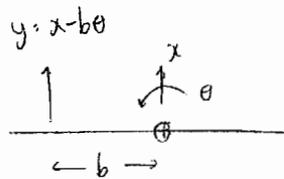


1. a)



$$y: x-b\theta \Rightarrow H_{yy} = H_{xy} - b H_{\theta y}$$

$$\Rightarrow \underline{H_{yy} = \alpha \omega - i b \beta / \omega}$$

[10%]

b) For acceleration $H_{\ddot{y}y} = -\omega^2 H_{yy}$

$$S_{\ddot{y}\ddot{y}}(\omega) = |H_{\ddot{y}y}|^2 S_{yy}(\omega) = \omega^4 [\alpha^2 \omega^2 + b^2 \beta^2 / \omega^2] S_{yy}(\omega)$$

$$\sigma_{\ddot{y}}^2 = S_0 \int_{\omega_1}^{\omega_2} \omega^4 [\alpha^2 \omega^2 + b^2 \beta^2 / \omega^2] d\omega$$

$$\underline{\sigma_{\ddot{y}}^2 = \frac{S_0 \alpha^2}{7} (\omega_2^7 - \omega_1^7) + \frac{S_0 b^2 \beta^2}{3} (\omega_2^3 - \omega_1^3)}$$

For \ddot{y} , $H_{\ddot{y}y} = -i\omega^3 H_{yy} \Rightarrow S_{\ddot{y}\ddot{y}}(\omega) = \omega^2 S_{yy}(\omega)$

$$\Rightarrow \underline{\sigma_{\ddot{y}}^2 = \frac{S_0 \alpha^2}{9} (\omega_2^9 - \omega_1^9) + \frac{S_0 b^2 \beta^2}{5} (\omega_2^5 - \omega_1^5)}$$

[40%]

c) For $S_0 = 30$, $\alpha = 0.4$, $\beta = 4 \times 10^{-3}$, $\omega_1 = 0.3$, $\omega_2 = 0.8$ then:

$$\sigma_{\ddot{y}}^2 = \frac{30 \times 0.4^2}{7} (0.8^7 - 0.3^7) + \frac{30 \times 50^2 \times (4 \times 10^{-3})^2}{3} (0.8^3 - 0.3^3)$$

$$\sigma_{\ddot{y}}^2 = 0.144 + 0.196 = \underline{0.338} \Rightarrow \underline{\sigma_{\ddot{y}} = 0.581 \text{ m/s}^2}$$

\uparrow \uparrow
 From heave From pitch

$$\text{Similarly: } \sigma_{\ddot{y}}^2 = 0.0715 + 0.07806 = \underline{0.149} \Rightarrow \underline{\sigma_{\ddot{y}} = 0.386 \text{ m/s}^3}$$

\uparrow \uparrow
 From heave From pitch

Probability of crossing $b = 1 - e^{-\lambda_b^+ \tau}$

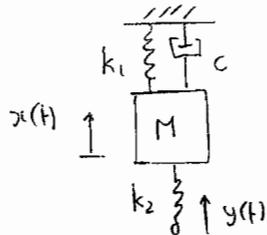
$$\lambda_b^+ = \left(\frac{1}{2\pi}\right) \left(\frac{\sigma_{\ddot{y}}}{\sigma_{\dot{y}}}\right) e^{-\frac{1}{2} \left(\frac{b}{\sigma_{\dot{y}}}\right)^2} \quad \text{with } b = 0.25 \times 10$$

$$u_b^+ = \frac{1}{2\pi} \left(\frac{0.386}{0.581} \right) e^{-\frac{1}{2} \left(\frac{0.25 \times 10}{0.581} \right)^2} = 1 \times 10^{-5}$$

$$P = 1 - e^{-1 \times 10^{-5} \times 3 \times 60 \times 60} = \underline{0.1} \Rightarrow 10\% \text{ probability of exceedance.}$$

[50%]

2. a)



$$M\ddot{x} + c\dot{x} + k_1x + k_2(x-y) = 0$$

$$M\ddot{x} + c\dot{x} + (k_1+k_2)x = k_2y$$

$$\ddot{x} + \underbrace{2\beta\omega_n}_{c/M}\dot{x} + \underbrace{\omega_n^2}_{(k_1+k_2)/M}x = (k_2/M)y$$

Take F.T. $\Rightarrow (-\omega^2 + 2i\beta\omega_n\omega + \omega_n^2)x(\omega) = (k_2/M)y(\omega)$

$$x(\omega) = \left[\frac{k_2/M}{-\omega^2 + 2i\beta\omega_n\omega + \omega_n^2} \right] y(\omega)$$

$\longleftarrow H(\omega) \longrightarrow$

$$S_{xx}(\omega) = |H(\omega)|^2 = \left[\frac{(k_2/M)^2}{(\omega_n^2 - \omega^2)^2 + (2\beta\omega_n\omega)^2} \right] S_{yy}(\omega) \quad [25\%]$$

b) Standard double-sided white noise result for $F = k_2y/M$: $\sigma_{\dot{x}}^2 = \frac{\pi S_0}{2\beta\omega_n^3}$ $\leftarrow S_{FF}(\omega)$, in this case $(k_2/M)^2 S_0$

$$\Rightarrow \sigma_{\dot{x}}^2 = \frac{\pi(k_2/M)^2 S_0}{2\beta\omega_n^3} = \frac{\pi(k_2/M)^2 S_0}{(c/M)(k_1+k_2)/M} = \frac{\pi k_2^2 S_0}{c(k_1+k_2)}$$

$$\sigma_{\ddot{x}}^2 = \omega_n^2 \sigma_{\dot{x}}^2 = \pi \left(\frac{k_1+k_2}{M} \right) \left(\frac{k_2^2 S_0}{c(k_1+k_2)} \right) = \frac{\pi k_2^2 S_0}{Mc} \quad [25\%]$$

c) For white noise, $\sigma_{\ddot{x}}^2$ is inversely proportional to stiffness (in this case k_1+k_2). The mean squared velocity is $\omega_n^2 \times$ this result, to give a result independent of stiffness. [15%]

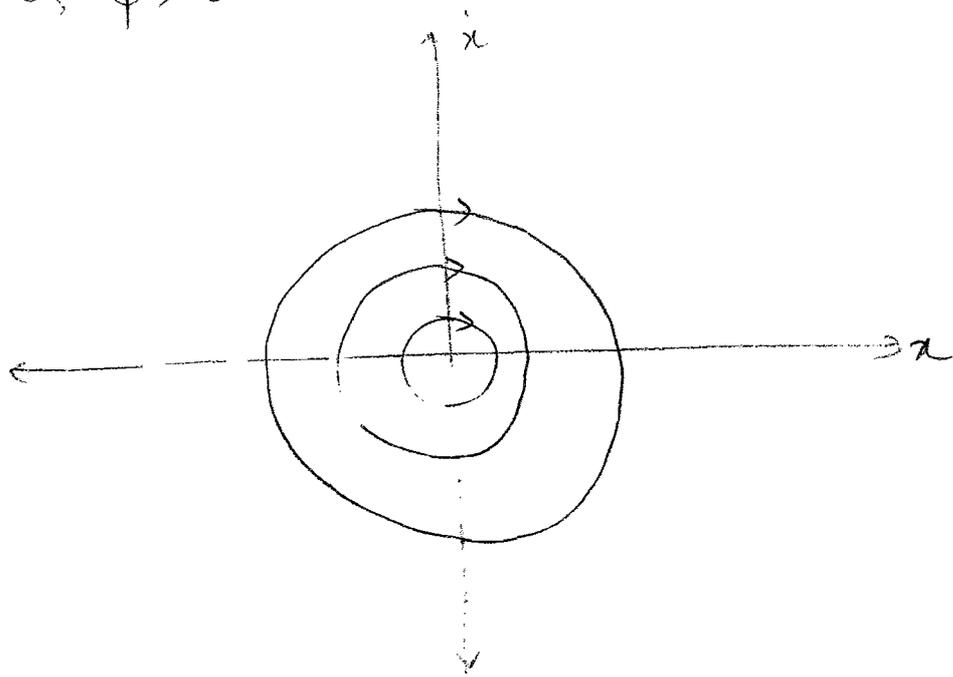
d) $P = \text{Power} = \text{damper force} \times \text{velocity} = c\dot{x} \times \dot{x} = c\dot{x}^2$

$$\Rightarrow E[P] = c E[\dot{x}^2] = c \sigma_{\dot{x}}^2 = \frac{c \pi k_2^2 S_0}{Mc} = \frac{\pi k_2^2 S_0}{M} \quad [35\%]$$

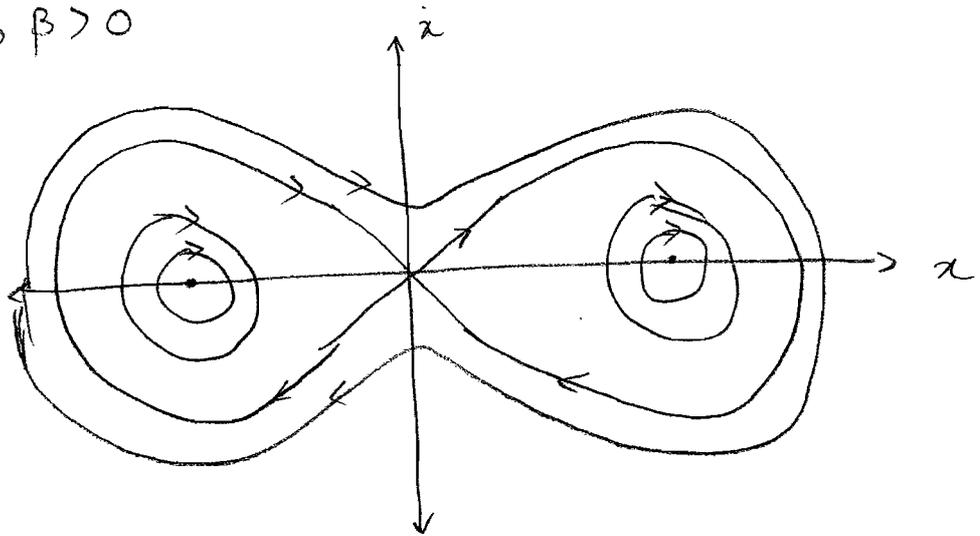
High damping \Rightarrow low velocity, but also high coefficient c ; effects cancel out to give a result independent of c . Does not happen for general $S_{yy}(\omega)$.

3

(a) $\alpha > 0, \beta > 0$



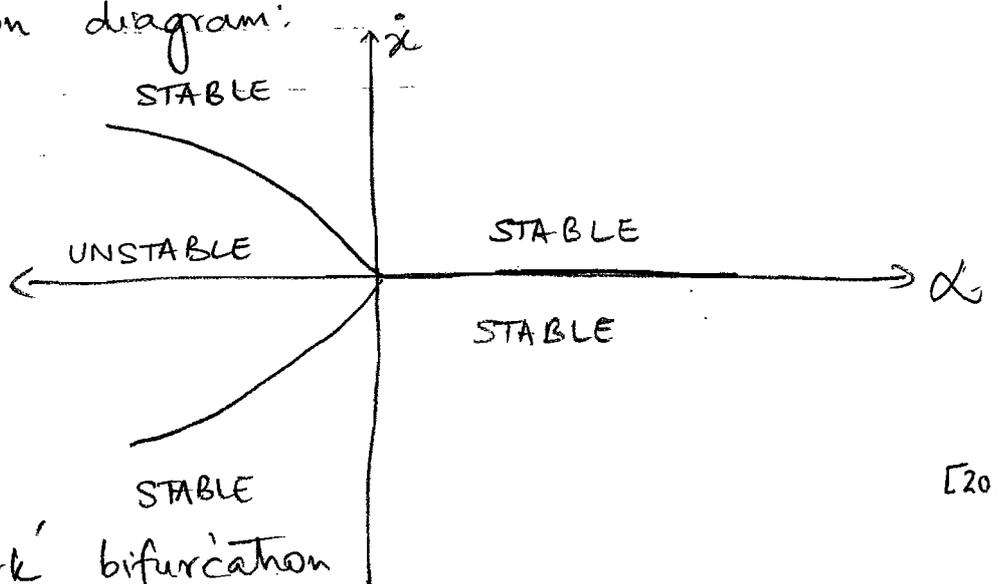
$\alpha < 0, \beta > 0$



[20%]

(b)

Bifurcation diagram:



∴ 'Pitchfork' bifurcation

[20%]

4.

$$\ddot{x} + \varepsilon \sin x + x = 0$$

(a)

Transform to 2 1st order differential equations to work out equilibrium points

$$\begin{aligned} \dot{x} &= y \\ \dot{y} &= -\varepsilon \sin y - x \end{aligned}$$

equilibrium points when $\dot{x} = \dot{y} = 0$
 $\Rightarrow x = 0, y = 0$ is an equilibrium point

(b) Linearising about $x = 0, \dot{x} = 0$

$$A = \begin{bmatrix} 0 & 1 \\ -1 & -\varepsilon \end{bmatrix}$$

Eigenvalues of A :

$$\begin{vmatrix} -\lambda & 1 \\ -1 & -\varepsilon - \lambda \end{vmatrix} = 0$$

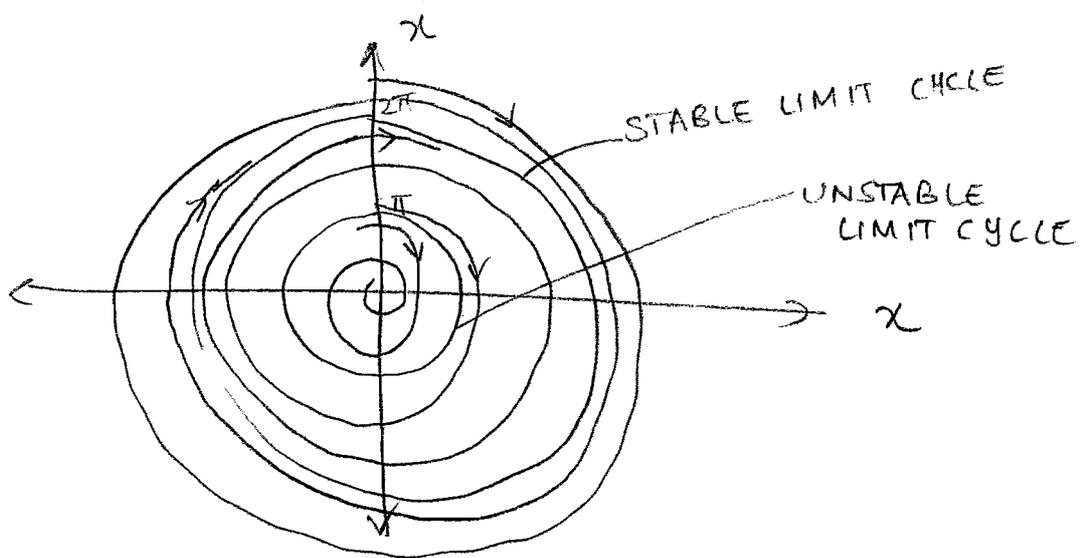
$$\Rightarrow \lambda^2 + \varepsilon\lambda + 1 = 0$$

$$\lambda = \frac{-\varepsilon \pm \sqrt{\varepsilon^2 - 4}}{2}$$

For $0 < \varepsilon < 1$, λ is complex with negative real part \therefore stable spiral

(c) For $0 < x < \pi$, damping is positive and amplitude decays
 $\pi < x < 2\pi$, damping is negative and amplitude grows
 $2\pi < x < 3\pi$, damping is positive and amplitude decays

and so there is a periodicity of 2π in the damping. This suggests an infinite set of limit cycles in the phase plane. LIMIT CYCLE is stable when all neighbourhood trajectories converge to it. There is now the possibility of an infinite set of limit cycles, the first is unstable, the second stable, the third unstable and so on.



(d) If ϵ is negative, $|\epsilon| < 1$, the structure of phase plane remains the same but stability of limit cycles is reversed.