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ENGINEERING TRIPOS PART IB

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Paper 7

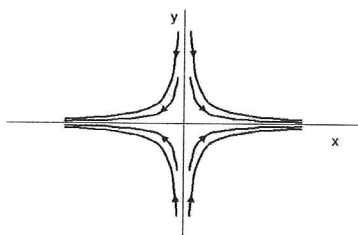
MATHEMATICAL METHODS

*Solutions*

## SECTION A

- 1 (a) Field lines obey  $\frac{dy}{dx} = \frac{u_y}{u_x}$ . Therefore:

$$\begin{aligned} \frac{dy}{dx} = \frac{u_y}{u_x} &\Leftrightarrow \frac{dy}{dx} = -\frac{Sy}{Sx} \Leftrightarrow \frac{dy}{y} = -\frac{dx}{x} \\ &\Leftrightarrow \int \frac{dy}{y} = -\int \frac{dx}{x} \Leftrightarrow \ln y = -\ln x + C' \\ &\Leftrightarrow y = \frac{C}{x} \end{aligned}$$



- (b) Solenoidal if  $\nabla \cdot \mathbf{u} = 0$  and irrotational if  $\nabla \times \mathbf{u} = 0$ .

$$\nabla \cdot \mathbf{u} = \frac{\partial(Sx)}{\partial x} + \frac{\partial(-Sy)}{\partial y} = S - S = 0$$

$$\nabla \times \mathbf{u} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ Sx & -Sy & 0 \end{vmatrix} = 0$$

QED

- (c) Scalar potential,  $\phi$ , for  $\mathbf{u}$  is such that  $\mathbf{u} = \nabla\phi$ . Therefore:

$$\frac{\partial\phi}{\partial x}\mathbf{i} + \frac{\partial\phi}{\partial y}\mathbf{j} = (Sx)\mathbf{i} - (Sy)\mathbf{j}$$

For the x-component:

$$\frac{\partial\phi}{\partial x} = Sx \Leftrightarrow \phi = \frac{S}{2}x^2 + f_x(x)$$

(cont.)

For the y-component:

$$\frac{\partial \phi}{\partial y} = -Sy \Leftrightarrow \phi = -\frac{S}{2}y^2 + f_y(y)$$

$$\text{so } \phi = \frac{S}{2}(x^2 - y^2) + K.$$

The line integral between two points can be found from the difference between the scalar potential at these points and is hence:

$$\int \mathbf{u} \cdot d\mathbf{l} = \phi(\sqrt{2/S}, 1/\sqrt{S}) - \phi(0, 0) = \left[ \frac{S}{2} \left( \frac{2}{S} - \frac{1}{S} \right) + K \right] - \left[ \frac{S}{2}(0 - 0) + K \right] = \frac{1}{2}$$

(d) The position  $(X, Y)$  of the particle obeys  $dX/dt = u_x$  and  $dY/dt = u_y$ , therefore:

$$\frac{dX}{dt} = SX \Leftrightarrow X = X_0 e^{St}$$

$$\frac{dY}{dt} = -SY \Leftrightarrow Y = Y_0 e^{-St}$$

Therefore after a time  $t$  the distance  $r$  between the two particles released from  $(X_0, Y_0)$  and  $(X_0 + r_0, Y_0)$  will be:

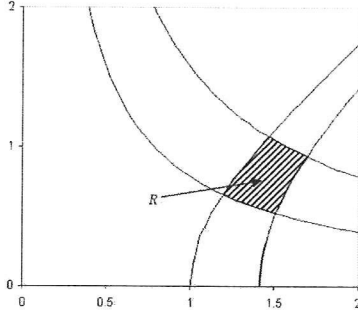
$r = (X_0 + r_0)e^{St} - X_0 e^{St} \Leftrightarrow r = r_0 e^{St}$ . Differentiating w.r.t  $t$  gives  $dr/dt = Sr_0 e^{St}$ , i.e.  $dr/dt = rS$ . QED.

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- 2 (a) If  $r = x$  and  $s = y$ , then the given identity becomes

$$1 = \frac{\partial(x,y)}{\partial(u,v)} \frac{\partial(u,v)}{\partial(x,y)} \Leftrightarrow \frac{\partial(x,y)}{\partial(u,v)} = \left[ \frac{\partial(u,v)}{\partial(x,y)} \right]^{-1}$$

- (b) Curve sketching: consider behaviour as  $x, y \rightarrow \infty$ , find  $x$  when  $y = 0$  etc.



- (c) The transformation  $x^2 - y^2 = u$ ,  $2xy = v$  suggests itself. Then, the limiting curves become:  $x^2 - y^2 = 1 \Rightarrow u = 1$ ;  $x^2 - y^2 = 2 \Rightarrow u = 2$ ;  $2xy = \pi/2 \Rightarrow v = \pi/2$ ; and  $2xy = \pi \Rightarrow v = \pi$ .

To calculate the integral, we need to calculate the Jacobian  $\left| \frac{\partial(x,y)}{\partial(u,v)} \right|$ . Since we do not have explicitly  $x$  and  $y$  as functions of  $u$  and  $v$  (we can get such expressions, but the algebra is messy), we use the result from part (a). Therefore:

$$\left| \frac{\partial(u,v)}{\partial(x,y)} \right| = \left| \begin{array}{cc} \frac{\partial u}{\partial x} & \frac{\partial v}{\partial x} \\ \frac{\partial u}{\partial y} & \frac{\partial v}{\partial y} \end{array} \right| = \left| \begin{array}{cc} 2x & 2y \\ -2y & 2x \end{array} \right| = 4(x^2 + y^2)$$

The integrand becomes:  $4(x^4 - y^4) \sin(2xy) = 4(x^2 + y^2) u \sin(v)$ . Therefore the integral  $I = \iint 4(x^4 - y^4) \sin(2xy) dx dy$  becomes:

$$\begin{aligned} I &= \int \int 4(x^2 + y^2) u \sin(v) \frac{1}{4(x^2 + y^2)} du dv = \int_1^2 u du \int_{\pi/2}^{\pi} \sin(v) dv \\ &= \left[ \frac{u^2}{2} \right]_1^2 [-\cos(v)]_{\pi/2}^{\pi} \\ &= \frac{3}{2} \end{aligned}$$

NOTE: Some books define the Jacobian matrix  $\begin{bmatrix} \frac{\partial u}{\partial x} & \frac{\partial u}{\partial y} \\ \frac{\partial v}{\partial x} & \frac{\partial v}{\partial y} \end{bmatrix}$ , which has the same determinant as the Jacobian we use in our course.

3 (a) If  $A$  is an area enclosing a volume  $V$ , and if  $\mathbf{n}$  is the normal vector pointing *outwards*, then Gauss's theorem for the heat flux vector  $\mathbf{q}$ , using  $\mathbf{q} = -\lambda \nabla T$ , gives for the overall heat flow *out* of  $V$ :

$$\begin{aligned} \iint_A \mathbf{q} \cdot \mathbf{n} dA &= \iiint_V \nabla \cdot \mathbf{q} dV \\ &= - \iiint_V \lambda \nabla^2 T dV \end{aligned}$$

But this must be equal to the rate of change (rate of decrease) of the internal energy of the material inside  $V$ , or:

$$-\frac{\partial}{\partial t} (\rho c_p T V) = - \iiint_V \lambda \nabla^2 T dV$$

In the limit  $V \rightarrow 0$ ,  $T$  and  $\nabla^2 T$  are uniform inside  $V$ , and therefore:

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T, \quad \alpha = \frac{\lambda}{\rho c_p}$$

(b) Separation of variables means we seek solutions of the form  $T = X(x)\Theta(t)$ . By putting in the pde, we get  $\alpha X''\Theta = X\Theta'$ , or:

$$\frac{\Theta'}{\Theta} = \alpha \frac{X''}{X} = K$$

with  $K$  the separation constant and  $'$  implying differentiation with respect to the corresponding independent variable. The general form of the solution of these equations is:

$$\Theta = \exp(Kt), \quad X = \exp\left(\pm \sqrt{K/\alpha} x\right)$$

Let us explore the nature of these solutions for various values of  $K$ . If  $K > 0$ , then  $\Theta$  grows exponentially, which is unrealistic for our problem. If  $K < 0$ ,  $\Theta \rightarrow 0$  at large  $t$  for all  $x$ , which is unrealistic since the boundary value is oscillating. Therefore let us test  $K = i\omega$ . In this case,

$$\Theta = \exp(i\omega t), \quad X = \exp\left(\pm \sqrt{i\omega/\alpha} x\right)$$

The equation for  $X$  needs some attention. Using  $\sqrt{i} = (1+i)/\sqrt{2}$ , we get:  $X = \exp\left[\pm(1+i)\sqrt{\frac{\omega}{2\alpha}}x\right]$ , from which we must avoid the  $e^x$  behaviour, and therefore  $X = \exp\left(-\sqrt{\frac{\omega}{2\alpha}}x\right) \exp\left(-i\sqrt{\frac{\omega}{2\alpha}}x\right)$ . Putting everything together:

$$T = T_0 \exp\left[i\left(\omega t - \sqrt{\frac{\omega}{2\alpha}}x\right)\right] \exp\left(-\sqrt{\frac{\omega}{2\alpha}}x\right)$$

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where use of the boundary condition has been made. Taking the real part, we get the final answer:

$$T(x,t) = T_0 \cos\left(\omega t - \sqrt{\frac{\omega}{2\alpha}}x\right) \exp\left(-\sqrt{\frac{\omega}{2\alpha}}x\right) \quad (1)$$

Before finishing, let's make some checks. At  $x = 0$ ,  $T = T_0 \cos(\omega t)$ , as it should. As  $x \rightarrow \infty$ ,  $T \rightarrow 0$ , i.e. the thermal wave does not reach far. (Note that since the heat equation is linear,  $T = 0$  is not unrealistic, since we can understand physically  $T$  as the temperature above some finite value.) As  $x$  increases, the oscillating  $T$  lags behind the oscillation at the boundary and the amplitude decreases.

(c) The student is urged to sketch Eq. (1) carefully, for example in Excel or Matlab. The fact that  $\omega$  appears in both the exponential decay of the amplitude with  $x$  and in the cosine describing the oscillation with  $t$  implies a special form of the  $T$  variation with  $t$  and  $x$ . An interesting animation of this solution (which is also applicable for other problems, e.g. in the viscous fluid flow above an oscillating plate) can be found at:

[en.wikipedia.org/wiki/Stokes\\_boundary\\_layer](http://en.wikipedia.org/wiki/Stokes_boundary_layer)

(accessed June 2010).

## SECTION B

4 (a) Arrivals are independent, so we have a Poisson distribution with intensity  $\lambda = 3000$  per hour.

(b) Arrivals at CPU B are Poisson with  $\lambda_B = 1000$  per hour, as the requests are assigned randomly. The approximating Gaussian has mean  $\mu = \lambda_B$  and variance  $\sigma^2 = \lambda_B$ .

(c) Look up cumulative Gaussian at  $(1050 - \lambda_B)/\sqrt{\lambda_B} \simeq 1.58$  in data book standard Normal table, which is  $p(f|B) = 1 - 0.9429 = 0.0571$ .

(d) For CPU A, the similar probability is Gaussian exceeding  $(2100 - \lambda_A)/\sqrt{\lambda_A} \simeq 2.24$  which is  $p(f|A) = 1 - 0.9875 = 0.0125$  (data book). The probability that the failure was caused by A is given by Bayes' rule:

$$p(A|f) = \frac{p(f|A)p(A)}{p(f|B)p(B) + p(f|A)p(A)} \simeq 0.30.$$

(e) Probability of failure with random assignment  $p(f|B)p(B) + p(f|A)p(A) = 0.0274$ . Optimal assignment corresponds to a single Poisson with rate 3000 exceeding the total capacity 3150, ie the probability of failure is the prob that std Gaussian exceeds  $150/\sqrt{3000} = 2.74$  which is  $1 - 0.9969 = 0.0031$  (ie a much lower failure rate).

(TURN OVER

5 (a) We perform L-U decomposition on the matrix:

$$\mathbf{A} = \begin{bmatrix} 1 & 3 & 1 & 4 \\ -1 & -1 & 0 & -3 \\ 2 & 4 & 1 & 7 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 2 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 3 & 1 & 4 \\ 0 & 2 & 1 & 1 \\ 0 & -2 & -1 & -1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 2 & -1 & 1 \end{bmatrix} \begin{bmatrix} 1 & 3 & 1 & 4 \\ 0 & 2 & 1 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} = \mathbf{L} \mathbf{U}$$

Column space: columns of  $\mathbf{L}$  corresponding to non-zeros rows of  $\mathbf{U}$ , therefore the basis is:

$$\begin{bmatrix} 1 \\ -1 \\ 2 \end{bmatrix}, \begin{bmatrix} 0 \\ 1 \\ -1 \end{bmatrix}$$

Row space: The non-zeros rows of  $\mathbf{U}$ , therefore the basis is:

$$\begin{bmatrix} 1 \\ 3 \\ 1 \\ 4 \end{bmatrix}, \begin{bmatrix} 0 \\ 2 \\ 1 \\ 1 \end{bmatrix}$$

Null space: the solution of  $\mathbf{A} \mathbf{x} = 0$ , or equivalently, the solution of  $\mathbf{U} \mathbf{x} = 0$ . This gives:

$$\begin{bmatrix} 1 & 3 & 1 & 4 \\ 0 & 2 & 1 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Using  $(x_3, x_4) = (1, 0)$  and  $(x_3, x_4) = (0, 1)$  as two sets of values for the free variables, we get the two basis vectors:

$$\begin{bmatrix} 1/2 \\ -1/2 \\ 1 \\ 0 \end{bmatrix}, \begin{bmatrix} -5/2 \\ -1/2 \\ 0 \\ 1 \end{bmatrix}$$

Left null space: the solution of  $\mathbf{A}^T \mathbf{x} = 0$ . Therefore:

$$\begin{bmatrix} 1 & -1 & 2 \\ 3 & -1 & 4 \\ 1 & 0 & 1 \\ 4 & -3 & 7 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

(cont.)



which gives the vector

$$\begin{bmatrix} -1 \\ 1 \\ 1 \end{bmatrix}$$

(b)  $\mathbf{A} \mathbf{x} = \mathbf{b} \Leftrightarrow \mathbf{LU} \mathbf{x} = \mathbf{b} \Leftrightarrow \mathbf{L} \mathbf{c} = \mathbf{b}$ , where  $\mathbf{U} \mathbf{x} = \mathbf{c}$ . For a solution to exist,  $\mathbf{b}$  must be in column space, therefore  $\mathbf{b}$  must be normal to every vector in null space. Therefore

$$\mathbf{b} \cdot \begin{bmatrix} -1 \\ 1 \\ 1 \end{bmatrix} = 0 \Rightarrow -1 + a = 0 \Rightarrow a = 1$$

(c) The general solution will be the particular solution plus a linear combination of the null space basis vectors. To find the particular solution, we first find  $\mathbf{c}$  given by  $\mathbf{Lc} = \mathbf{b}$ , which gives  $\mathbf{c} = [1 \ 1 \ 0]^T$ , and then we solve for  $\mathbf{Ux} = \mathbf{c}$ . Therefore:

$$\begin{bmatrix} 1 & 3 & 1 & 4 \\ 0 & 2 & 1 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}$$

(putting zero's for the free variables), which gives  $x_1 = -1/2$  and  $x_2 = 1/2$ . Therefore the general solution is:

$$\mathbf{x} = \begin{bmatrix} -1/2 \\ 1/2 \\ 0 \\ 0 \end{bmatrix} + z \begin{bmatrix} 1/2 \\ -1/2 \\ 1 \\ 0 \end{bmatrix} + t \begin{bmatrix} -5/2 \\ -1/2 \\ 0 \\ 1 \end{bmatrix}$$

By performing the multiplication  $\mathbf{Ax}$ , it is easy to show that  $\mathbf{Ax} = \mathbf{b}$ .

(TURN OVER)

6 (a) Provided the eigenvectors of  $\mathbf{A}$  span  $\mathfrak{R}^N$ , any vector  $\mathbf{x}$  can be written as  $\mathbf{x} = a_1\mathbf{u}_1 + a_2\mathbf{u}_2 + \dots + a_N\mathbf{u}_N$ , where  $\mathbf{u}_1$  etc are the eigenvectors with corresponding eigenvalues  $|\lambda_1| > |\lambda_2| > \dots > |\lambda_N|$ . Then,  $\mathbf{A}^k\mathbf{x} = a_1\lambda_1^k\mathbf{u}_1 + a_2\lambda_2^k\mathbf{u}_2 + \dots + a_N\lambda_N^k\mathbf{u}_N$ . For large  $k$ , the first terms dominate, so  $\mathbf{A}^k \approx a_1\lambda_1^k\mathbf{u}_1 + a_2\lambda_2^k\mathbf{u}_2$ , which implies

$$\frac{|\mathbf{A}^{k+1}\mathbf{x}|}{|\mathbf{A}^k\mathbf{x}|} \approx \lambda_1$$

The rate of convergence is determined by  $|\lambda_1/\lambda_2|$ .

(b) The matrix  $(\mathbf{A} - 3\mathbf{I})^{-1}$  has eigenvalues  $(\lambda_i - 3)^{-1}$ , where  $\lambda_i$  are the eigenvalues of  $\mathbf{A}$ . The closest eigenvalue to 3 will be the largest (in magnitude) eigenvalue of  $(\mathbf{A} - 3\mathbf{I})^{-1}$ . We expect the convergence rate to be:

$$\left| \frac{\lambda' - 3}{\lambda - 3} \right|$$

with  $\lambda$  the nearest eigenvalue to 3 and  $\lambda'$  the next nearest.

(c)

$$(\mathbf{B} - \mathbf{I})^{-1} = \begin{bmatrix} 0 & 0.1 \\ 0.1 & 0 \end{bmatrix}^{-1} = \begin{bmatrix} 0 & 10 \\ 10 & 0 \end{bmatrix}$$

Therefore:

$$(\mathbf{B} - \mathbf{I})^{-1}\mathbf{x} = \begin{bmatrix} 0 & 10 \\ 10 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 10y \\ 10x \end{bmatrix}$$

and

$$(\mathbf{B} - \mathbf{I})^{-2}\mathbf{x} = \begin{bmatrix} 100x \\ 100y \end{bmatrix}$$

which evidently means that  $(\mathbf{B} - \mathbf{I})^{-1}$  has eigenvalue 10,  $(\mathbf{B} - \mathbf{I})^{-2}$  has eigenvalue 100, etc., therefore the eigenvalues of  $\mathbf{B}$  are  $1 \pm 0.1$ , i.e. 0.9 and 1.1. (Note: by performing the calculation of the eigenvalues of  $\mathbf{B}$  one finds the same values.) The procedure does not work for the eigenvectors because it enters a cycle.

(d) The inverse power method implies  $\mathbf{y}_k = (\mathbf{A} - \alpha\mathbf{I})^{-1}\mathbf{y}_{k+1}$ , with  $\mathbf{y}_k = (\mathbf{A} - \alpha\mathbf{I})^{-k}\mathbf{x}$ . It is computationally cheaper to solve  $(\mathbf{A} - \alpha\mathbf{I})\mathbf{y}_{k+1} = \mathbf{y}_k$  with an LU factorisation.

**END OF PAPER**