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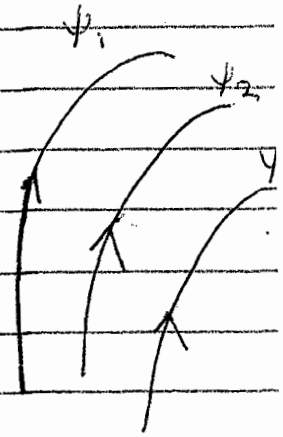
4A12

① (a) If α is small,

$$\underline{\underline{u}} \cdot \nabla T \approx 0$$

\Rightarrow T constant along streamlines

$$\Rightarrow \underline{\underline{T}} = \underline{\underline{T}}(\psi)$$



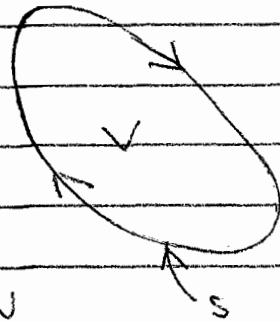
$$\Rightarrow \nabla T = T'(\psi) \nabla \psi$$

$$\Rightarrow \underline{\underline{u}} \cdot \nabla T = \alpha \nabla \cdot (T'(\psi) \nabla \psi) = \alpha \nabla \cdot (T'(\psi) \nabla \psi)$$

Integrating of volume V

$$\int_V \underline{\underline{u}} \cdot \nabla T \, dV = \alpha \int_V \nabla \cdot (T'(\psi) \nabla \psi) \, dV$$

$$\Rightarrow \int_V \nabla \cdot (T \underline{\underline{u}}) \, dV = \alpha \int_V \nabla \cdot (T'(\psi) \nabla \psi) \, dV$$



Use Gauss to convert to surface integrals,

$$\oint_S T \underline{\underline{u}} \cdot d\underline{\underline{s}} = \alpha \oint_S T'(\psi) \nabla \psi \cdot d\underline{\underline{s}}$$

But $\underline{\underline{u}} \cdot d\underline{\underline{s}} = 0$ and $T'(\psi)$ is constant on S .

Thus

$$\underline{\underline{\alpha T'(\psi) \oint_S \nabla \psi \cdot d\underline{\underline{s}} = 0}}$$

(b) Using Gauss again we have $\alpha T'(\psi) \int_V \nabla^2 \psi \, dV = 0$

But $\nabla^2 \psi = -\omega$

c.f. $\underline{u} = \left[\frac{\partial \psi}{\partial y}, -\frac{\partial \psi}{\partial x}, 0 \right]$

$\underline{\omega} = \nabla \times \underline{u} = \left(\frac{\partial u_y}{\partial x} - \frac{\partial u_x}{\partial y} \right) \hat{e}_z = \left(-\frac{\partial^2 \psi}{\partial x^2} - \frac{\partial^2 \psi}{\partial y^2} \right) \hat{e}_z$

$\Rightarrow \alpha T'(\psi) \int \omega \, dV = 0$

$\Rightarrow \alpha T'(\psi) \oint \underline{u} \cdot d\underline{l} = 0$ by Stokes.

But $\alpha \neq 0$ and $\oint \underline{u} \cdot d\underline{l} \neq 0$

Thus $T'(\psi) = 0$ \Rightarrow $T = \text{constant}$

This is achieved by a slow, cross-stream diffusion of ω which continues until T is perfectly uniform.

(c) The P-B theorem states that, 'if the flow is steady, 2D laminar, with closed streamlines and high Re, then ω is uniform. Reason:

• 2D Vorticity equation $\frac{D\omega}{Dt} = \nu \nabla^2 \omega$, is same as heat equation if $\alpha = \nu$. Thus ω behaves like T .

• ν small implies $\underline{u} \cdot \nabla \omega \approx \omega \Rightarrow \omega = \omega(\psi)$

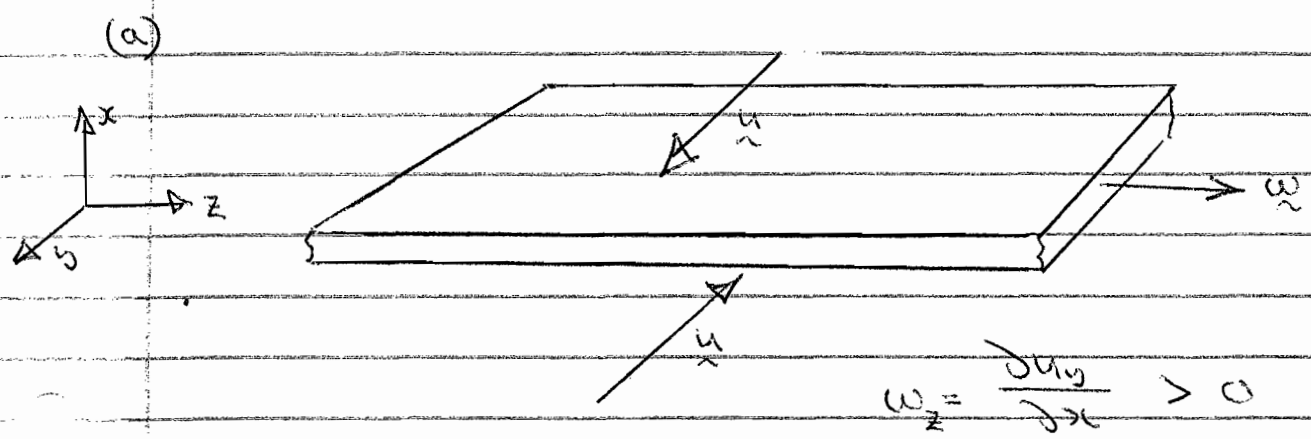
c.f. $T = T(\psi)$

• ν finite means a slow but finite diffusion eventually

eradicates any cross-stream gradients in ω .

② $\vec{\omega} = (u_0/\delta) \exp[-x^2/\delta^2] \hat{e}_z$, $\delta = \delta(t)$

$\vec{u} = u_y(x,t) \hat{e}_y$



(b) $\frac{D\vec{\omega}}{Dt} = (\vec{\omega} \cdot \nabla) \vec{u} + \nu \nabla^2 \vec{\omega}$

$\Rightarrow \frac{\partial \omega_z}{\partial t} + u_y \frac{\partial \omega_z}{\partial y} = \omega_z \frac{\partial u_y}{\partial z} + \nu \frac{\partial^2 \omega_z}{\partial x^2}$

$\Rightarrow \frac{\partial \omega_z}{\partial t} = \nu \frac{\partial^2 \omega_z}{\partial x^2}$

$\Rightarrow u_0 \frac{\partial}{\partial \delta} \left[\frac{1}{\delta} \exp(-x^2/\delta^2) \right] \delta'(t) = \nu \frac{\partial^2}{\partial x^2} \left[\frac{u_0}{\delta} \exp(-x^2/\delta^2) \right]$

$\Rightarrow u_0 \delta'(t) \left[-\frac{1}{\delta^2} + \frac{2x^2}{\delta^4} \right] e^{-x^2/\delta^2} = \nu \frac{u_0}{\delta} \frac{\partial}{\partial x} \left[-\frac{2x}{\delta^2} e^{-x^2/\delta^2} \right]$

$\Rightarrow u_0 \delta'(t) e^{-x^2/\delta^2} \left[-\frac{1}{\delta^2} + \frac{2x^2}{\delta^4} \right] = 2\nu \frac{u_0}{\delta} \left[-\frac{1}{\delta^2} + \frac{2x^2}{\delta^4} \right] e^{-x^2/\delta^2}$

$\Rightarrow \delta'(t) = 2\nu/\delta$

$\Rightarrow \underline{\underline{\delta \delta'(t) = 2\nu}}$

(c)

$$\frac{d\delta^2}{dt} = 4\nu$$

$$\Rightarrow \delta^2 = \delta_0^2 + 4\nu t$$

$$\Rightarrow \delta = \sqrt{\delta_0^2 + 4\nu t}$$

The sheet is diffusing, with diffusion length $\sim \sqrt{4\nu t}$

The net flux of vorticity per-unit length of the sheet is,

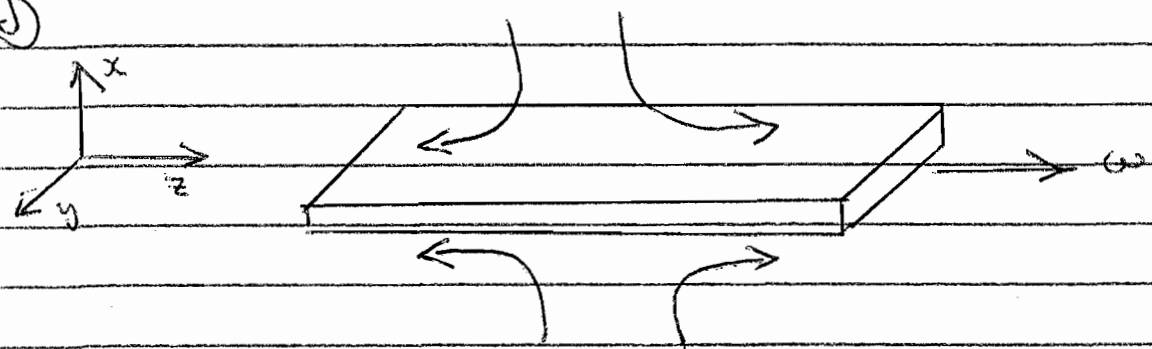
$$\begin{aligned} \Phi &= \int_{-\infty}^{\infty} \omega_z dx = \frac{u_0}{\delta} \int_{-\infty}^{\infty} \exp[-x^2/\delta^2] dx \\ &= u_0 \int_{-\infty}^{\infty} e^{-p^2} dp \quad p = x/\delta \end{aligned}$$

Thus $\Phi \propto u_0$. This flux cannot be changed by diffusion.

c.f. $\frac{\partial \omega_z}{\partial t} = \nu \frac{\partial^2 \omega_z}{\partial x^2}$

$$\Rightarrow \frac{d\Phi}{dt} = \frac{d}{dt} \int_{-\infty}^{\infty} \omega_z dx = \nu \left[\frac{\partial \omega_z}{\partial x} \right]_{-\infty}^{\infty} = 0$$

(d)



The sheet is now subject to stretching by the rotational shearing flow.

Physical Processes:

① Diffusion causes δ to increase and $u_{max} \sim \frac{u_0}{\delta}$ to fall

② Advection by the straining flow causes δ to decrease.

③ Stretching by the straining flow causes u_{max} to increase

With the correct choice of α , we can get a steady flow

If $\left\{ \begin{array}{l} \alpha \gg \nu/\delta_0^2 \text{ the sheet will thin and } u_{max} \text{ rise,} \\ \alpha \ll \nu/\delta_0^2 \text{ the sheet will thicken and } u_{max} \text{ fall} \end{array} \right.$

QUESTION 3

(a) BULKWIND - TO CASE

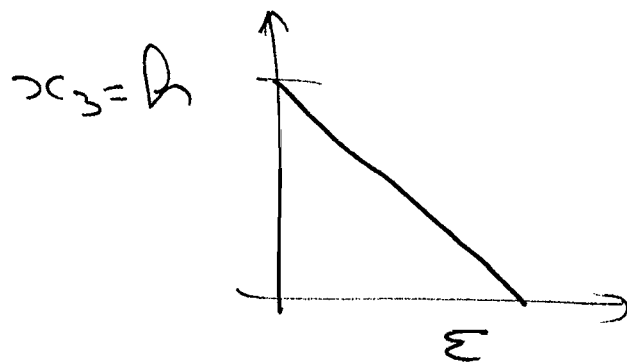
(b) (i) NO MEAN WIND

$$\therefore -\nu \frac{\partial u_i}{\partial x_i} \dots + \frac{g}{T} \overline{\Theta u} = 0$$

$$\downarrow$$

$$-\Sigma + \frac{g}{T} \frac{Q}{\rho c_p} = 0$$

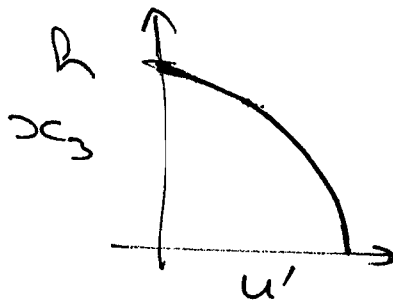
$$\therefore \Sigma = Q_0 \left(1 - \frac{x_3}{h}\right)$$



(ii) $l \sim h$

$$\Sigma \sim u'^3 / l \sim Q_0 \left(1 - \frac{x_3}{h}\right) \sim u'^3 / h$$

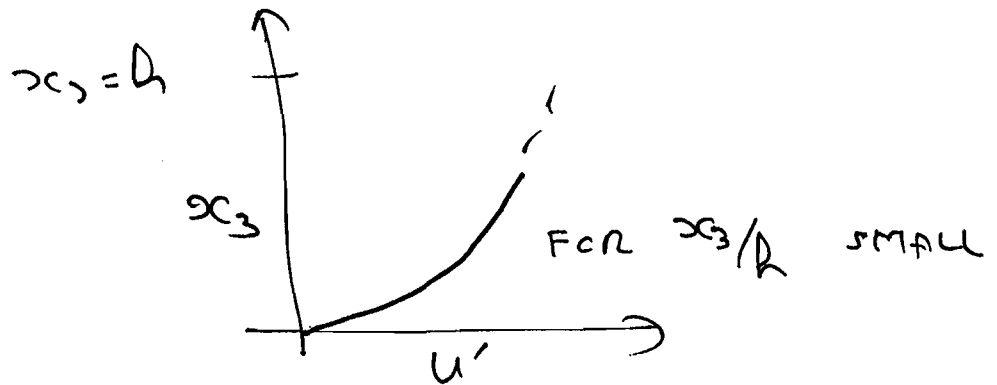
$$\therefore u' = \left\{ Q_0 h \left(1 - \frac{x_3}{h}\right) \right\}^{1/3}$$



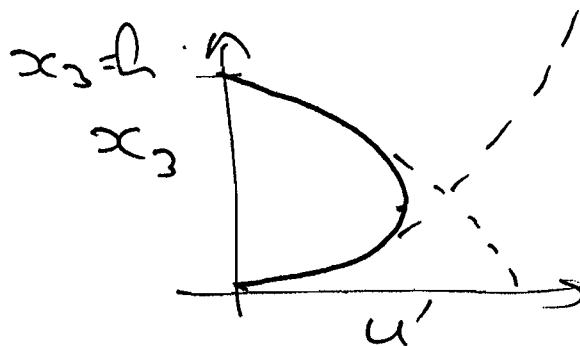
$$(iii) \quad l \sim x_3$$

$$\Sigma \sim u'^3 / l \sim Q_0 (1 - x_3/h) \sim u'^3 / x_3$$

$$\therefore u' \sim \left(Q_0 x_3 (1 - x_3/h) \right)^{1/3}$$



COMPOSITE



QUESTION 4

$$\begin{aligned} \text{(i) INCREASE IN ENERGY} &= \frac{1}{2} m v^2 = m g h \\ &= 20 \times 10^{-6} \times 1000 \times 9.81 \times 0.2 \\ &= 3.92 \times 10^{-2} \text{ JOULES} \end{aligned}$$

(ii) TOTAL ENERGY

$$= 3.92 \times 10^{-2} \text{ JOULES}$$

Now in 250 cm^3 of WATER

$$\therefore \frac{1}{2} m_2 \cdot 3 u'^2 = 3.92 \times 10^{-2}$$

$$\frac{1}{2} \times 250 \times 10^{-6} \times 1000 \times 3 \times u'^2 = 3.92 \times 10^{-2}$$

$$\therefore u'^2 = 0.105 \text{ m}^2/\text{s}^2; \quad u' = 0.323 \text{ m/s}$$

$$Re = \frac{u' l}{\nu} = \frac{0.323 \times 0.07}{1 \times 10^{-6}} = 2.26 \times 10^4$$

$$\text{(iii) } \varepsilon \sim \frac{u'^3}{l} = \frac{(0.323)^3}{0.07} = 0.481 \left(\frac{\text{m}^2}{\text{s}^2} \right) /$$

NETS IF A LINEAR DECAy AT THIS
RATE THE $u'^2 = 0$ WHEN $t = \frac{0.105}{0.481} = 0.21$
50000

$$(iv) \quad \frac{d}{dt} \frac{3}{2} u'^2 = - u'^3 / l$$

$$l = \text{constant} = 0.07 \text{ m}$$

$$k = \frac{3}{2} u'^2$$

$$\therefore \frac{dk}{dt} = - \left(\frac{2}{3} k \right)^{3/2} / l$$

$$k^{-3/2} dk = - \left(\frac{2}{3} \right)^{3/2} \frac{dt}{l}$$

$$-2 k^{-1/2} = - \left(\frac{2}{3} \right)^{3/2} t / l + \text{const.}$$

$$\therefore k^{-1/2} = \left(\frac{2}{3} \right)^{3/2} t / l + \text{const.}$$

$$\text{at } t=0 \quad k = k_0$$

$$\therefore k^{-1/2} = \left(\frac{2}{3} \right)^{3/2} t / l + k_0^{-1/2} \quad \left| \begin{array}{l} \text{LEAVE AS} \\ \text{SOLUTION IN} \\ \text{THIS FORM.} \end{array} \right.$$

$$\text{At } Re. = 100 ; \quad \frac{u' l}{\nu} = 100.$$

$$u' = \frac{100 \times 1 \times 10^{-6}}{0.07} = 1.43 \times 10^{-3} \text{ m/s.}$$

$$u'^2 = 2.04 \times 10^{-6} \text{ m}^2/\text{s}^2$$

$$\therefore k = \frac{3}{2} u'^2 = 3.06 \times 10^{-6} \text{ m}^2/\text{s}^3$$

$$\left\{ 3.06 \times 10^{-6} \right\}^{-1/2} = \left(\frac{2}{3} \right)^{3/2} t / l + \left(0.1575 \right)^{-1/2}$$

$$\downarrow$$

$$0.57 \times 10^3 = \frac{0.544}{0.07} t + 2.52$$

$$t = \frac{567.5 \times 0.07}{0.544} = 73.0 \text{ seconds.}$$

$$\begin{aligned}
 \text{(v)} \quad \text{Initially } \eta &= \left(\frac{\nu^3}{\varepsilon} \right)^{1/4} \\
 &= \left(\frac{(1 \times 10^{-6})^3}{0.481} \right)^{1/4} = 3.8 \times 10^{-5} \text{ m.}
 \end{aligned}$$

$$\begin{aligned}
 \text{Finally } \eta &= \left(\frac{\nu^3}{\varepsilon} \right)^{1/4} \\
 \varepsilon &= u'^3 / \ell = (0.00143)^3 / 0.07 \\
 \eta &= \left(\frac{(1 \times 10^{-6})^3 \times 0.07}{(0.00143)^3} \right)^{1/4} \\
 &= 2.21 \times 10^{-3}
 \end{aligned}$$

$$\begin{aligned}
 \text{(vi)} \quad \text{Temperature rise due to} \\
 \text{dissipation} &= \frac{3.92 \times 10^{-2} \text{ Joules}}{m C_p} \\
 &= \frac{3.92 \times 10^{-2} \text{ Joule}}{250 \times 10^{-6} \times 1000 \times 4,200 \text{ J/kg K}} \\
 &= 3.7 \times 10^{-6} \text{ Kelvin}
 \end{aligned}$$

