

ENGINEERING TRIPOS PART IIA

Thursday 6 May 2010 2.30-4.00

Module 4A13

COMBUSTION AND IC ENGINES

*Answer not more than **three** questions.*

All questions carry the same number of marks.

*The **approximate** percentage of marks allocated to each part of a question is indicated in the right margin.*

There are no attachments.

STATIONERY REQUIREMENTS

Single-sided script paper

SPECIAL REQUIREMENTS

Engineering Data Book

CUED approved calculator allowed

**You may not start to read the questions
printed on the subsequent pages of this
question paper until instructed that you
may do so by the Invigilator**

1 Consider a laminar flame of a hydrocarbon in an oxygen-carbon dioxide mixture. The reaction of the hydrocarbon in a flame is approximated as a one-step reaction $F + O \rightarrow P$, where F denotes the fuel, O , the oxidiser, and P the product. Reactants flow from left ($x = -\infty$) to products on the right ($x = +\infty$).

(a) Starting from the one dimensional energy equation for constant specific heat and conductivity:

$$\dot{m}c_p \frac{dT}{dx} - \lambda \frac{d^2T}{dx^2} - wQ = 0$$

where T is the temperature, \dot{m} , the mass flow rate per unit area, c_p , the specific heat capacity at constant pressure, x , the streamwise coordinate, λ , the mixture thermal conductivity, w , the mass reaction rate per unit volume and Q , the heat of combustion per unit mass. Show that the temperature gradient at the downstream edge of the preheat zone ($x = 0^-$) is given as:

$$\left(\frac{dT}{dx}\right)_{x=0^-} = \frac{\dot{m}c_p}{\lambda}(T(0^-) - T_R)$$

where T_R is the temperature of the reactants. Explain in detail all assumptions made regarding the different terms, and the appropriate boundary conditions. [20%]

(b) Starting from the same equation, show that at the upstream edge of the the reaction zone ($x = 0^+$), we have:

$$\left(\frac{dT}{dx}\right)_{x=0^+}^2 = 2\frac{Q}{\lambda} \int_{T(0^+)}^{T_P} w dT$$

where T_P is the temperature of the products. Explain in detail all assumptions made, and the appropriate boundary conditions. [20%]

(c) Show that the premixed laminar flame speed u_L is given by:

$$u_L = \left(\frac{2\lambda}{\rho_R^2 c_p (T_P - T_R)} \int_{T_0}^{T_P} w dT \right)^{\frac{1}{2}}$$

where T_0 is the temperature of the interface between the premixed and reaction zone and ρ_R is the density of the reactants. Explain in detail all assumptions made. [20%]

(d) If the reaction rate is given by the expression $w = A \exp(-E/(RT))$, where E and R are constants, explain how a closed form expression can be obtained for the reaction rate as:

$$u_L = \left[\frac{2\lambda A}{\rho_R^2 c_p (T_P - T_R)} \frac{RT_P^2}{E} \exp\left(-\frac{E}{RT_P}\right) \right]^{\frac{1}{2}}$$

[20%]

(e) Using the expression above and physical interpretation, explain how the laminar flame speed of a hydrocarbon/oxygen/carbon dioxide flame should vary with the ratio of oxygen and carbon dioxide in the mixture. Why would one want to use such a mixture in a combustor?

[20%]

2 Consider a non-premixed flamelet, which can be characterised parametrically as a strained non-premixed flame. The mixture fraction is defined as $Z = (\beta - \beta_2)/(\beta_1 - \beta_2)$, where $\beta = sY_F - Y_O$, 1 and 2 are the two different streams, Y_F and Y_O the mass fractions of fuel and air, and s the mass stoichiometric coefficient.

(a) Determine the stoichiometric mixture fraction Z_s for (i) streams of methane (CH_4) on one side and pure air on the other, (ii) methane on one side and pure oxygen on the other. [20%]

(b) The simplified balance equation for the mixture fraction balance in a two-dimensional opposed flame along the symmetry axis y is given as:

$$\rho v \frac{\partial Z}{\partial y} = \frac{\partial}{\partial y} \left(\rho D \frac{\partial Z}{\partial y} \right)$$

where Z is the mixture fraction. The diffusion coefficient, D , and the density, ρ , are assumed to be constant. The axial velocity v is given as $v = -ay$, where a is the constant strain rate. The mixture fraction at either boundary is equal to the free stream value. Show that it is possible to reduce the equation to:

$$\frac{\partial^2 Z}{\partial \eta^2} + 2\eta \frac{\partial Z}{\partial \eta} = 0$$

where $\eta = y/\sqrt{(2D/a)}$. [30%]

(c) Show that the solution of the equation for the mixture fraction, subject to the boundary conditions where the fuel stream is on the $y \rightarrow -\infty$ side, and the oxidizer on the $y \rightarrow +\infty$ side, is:

$$Z = \frac{1}{2}[1 - \text{erf}(\eta)]$$

where $\text{erf}(\eta) = \frac{2}{\sqrt{\pi}} \int_0^\eta \exp(-u^2) du$, $\text{erf}(-\infty) = -1$ and $\text{erf}(+\infty) = 1$. [20%]

(d) Carefully sketch the mixture fraction profile and the location of the flame as shown in the solution in (c) for methane-air and methane-oxygen flamelets, indicating the respective flame locations. [15%]

(e) Sketch the temperature, fuel and oxygen profile for one of the cases in (d). [15%]

3 Write brief notes which would convey to an engineer not versed in IC engine technology why the following statements are true:

- (a) A throttle is required to vary the load of gasoline engines. [15%]
- (b) The crank angle over which combustion takes place is roughly independent of engine speed for gasoline engines. [15%]
- (c) The bore sizes of most automotive gasoline engines are similar. [20%]
- (d) Diesel engines of a similar power output typically have a better sfc than gasoline engines. [20%]
- (e) Large cylinder volume diesel engines have a better specific fuel consumption rate than small cylinder volume engines. [15%]
- (f) Turbochargers are useful, but have disadvantages. [15%]

4 Automobiles that use a compressed air reservoir as the energy supply are in small scale production. A reciprocating expander is used to extract mechanical work from the reservoir and propel the vehicle. The expander consists of a single piston-in-cylinder arrangement (see Fig. 1), where the maximum cylinder volume is V_{max} .

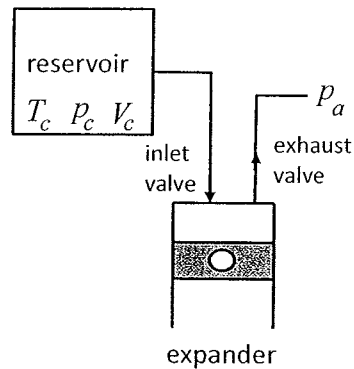


Fig. 1

The cycle proceeds as follows:

Charge: at the minimum cylinder volume, *assumed negligible*, the inlet valve opens which admits compressed air from the reservoir, at a pressure and temperature of p_c , T_c , respectively, into the cylinder, and the inlet valve closes when the volume is αV_{max} .

Expansion: the trapped air, assumed initially to be at p_c , T_c , is expanded adiabatically and reversibly to V_{max} . The value of α can be varied (i.e. the inlet valve closing time), so that whatever the value of p_c , the pressure at the end of the expansion is always p_a , the ambient pressure.

Exhaust: the exhaust valve opens, which allows the air to be ejected to ambient during the return to the minimum volume position. The exhaust valve then closes.

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(cont.)

(a) Sketch the cycle on a $p - V$ diagram. [10%]

(b) Show that $\alpha = \left(\frac{p_a}{p_c}\right)^{(1/\gamma)}$. [10%]

(c) Show that the work done during each revolution of the engine, W , is given by:

$$W = p_a V_{max} \frac{\gamma}{\gamma - 1} \left[\left(\frac{p_c}{p_a}\right)^{(\gamma-1)/\gamma} - 1 \right]$$

[30%]

(d) Find an expression for the air mass flow rate leaving the reservoir if the engine is rotating at N rev/sec as a function of the parameters defined above. [10%]

(e) The engine is required to maintain a constant power output of 5 kW. This means that the engine rotation speed varies from a low value, when p_c (and thus the work per cycle) is high, to the maximum engine speed, N_{max} , when the minimum p_c that will still deliver 5 kW is reached. Assume T_c remains constant at 25 °C, $p_a = 1$ bar, $V_{max} = 1$ litre and $N_{max} = 100$ rev/s.

(i) What is the minimum value of p_c that will deliver 5 kW? [20%]

(ii) If the compressed air reservoir has a volume V_c of 340 litres and p_c is initially 300 bar, find the maximum trip duration, assuming that the delivered power remains constant.

[20%]

END OF PAPER