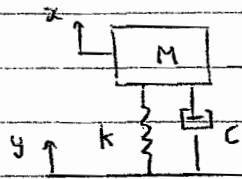


1) a)



$$M\ddot{x} + C(\dot{x} - \dot{y}) + k(x - y) = 0$$

$$\text{or } \ddot{x} + 2\beta\omega_n(\dot{x} - \dot{y}) + \omega_n^2(x - y) = 0 \quad \left. \begin{array}{l} \omega_n^2 = k/M \\ 2\beta\omega_n = c/M \end{array} \right\}$$

Put $r = x - y \Rightarrow \ddot{r} + 2\beta\omega_n\dot{r} + \omega_n^2 r = -\ddot{y}$

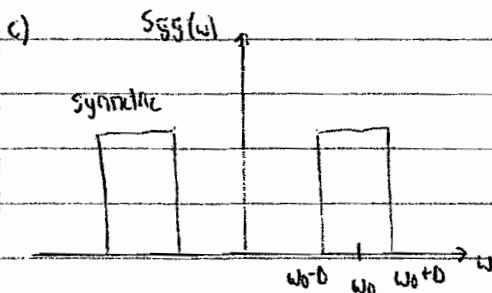
For ω_n within spectral bandwidth, $S_{\ddot{y}\ddot{y}}(\omega_n) = S_0 \leftarrow$ white noise approximation.

So, standard results for white noise excitation: $\sigma_r^2 = \frac{\pi S_0}{2\beta\omega_n^3}$ $\sigma_{\dot{r}}^2 = \frac{\pi S_0}{2\beta\omega_n}$

Power dissipated = Force \times velocity = $C \dot{r} \dot{r} \Rightarrow E[P] = C \sigma_{\dot{r}}^2 = \frac{C \pi S_0}{2\beta\omega_n} = M \pi S_0$ [30%]

b) Low damping \Rightarrow high response but low C } Mean square response $\propto \frac{1}{c}$ implies power
 High damping \Rightarrow low response but high C } is independent of C

For $C=0$ the response cannot be stationary and hence result does not hold. For $C \rightarrow 0$ the result will break down due to onset of non-linearity introduced by large response [20%]



$$S_{\dot{y}\dot{y}}(\omega) = \frac{1}{\omega^2} S_{yy}(\omega)$$

$$\sigma_{\dot{y}}^2 = \int_{-\infty}^{\infty} S_{\dot{y}\dot{y}}(\omega) d\omega = 2 \int_{\omega_0 - D}^{\omega_0 + D} \frac{1}{\omega^2} S_0 d\omega$$

$$\sigma_{\dot{y}}^2 = 2 \left[\frac{1}{\omega_0 - D} - \frac{1}{\omega_0 + D} \right] S_0 = \frac{4D}{\omega_0^2 - D^2} S_0$$

Power dissipated by $C_d = C_d \sigma_{\dot{y}}^2 = C_d \frac{4D}{\omega_0^2 - D^2} S_0 \rightarrow$ place equal to $M \pi S_0$

$$\Rightarrow C_d = \frac{M \pi S_0}{4D} (\omega_0^2 - D^2) \quad [25\%]$$

d) Probability that ω_n falls within $\omega_0 - \Delta$ to $\omega_0 + \Delta$ is $\frac{2\Delta}{\omega_0 + \Delta}$ ← interval
range of ω_n 's

Number of oscillators with ω_n in spectrum = $N \times \frac{2\Delta}{\omega_0 + \Delta}$

If ω_n is outside spectrum then response is small and power dissipation is negligible

Thus $E[P] = M T T S_0 \times \frac{2\Delta N}{\omega_0 + \Delta}$
↑ ↑ number of absorbers
From one absorber

⇒ $C_a = \frac{M T T S_0}{k D} (\omega_0^2 - \Delta^2) \times \left(\frac{2\Delta N}{\omega_0 + \Delta} \right) = \frac{M T T S_0}{Z} \underbrace{\left(\frac{N}{\omega_0 + \Delta} \right)}_{\text{"Modal density"}} (\omega_0^2 - \Delta^2)$ [25%]

- 2) a) Gap $r = x - y$ - For standard deviations assume all variables are adjusted to zero mean, i.e. r is gap - mean value

$$r^2 = x^2 + y^2 - 2xy \Rightarrow \sigma_r^2 = \sigma_x^2 + \sigma_y^2 - 2E[xy] = \sigma_x^2 + \sigma_y^2 - 2\rho_{xy}\sigma_x\sigma_y$$

Similarly $\sigma_{\bar{r}}^2 = \sigma_{\bar{x}}^2 + \sigma_{\bar{y}}^2 - 2\rho_{\bar{x}\bar{y}}\sigma_{\bar{x}}\sigma_{\bar{y}}$ [25%]

b) $v_b^+ = \left(\frac{1}{2\pi}\right)\left(\frac{\sigma_r}{\sigma_r}\right) e^{-\frac{1}{2}(b/\sigma_r)^2}$ with σ_r and $\sigma_{\bar{r}}$ as above.

For $\rho_{xy} \rightarrow 1$, $\sigma_r \rightarrow 0$. The term $\frac{1}{\sigma_r} \rightarrow \infty$, but the exponential $\rightarrow 0$ at a much faster rate

$\Rightarrow v_b^+ \rightarrow 0$ as $\rho_{xy} \rightarrow 1$

This makes physical sense: x and y are fully correlated and $x - y$ never changes [25%]

- c) Need to maximise $\sigma_r \Rightarrow \rho_{xy} = -1$ (bounded between -1 and 1, hence this is the lowest value). [10%]

d) $\sigma_r^2 = 2^2 + 4^2 - 2 \times 0.7 \times 2 \times 4 = 8.8 \Rightarrow \sigma_r = 2.96$

$\sigma_{\bar{r}}^2 = 0.6^2 + 1^2 - 2 \times 0.6 \times 1 \times 0.6 = 0.88 \Rightarrow \sigma_{\bar{r}} = 0.9381$

$v_b^+ = \frac{1}{2\pi} \left(\frac{\sigma_r}{\sigma_r}\right) e^{-\frac{1}{2}(b/\sigma_r)^2}$ with $b = 12 \Rightarrow v_b^+ = 1.504 \times 10^{-5}$

Failure probability $P_f = 1 - e^{-v_b^+ T} = 1 - e^{-1.504 \times 3 \times 60 \times 60} = 0.1507$ [20%]

- e) Factors: storm statistics

consequences of sea hitting deck - danger, cost of damage

cost of reducing probability

confidence in analysis

etc

Q3

$$\ddot{x} - \epsilon(1-x^4)\dot{x} + x = 0, \quad 0 < \epsilon \ll 1$$

zero order (set $\epsilon=0$)

$$\ddot{x}_0 + x_0 = 0$$

$$x_0 = A \cos t$$

1st order

$$\ddot{x}_1 + x_1 = \epsilon(1-x_0^4)\dot{x}_0$$

$$\ddot{x}_1 + x_1 = \epsilon(1-A^4 \cos^4 t)(A \sin t)$$

$$\ddot{x}_1 + x_1 = -A\epsilon \left(1 - A^4 \left[\frac{3 + 4 \cos 2t + \cos 4t}{8} \right] \right) \sin t$$

$$= -A\epsilon \sin t + \frac{A^5 \epsilon}{8} (3 \sin t)$$

$$+ \frac{A^5 \epsilon}{8} (4 \cos 2t \sin t + \cos 4t \sin t)$$

$$= -A\epsilon \sin t + \frac{A^5 \epsilon}{8} \cdot 3 \sin t$$

$$+ \frac{A^5 \epsilon}{8} \left(\frac{4}{2} (\sin 3t - \sin t) + \frac{1}{2} (\sin 5t - \sin 3t) \right)$$

$$= \sin t \left(-A\epsilon + \frac{1}{8} A^5 \epsilon \right) + \frac{A^5 \epsilon}{8} \sin 3t \left(\frac{3}{2} \right)$$

$$+ \frac{A^5 \epsilon}{16} \sin 5t$$

①

For a P.I. try!

$$x_1 = \alpha \sin 3t + \beta \sin 5t + \gamma t \cos t$$

$$x_1 = 3\alpha \cos 3t + 5\beta \cos 5t + \gamma \cos t - \gamma t \sin t$$

$$x_1 = -9\alpha \sin 3t - 25\beta \sin 5t - 2\gamma \sin t - \gamma t \cos t$$

$$x_1 + x_1 = -8\alpha \sin 3t - 24\beta \sin 5t - 2\gamma \sin t \quad \text{--- (2)}$$

equating (1) and (2) :

$$\alpha = \frac{-3 A^5 E}{128}$$

$$\beta = \frac{-A^5 E}{384}$$

$$\gamma = \frac{A E}{2} - \frac{A^5 E}{16}$$

solution to first order is found.

(ii) For a steady amplitude solution, the secular term in $\sin t$ must vanish or :-

$$\frac{A^5 E}{8} = A E$$

$$A^4 = 8$$

$$A = \sqrt[4]{8} = 1.68$$

Q4
(a)

$$\dot{x} + \left(x - \frac{\alpha}{\beta - x} \right) = 0$$

Transform equations to two first order differential

$$\begin{aligned} \dot{x} &= y \\ \dot{y} &= -x + \frac{\alpha}{\beta - x} \end{aligned}$$

Equilibrium points: $y = 0$ and $x = \frac{\alpha}{\beta - x}$

$$x(\beta - x) - \alpha = 0$$

$$x^2 - \beta x + \alpha = 0$$

Roots $x_{\pm} = \frac{\beta \pm \sqrt{\beta^2 - 4\alpha}}{2}$

Equilibrium points exist for

$$\alpha < \frac{\beta^2}{4}$$

(b) Linearise about equilibrium point

$$x = x_{\pm} + \epsilon_1$$

$$y = \epsilon_2$$

$$\dot{\epsilon}_1 = \epsilon_2$$

$$\dot{\epsilon}_2 \approx -\epsilon_1 + \frac{\alpha}{\beta - x_{\pm}} \epsilon_1$$

$A \in \mathbb{R}^{-1}$

The eigenvalues (λ) are given by (for characteristic matrix A)

$$\lambda^2 + 1 - \frac{\alpha}{(\beta - x_{\pm})^2} = 0$$

$$\lambda = \pm \sqrt{\frac{\alpha}{(\beta - x_{\pm})^2} - 1}$$

For equilibrium point $(0, x_+)$ it can be shown that $\frac{\alpha}{(\beta - x_+)^2} - 1 > 0$

\therefore Saddle point

equilibrium point $(0, x_-)$ is a centre as $\frac{\alpha}{(\beta - x_-)^2} - 1 < 0$.

(iii)

