ENGINEERING TRIPOS PART IIB

Friday 27 April 20129 to 10.30

Module 4A15

## AEROACOUSTICS

Answer not more than three questions.
All questions carry the same number of marks.
The approximate percentage of marks allocated to each part of a question is indicated in the right margin.

Attachments: 4A15 data sheet (6 pages).

STATIONERY REQUIREMENTS
Single-sided script paper

SPECIAL REQUIREMENTS
Engineering Data Book
CUED approved calculator allowed

4A15, 2012, Answers
Q1
(a) -
(b) -
(c) -

Q2
(a) -
(b)

Q3
(a) -
(b) -
(c)

Q4
(a) Porosity $=0.1$
(b) Hole diameter $=0.0177 \mathrm{~m}$.

1 A source $S$ of spherical waves of angular frequency $\omega$ is located at the centre of a helium-filled spherical balloon of radius $a$ as shown in Fig. 1. The balloon is surrounded by air. The values of density and speed of sound are respectively, $\rho_{1}$ and $c_{1}$ inside the balloon and $\rho_{2}$ and $c_{2}$ outside the balloon. The incident, reflected, and transmitted waves may be represented respectively by

$$
\begin{aligned}
& p_{i}^{\prime}(r, t)=\frac{A}{r} \exp \left[i \omega\left(t-(r-a) / c_{1}\right)\right] \\
& p_{r}^{\prime}(r, t)=\frac{B}{r} \exp \left[i \omega\left(t+(r-a) / c_{1}\right)\right] \\
& p_{t}^{\prime}(r, t)=\frac{C}{r} \exp \left[\mathrm{i} \omega\left(t-(r-a) / c_{2}\right)\right]
\end{aligned}
$$

where $r$ denotes the radial distance and $t$ the time.
(a) Show that the corresponding radial velocity fields are given by

$$
\begin{align*}
v_{i}^{\prime}(r, t) & =\frac{1-\mathrm{i} c_{1} /(\omega r)}{Z_{1}} p_{i}^{\prime}(r, t) \\
v_{r}^{\prime}(r, t) & =-\frac{1+\mathrm{i} c_{1} /(\omega r)}{Z_{1}} p_{r}^{\prime}(r, t) \\
v_{t}^{\prime}(r, t) & =\frac{1-\mathrm{i} c_{2} /(\omega r)}{Z_{2}} p_{t}^{\prime}(r, t)
\end{align*}
$$

where $Z_{1}=\rho_{1} c_{1}$ and $Z_{2}=\rho_{2} c_{2}$.
(b) By applying the appropriate boundary conditions on the surface of the balloon, show that the pressure reflection coefficient is given by

$$
R=\frac{p_{r}^{\prime}(a, t)}{p_{i}^{\prime}(a, t)}=\frac{\left(1-Z_{1} / Z_{2}\right)-\mathrm{i} \alpha_{1}\left(1-\rho_{1} / \rho_{2}\right)}{\left(1+Z_{1} / Z_{2}\right)+\mathrm{i} \alpha_{1}\left(1-\rho_{1} / \rho_{2}\right)}
$$

where $\alpha_{1}=c_{1} /(\omega a)$.
(c) Use this result to show that for a compact balloon the transmitted pressure is small in comparison with $p_{i}^{\prime}$ and $p_{r}^{\prime}$ on $r=a$.


Fig. 1

2 Consider a low Mach-number, isentropic cold turbulent jet.
(a) By finding the sound radiated from a single compact eddy, show that the acoustic far-field density from the eddy scales as

$$
\rho^{\prime} \sim \rho_{0} \frac{x_{i}}{x} \frac{x_{j}}{x} \frac{l}{x} m^{4}
$$

where $\rho_{0}$ is the ambient density, $x$ is the distance from the source to the observer, $x_{i}$ represents the component of $\mathbf{x}$ in the $i$-direction, $l$ is the length scale of the eddy, $m=u^{\prime} / c_{0}, u^{\prime}$ is the velocity scale of the eddy and $c_{0}$ represents the speed of sound.

Hint: $\frac{\partial^{2}}{\partial x_{i} \partial x_{j}} \int T_{i j}\left(\mathbf{y}, t-\frac{x}{c_{0}}\right) \mathrm{d} \mathbf{y}=\frac{1}{c_{0}^{2}}\left(\frac{x_{i} x_{j}}{x^{2}}\right) \frac{\partial^{2}}{\partial t^{2}} \int T_{i j}\left(\mathbf{y}, t-\frac{x}{c_{0}}\right) \mathrm{d} \mathbf{y}$
(b) Use this result to deduce an expression for the acoustic power radiated by the jet (Lighthill's eighth power law).

3 The acoustic pressure for a plane sound wave with an angular frequency $\omega$ and wavenumber $k_{0}$ is given by

$$
p^{\prime}=p_{i} \exp \left(\mathrm{i} \omega t-\mathrm{i} k_{0} y\right)
$$

The sound wave is incident on to a thin rigid plate, which is between $\{-L<x<L, y=0\}$, with $k_{0} L \gg 1$.
(a) Calculate the acoustic pressure along the line $x=0, y>0$.
(b) Sketch a graph of the variation of the acoustic pressure with $x$ along the lines $y=-H$ and $y=+H$, where $H \gg L$. (detailed calculations are not required)
(c) Explain briefly how your answer to (b) would change if the thin rigid plate were replaced by a rigid circular cylinder of radius $L$.

4 (a) A Helmholtz resonator has a bulb of volume $V$, a neck of cross-sectional area $A$ and effective length $l$ as shown in Fig. 2. Viscous and flow separation effects cause a pressure drop of $\rho_{0} c_{0} \alpha u_{1}^{\prime}(t)$ across the neck of the Helmholtz resonator, where $\rho_{0}$ is the mean density, $c_{0}$ is the speed of sound, $u_{1}^{\prime}(t)$ is the unsteady air velocity into the neck of the Helmholtz resonator and $\alpha$ is a constant. Show that for perturbations of frequency $\omega, u_{1}^{\prime}(t)$ is related to $p_{1}^{\prime}(t)$ the pressure perturbation at the neck of the Helmholtz resonator by

$$
p_{1}^{\prime}(t)=\rho_{0} u_{1}^{\prime}(t)\left(\frac{c_{0}^{2} A}{V \mathrm{i} \omega}+l \mathrm{i} \omega+c_{0} \alpha\right)
$$

(b) An aeroengine acoustic liner has circular holes of radius $a$, porosity (i.e. open area ratio) $\beta$ and a honeycomb structure with cavity depth $d$ as shown in Fig. 3. Each cavity within the honeycomb can be treated as a Helmholtz resonator as modelled by the above equation with $\alpha=0.1$. The walls of the honeycomb are rigid but very thin and the effective neck length of each hole is $1.2 a$. If $d=0.05 \mathrm{~m}$, what porosity and hole radius would you choose to absorb all the energy in a normally incident plane sound wave of frequency 750 Hz ? Take $\rho_{0}=1.2 \mathrm{~kg} \mathrm{~m}^{-3}$ and $c_{0}=343 \mathrm{~ms}^{-1}$.


Fig. 2


Fig. 3

## END OF PAPER

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