#### EGT3

### **ENGINEERING TRIPOS PART IIB**

27 April 2017 2 to 3.30

### **Module 4C2**

## **DESIGNING WITH COMPOSITES**

Answer not more than three questions.

All questions carry the same number of marks.

The approximate percentage of marks allocated to each part of a question is indicated in the right margin.

Write your candidate number <u>not</u> your name on the cover sheet.

# STATIONERY REQUIREMENTS

Single-sided script paper

# SPECIAL REQUIREMENTS TO BE SUPPLIED FOR THIS EXAM

CUED approved calculator allowed

Attachment: Module 4C2 Designing with Composites data sheet (6 pages).

**Engineering Data Book** 

10 minutes reading time is allowed for this paper.

You may not start to read the questions printed on the subsequent pages of this question paper until instructed to do so.

- 1 (a) Explain what is meant by "a *balanced* laminate". Show that a  $\pm \phi$  "angle-ply" laminate, with a ply thickness t/2, is balanced when loaded at an angle equally inclined to the  $+\phi$  and  $-\phi$  plies. [30%]
- (b) A small aircraft is being designed and an angle-ply fibre-glass polyester composite is being used for the fuselage. The fuselage, which will approximate to a thin-walled cylinder with closed ends of outside diameter D=2 m is subjected to an internal pressure P and a bending moment M as shown in Fig. 1. The fuselage is produced by filament winding at  $\pm 45^{\circ}$  to the longitudinal axis of the fuselage. A total of 100 layers of  $\pm 45^{\circ}$  fibres and 100 layers of  $\pm 45^{\circ}$  fibres are laid down, giving a total wall thickness t. Each layer has the following properties:  $E_2 = 0.2E_1$ ,  $G_{12} = 0.09E_1$  and  $v_{12} = 0.3$ .
  - (i) Find the stiffness matrix [Q] for each ply in the principal material axes (1, 2) in terms of  $E_1$ . [15%]
  - (ii) Find the extensional stiffness matrix [A] for the wall material in terms of  $E_1$  and t, in axes (x,y) aligned with those of the cylinder. [25%]
  - (iii) Find the strains ( $\varepsilon_x$ ,  $\varepsilon_y$ ,  $\gamma_{xy}$ ) induced in the tensile outer surface of the fuselage when it is subjected to an internal pressure of 0.06 MPa and a bending moment of 500 kN m. [30%]

[The second moment of area of a thin-walled cylinder is given by  $\pi R^3 t$ .]

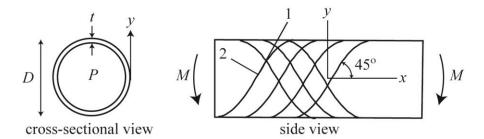


Fig. 1

- Table 1 gives the stiffness properties of three laminates made from four plies of a CFRP prepreg material, where the laminate x and y axes coincide with the  $0^{\circ}$  and  $90^{\circ}$  directions respectively. Table 1 also includes the measured first-ply failure stress for tensile loading along the laminate x direction.
- (a) Show that the given failure stresses are consistent with lamina failure strains of  $\varepsilon_L^+ = 0.010$ ,  $\varepsilon_T^+ = 0.0050$ ,  $\varepsilon_L^- = 0.020$  and  $\varepsilon_T^- = 0.010$ . What are the corresponding expected failure modes for each of the laminates? [20%]
- (b) Use the failure strains given in part (a) to predict the magnitude of equal tensile stresses applied in the *x* and *y* directions (i.e. a biaxial loading) which would cause first ply failure for each of the three laminates. [25%]
- (c) For the cross-ply laminate given in Table 1, use the lamina failure stresses given on the datasheet for AS/3501 to predict the biaxial tensile stress loading, as per part (b), which would cause failure according to the Tsai-Hill failure criterion. [35%]
- (d) Describe suitable tests to measure the uniaxial and biaxial tensile strength of such laminates. [20%]

Laminate	$[0_4]$	$[0,90]_s$	[90 <sub>4</sub> ]
$E_x$ (GPa)	138	74	9.0
$E_y$ (GPa)	9.0	74	138
<i>V</i> <sub>xy</sub> (−)	0.30	0.037	0.020
Failure stress (MPa)	1400	370	45

Table 1

- 3 (a) Derive an expression for the compressive strength associated with plastic microbuckling of a unidirectional composite with initial fibre misalignment angle  $\phi_0$  and matrix shear yield strength  $\tau_V$ . Detail any assumptions made in your derivation. [15%]
- (b) Describe, with the aid of a sketch, the pultrusion process. [15%]
- (c) Explain why the compressive strength of pultruded unidirectional CFRP might be significantly greater than that of equivalent moulded material. [10%]
- (d) Discuss the factors that contribute to the increasing use of GFRP pultruded composites for bridge construction. [20%]
- (e) Figure 2 illustrates a hollow square-section GFRP composite beam of uniform layup and wall thickness t. The side length d of the section, which can be assumed to be large compared with t, equals 100 mm. The beam of length 3 m is mounted as a cantilever, rigidly fixed to a wall. A transverse load F = 30 N and a torsional load Q = 80 N m are applied simultaneously to the free end of the cantilever. Use the carpet plots provided in Fig. 3 to select an appropriate ply mix and thickness for a laminate containing a mixture of  $0^{\circ}$ ,  $90^{\circ}$  and  $\pm 45^{\circ}$  plies which minimise the mass of the beam, while ensuring that the end deflection is less than 2 mm and the end rotation is less than  $0.2^{\circ}$  under the applied loading. [40%]

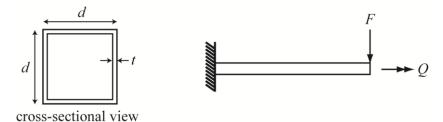


Fig. 2

(cont.

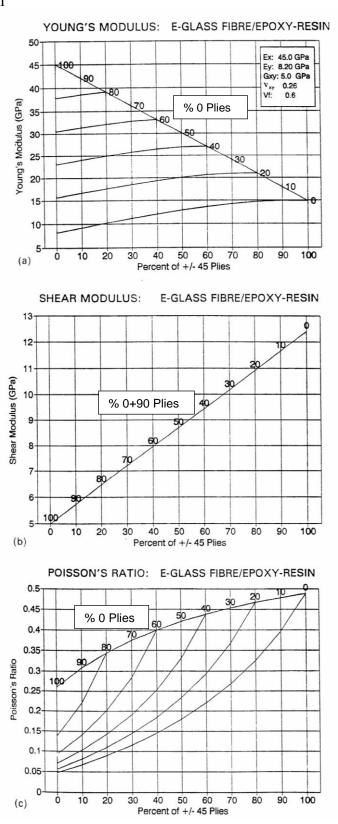


Fig. 3

## Version AEM/final

- 4 (a) Discuss the design and manufacture of composite garden furniture. Include the following points in your discussion: material and layup, manufacturing route, structural design and any other relevant aspects. [45%]
- (b) Figure 4 illustrates a semi-circular unidirectional composite beam of radius R, thickness t and depth b (out of the plane of the figure) subjected to end loads P. Stress concentration effects at the loading points can be neglected.
  - (i) Derive an expression for the maximum through-thickness stress in the beam in terms of P, R, b and t. [20%]
  - (ii) Predict the load P which will cause failure of a beam made of AS/3501 (data on datasheet) with R = 800 mm, b = 60 mm and t = 20 mm. Detail any assumptions made. [20%]
- (c) Discuss when through-thickness stresses in composites are of concern for predicting failure. [15%]

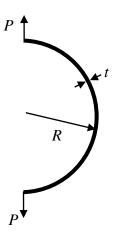


Fig. 4

## **END OF PAPER**

#### **Answers**

1. (b)(i) 
$$[Q] = E_1 \begin{bmatrix} 1.02 & 0.06 & 0\\ 0.06 & 0.20 & 0\\ 0 & 0 & 0.09 \end{bmatrix}$$

(b)(ii) 
$$[A] = tE_1 \begin{bmatrix} 0.43 & 0.25 & 0\\ 0.25 & 0.43 & 0\\ 0 & 0 & 0.28 \end{bmatrix}$$
  
(b)(iii)  $\begin{pmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{pmatrix} = \frac{1}{tE_1} \begin{pmatrix} 5.4 \times 10^{-4} \\ -1.8 \times 10^{-4} \\ 0 \end{pmatrix}$ 

(b)(iii) 
$$\begin{pmatrix} \varepsilon_{x} \\ \varepsilon_{y} \\ \gamma_{xy} \end{pmatrix} = \frac{1}{tE_{1}} \begin{pmatrix} 5.4 \times 10^{-4} \\ -1.8 \times 10^{-4} \\ 0 \end{pmatrix}$$

$$[0_4] \ \sigma = 46 \text{ MPa};$$

2. (b) 
$$[0,90]_s$$
  $\sigma = 380 \text{ MPa};$   $[90_4]$   $\sigma = 46 \text{ MPa}.$ 

(c) 
$$\sigma = 290 \text{ MPa}$$

4. (b)(i) 
$$\sigma_z = \frac{3P}{2bt}$$
, (b)(ii)  $P = 5860 \text{ N}$