) e^{-\frac{(c_0 t + x - L)}{mL}}$$



(d) at clamped end when wavefront arrives, $t = L/c_0$

$$\sigma(0, L/c_0^+) = \sigma_F = \frac{Mg}{A} + 2\rho c_0 V_0 = \frac{Mg}{A} + 2\rho c_0 \frac{\tilde{V}_{0F}}{2}$$

$$\therefore \tilde{V}_{0F} = \frac{\sigma_F}{\rho c_0} - \frac{Mg}{\rho c_0 A} = \frac{\sigma_F}{\rho c_0} - \frac{mgl}{2c_0}$$

break located at $x=0$ (the clamp) at $t = L/c_0^+$

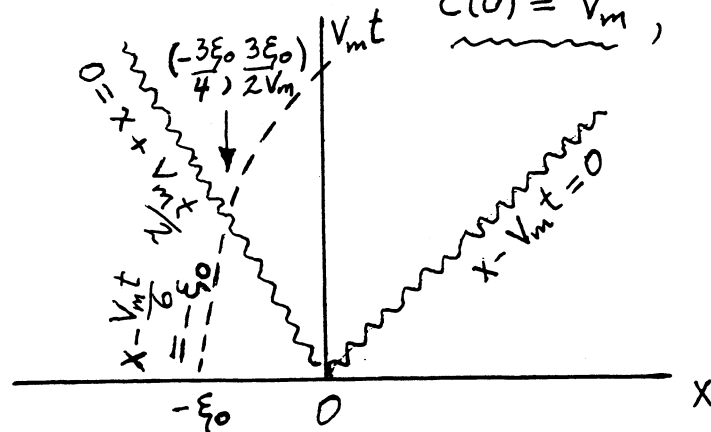
Q3 (a) flux: $q = \rho V = \rho_m V_m (y - y^{3/2})$, $y = \rho/\rho_m$

$$0 = \frac{d(q)}{dy} = \rho_m V_m (1 - \frac{3}{2} y^{1/2})$$

$$\therefore \rho = \frac{4}{9} \rho_m \rightarrow (\text{flux})_{\max}$$

(b) characteristic speeds $c(\rho) = dq/d\rho = V_m (1 - \frac{3}{2} \sqrt{\rho/\rho_m})$

$$c(0) = V_m, \quad c(\rho_m) = -V_m/2$$



constrained speed

$$V = V_m (1 - \sqrt{\rho/\rho_m}) = V_m (1 - 5/6) = V_m/6$$

(c) on characteristic lines in fan emanating from $(0,0)$

$$x = \frac{dq}{d\rho} t = V_m t (1 - \frac{3}{2} \sqrt{\rho/\rho_m}) \rightarrow \sqrt{\rho/\rho_m} = \frac{2}{3} (1 - \frac{x}{V_m t})$$

speed of beam located at $x = \xi(t)$

$$\frac{d\xi}{dt} = V_m \left[1 - \frac{2}{3} \left(1 - \frac{\xi}{V_m t} \right) \right] = \frac{V_m}{3} \left[1 + \frac{2\xi}{V_m t} \right]$$

$$\therefore 3t \frac{d\xi}{dt} - 2\xi = V_m t$$

$$\text{sol'n: } \left. \begin{aligned} \xi &= B_1 V_m t + B_2 t^\eta \\ \frac{d\xi}{dt} &= B_1 V_m + B_2 \eta t^{\eta-1} \end{aligned} \right\} \begin{aligned} 3B_1 V_m t + 2B_2 \eta t^\eta - 2B_1 V_m t \\ - 2B_2 \eta t^\eta &= V_m t \end{aligned}$$

$$\therefore B_1 = 1, \quad \eta = 2/3$$

$$\xi(t) = V_m t + B_2 t^{2/3}$$

(d) in fan: $\xi(t) = V_m t + B_2 t^{2/3}$

initial cond:

beam enters fan at $(-\frac{3\xi_0}{4}, \frac{3\xi_0}{2V_m})$

$$\therefore -\frac{3\xi_0}{4} = \frac{3\xi_0 V_m}{2V_m} + B_2 \left(\frac{3\xi_0}{2V_m}\right)^{2/3}$$

$$B_2 = -\frac{9\xi_0}{4} \left(\frac{2V_m}{3\xi_0}\right)^{2/3}$$

$$\xi(t) = V_m t - \frac{9\xi_0}{4} \left(\frac{2V_m t}{3\xi_0}\right)^{2/3}, \quad t > \frac{3\xi_0}{2V_m}$$

