

ENGINEERING TRIPOS PART IIB

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Monday 2 May 2005 9 to 10.30

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Module 4C7

RANDOM AND NONLINEAR VIBRATION

*Answer not more than three questions.*

*All questions carry the same number of marks.*

*The approximate percentage of marks allocated to each part of a question is indicated in the right margin.*

*Candidates may bring their notebooks to the examination.*

**You may not start to read the questions printed on the subsequent pages of this question paper until instructed that you may do so by the Invigilator.**

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1 The linear oscillator shown in Fig. 1 has a mass  $m$ , supported by a spring of stiffness  $k$  and light damping  $c$ . The displacement of the oscillator at time  $t$  is  $y(t)$ . The oscillator can be excited by force  $f(t)$  or by displacement of its base  $x(t)$ .

(a) If the displacement input is zero and the force input is white noise, with spectral density:

$$S_{ff}(\omega) = S_0 \quad -\infty < \omega < \infty,$$

calculate the mean square displacement of the mass  $E[y^2]$ . Hence show that the *mean square bandwidth*  $\Delta\omega$  is given by:

$$\Delta\omega = \pi\zeta\omega_n$$

where  $\zeta$  is the damping ratio and  $\omega_n$  is the undamped natural frequency of the oscillator. [30%]

The input force is now set to zero and the base is excited by a displacement  $x(t)$  with spectral density

$$S_{xx}(\omega) = \frac{S_1}{1 + (\omega/\omega_0)^2} \quad -\infty < \omega < \infty.$$

Since the damping is light, it may be assumed that the response of the oscillator is essentially in a narrow band of frequencies close to the natural frequency  $\omega_n$ .

(b) Starting from the standard Rayleigh distribution for the probability density of peak heights  $a$  of a narrow band process:

$$p_p(a) = \frac{a}{\sigma_y^2} \exp\left\{-\frac{a^2}{2\sigma_y^2}\right\} \quad (a \geq 0)$$

show that the probability of a peak exceeding a given level  $a$  is:

$$\Pr(y > a) = \exp\left\{-\frac{a^2}{2\sigma_y^2}\right\} \quad (a \geq 0) \quad [20\%]$$

(c) Use the mean square bandwidth to estimate the mean square velocity  $E[\dot{y}^2]$ . [30%]

(d) Using the results of (b) and (c), derive an approximate expression for the amount of viscous damping  $c$  required in order to achieve a given value  $p$  for the probability that a peak in the velocity  $\dot{y}(t)$  exceeds a given level  $v$  [20%]

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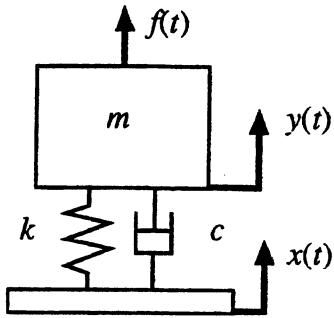


Figure 1

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2 Figure 2 shows a simple single degree-of-freedom model of a vehicle which is moving at constant speed  $V$  over a rough road surface, with displacement profile  $y(x)$ . The vehicle has mass  $m$ , and suspension of linear stiffness  $k$  and viscous damping  $c$ . The displacement of the vehicle body is  $z(t)$ .

The spatial correlation function  $R_{yy}(X)$  and corresponding spectral density  $S_{yy}(\gamma)$  of the road profile  $y(x)$  are given by:

$$R_{yy}(X) = E[y(x) y(x + X)]$$

$$S_{yy}(\gamma) = \frac{1}{2\pi} \int_{-\infty}^{\infty} R_{yy}(X) e^{-i\gamma X} dX$$

where  $X$  is a displacement and  $\gamma$  is wavenumber =  $2\pi/\text{wavelength}$ .

(a) Show that at angular frequency  $\omega$ , the spectral density  $S_{yy}(\omega)$  of the vertical displacement  $y(t)$  of the tyre contact point P is given by

$$S_{yy}(\omega) = \frac{1}{V} S_{yy}(\bar{\gamma})$$

where  $\bar{\gamma} = \omega/V$ .

[30%]

(b) The autocorrelation function of the road profile is measured to be

$$R_{yy}(X) = A e^{-b|X|} \quad -\infty < X < \infty$$

where  $A$  and  $b$  are constants. Show that the road profile spectral density observed by the moving vehicle is

$$S_{yy}(\omega) = \left( \frac{A}{bV\pi} \right) \left( \frac{1}{1 + (\omega/bV)^2} \right).$$

[30%]

(c) Calculate the spectral density  $S_{ff}(\omega)$  of the dynamic tyre force (i.e. the combined force in the spring and damper). [20%]

(d) Estimate the mean square value of the dynamic tyre force. [20%]

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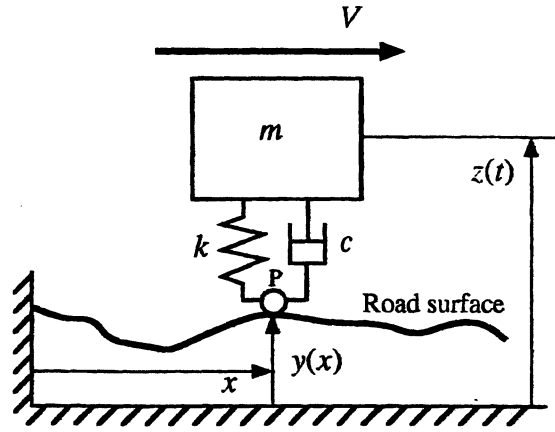


Figure 2

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3 A nonlinear oscillator driven with a sinusoidal force obeys the differential equation

$$m\ddot{x} + k(x) = f \cos \omega t$$

where the nonlinear element  $k(x)$  has the force-displacement characteristic shown in Fig. 3. It has a region at small displacement amplitude that describes a 'negative spring' of stiffness  $-s$ , while for larger amplitudes it shows a positive stiffness  $s$ .

- (a) For sinusoidal displacement with amplitude  $X$ , sketch the force waveform produced by the nonlinear element. [15%]
- (b) Determine the Describing Function for the nonlinear element. [40%]
- (c) Find the limiting form of the Describing Function for very large amplitude  $X$ , and explain this in terms of Fig. 3. [20%]
- (d) Find an approximate expression which determines the relation between the response amplitude  $X$  and frequency  $\omega$  for forced motion of the oscillator. (A closed-form expression is not expected.) [25%]

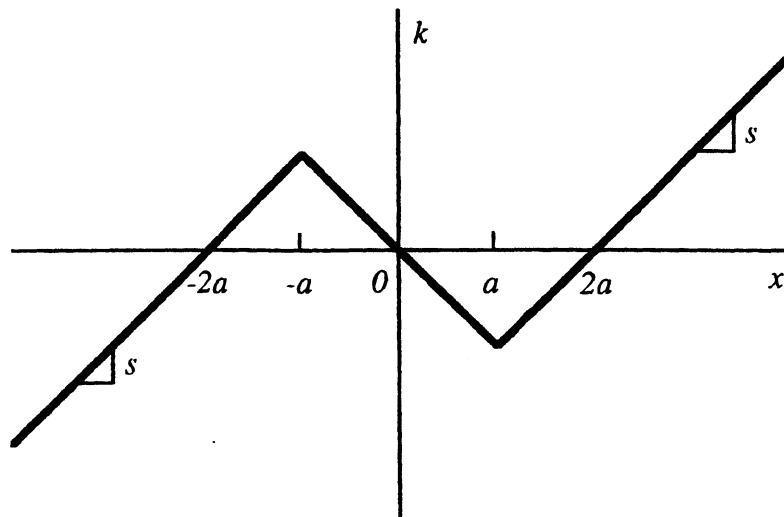


Figure 3

4 The motion of a nonlinear oscillator is described by the differential equation

$$\ddot{x} + kx - x^2 = 0$$

where  $k$  is a constant.

(a) Assuming that  $k > 0$ , find the equilibrium or critical points, and determine their type and stability. Sketch the behaviour of the system in the phase plane. [25%]

Assuming that the system is conservative, find a relation between the potential energy function and the displacement,  $x$ . [15%]

(b) Now assume that  $k < 0$ , so that the system has a negative linear spring. Determine the effect on the critical points and their stability. [20%]

(c) A linear damping term is added to the system from part (b), so that the differential equation becomes

$$\ddot{x} + b\dot{x} + kx - x^2 = 0$$

where  $b$  is the damping constant. Find the critical points and investigate their type and stability. Sketch the phase portrait for each distinct case found. [40%]

**END OF PAPER**

